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SIMPLE

ELEMENTS OF NAVIGATION.

BY

LUCIEN YOUNG,



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PREFACE.

This little work is not intended to supply any presumed deficiency in other books treating of the same subject, but to preserve one common method throughout and to omit all complicated mathematical formulæ and calculations beyond the reach of men of limited education.

The most simple elements of navigation only are treated of, and the tables added to make the little work complete in everything necessary to navigate a vessel to any port of the globe.

By a study of no other instructions than those contained in this little treatise, the nautical apprentice can soon fit himself for promotion; the merchantman make himself competent to conduct his vessel to his destination; and the owner of a yacht, with a little trouble, become able to co-operate with his captain. Other works are intended for the use of accomplished mathematicians or experienced navigators.

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SIMPLE ELEMENTS OF NAVIGATION.

CHAPTER I.

DESCRIPTION AND USE OF INSTRUMENTS.

Definitions. NAVIGATION is the science which treats of the determination of a ship's position at sea and the particular direction a vessel should steer to reach any given place. It may be said to consist of two kinds:

Firstly, the science of navigation by which the position of the ship is determined from day to day by referring it to some other geographical spot, such as a known landmark, a determinate bottom, or a previously defined place.

Secondly, the science by which the position of the ship is determined from observations of the heavenly bodies.

The voluminous works on this subject are full of difficult and complicated calculations, which only an expert mathematician could understand. They are beyond reach of the class of young men of limited education, who enter an apprentice-ship either in the merchant marine or the naval service. Moreover, these works are filled with many methods by which the same problem is solved, embarrassing to the beginner instead of instructing him.

In order to simplify this as much as possible it is proposed to imagine a vessel in port with everything stowed ready for sea, and to confine the problems to the most common methods in her voyage to some other port across the ocean.

Use of Instruments. The first thing to do on going on board is to become acquainted with the use and application of such instruments as are necessary to determine the distance which the ship sails, the direction in which she is steered, and

to deduce, from the data these instruments furnish, the situation of the ship at any time, and to find the distance and direction of any place to which it may be required that the ship should be taken.

Hand-lead is used to obtain soundings in shallow water, with a view of safely guiding the ship over shoals, through channels to an anchorage, or to sea; it is in weight ranging from five to fourteen pounds.

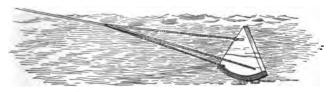
Deep-sea Lead is used to obtain soundings in deeper water and to ascertain the nature of the bottom; it is in weight ranging from twenty-five to one hundred pounds; is hollow at the bottom, for placing a lump of tallow called the Arming. The nature of the bottom is indicated by the portion of the bottom brought up in the arming.

In heaving this lead the headway of the ship must be checked to get a cast; to obviate this many ingenious instruments have been invented by which the soundings can be taken from a ship running at full speed, in water of any depth not exceeding one hundred and fifty fathoms (a fathom is six Some of these instruments register the depth of water descended through by wheel-work set in motion by a fly, and others by the condensation of air contained in a glass tube by the pressure of water; but the most common one in use is the Thomson sounding-machine, which has a glass tube connected with a sinker, closed at the top and coated inside with chromate of silver; the increased pressure at greater depths drives the water up the tube, and its action leaves a white mark, the position of which is estimated by a scale, and it is independent of the amount of line run out. A small steel wire is used instead of a line, and is coiled on a light reel.

Log and Glass are used to measure the rate of sailing, and a timepiece to note the interval. The log consists of several parts—chip, bridle, line, and reel.

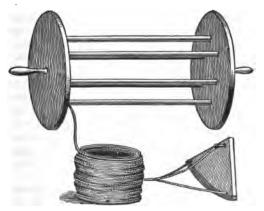
Log-chip is a thin piece of wood, in the form of a sector of about five inches radius, weighted on the circular edge with lead sufficient to make it swim upright in the water.

At each of the three corners is a hole, through which two of the legs of the bridle are rove and knotted; the third leg has a peg of wood in the end, which, when the log is hove, is firmly pressed into the unoccupied hole: it remains thus while the line is running out, and pulls away when the line is being hauled in. The legs of the bridle are about two feet long, and bent to the outer end of the log-line.



LOG-CHIP.

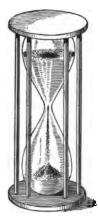
Log-line is a small line of about 150 fathoms long, one end attached to the bridle and the other fastened to a "reel," over which the log-line is wound. At about 15 fathoms from



LOG-REEL.

the chip a white rag is placed to mark what is called the "stray-line," which permits the chip to clear the wake of the ship or swash of the propeller. From this rag inboard the line is divided into equal portions by bits of small line through the strands of the log-line, and designated by the number of knots in each; hence are called knots. The length of each of these divisions of the line bears the same ratio to the nautical mile that the glass does to an hour. The division of the line between the knots is divided into tenths, marked by a small string.

Log-glass is an ordinary sand-glass constructed so as to



LOG-GLASS.

permit the sand to run from one end to the other in a certain time: those in common use are the long-glass, which requires 28 seconds, and the short-glass, 14 seconds, to run through. The line is graduated for the long-glass, and when the short-glass is used the knots indicated should be doubled.

Heaving the Log. In using these it is called heaving the log. One man holds the reel in a horizontal position and another holds the glass with the sand down, while a third takes the log-chip and presses the peg into its place, then unwinds a quantity of line, and holding it faked in his hand, calls "Clear glass," repeated by the man holding the glass. The one with the line throws the chip

over the lee quarter to clear the wake, and permits the line to run freely through his hand, feeding and checking if neces sary, and when the white rag passes his hand he cries out "Turn;" the glass is then turned. The glass-holder answers Turn, and holds the glass up so as to permit the sand to run through. The moment the sand is run out the glass-holder calls out "Up," when the line is checked and the knots and tenths indicated. The log is hove every hour, and should be whenever the course is changed.

Log Adjustments. The log requires to be frequently adjusted, to do which the peg should be examined and found to fii sufficiently tight. The log-line shrinks unequally, and requires to be frequently verified. A convenient method is by having nails placed in the deck at proper distances to measure from, the line being wet at the time. In damp weather the sand in the glass becomes wet, and is not only retarded, but often hangs altogether: when this is the case the cork stopper in the end is removed, the sand taken out and replaced by dry, or the quantity of sand can be reduced or increased in this way when the glass is in error. The glass error is found by comparison with the second hand of a watch or a small second pendulum. A pendulum for comparison can easily be constructed

by having hung from a nail a small bullet by a thread 38½ inches long from the centre of the bullet to the nail.

Many and most efficient patent logs have been devised, and have been found very accurate, and have been frequently substituted for the common log; however, one acts as a check on the other, and both should be used. The most common of these is the **Taffrail Log**, which consists of a rotator or fly towed astern clear of the wake by a line, and the register is attached to the taffrail. As the fly is drawn through the water in a horizontal position, the motion is communicated by means of the connecting cord to the wheel-work within the register, and sets in motion the indices. By this means the rate of the ship can be read off at any time by simply going to the rail and noting the interval it takes the dial to make one mile.

Ground-log is a log adapted for use in shoal water to ascertain when in doubt the set of the current; it consists of a small lead and a line divided in the same manner as the common line. When hove, the lead remains on the bottom and the line gives the combined motion of the ship through the water and that of the current.

Compass denotes the direction sailed, and indicates the future course. The compass is simply an instrument which utilizes the directive powers of the magnet.

Card and Needle. The essential part of the mariner's compass consists of a circular card upon which are marked the various points, and is carried by a magnetized needle placed under the line joining the north and south points.

The needle is freely balanced upon a fine pivot rising from the bottom of a brass or copper bowl by means of a small agate cup fixed in the centre of the needle.

Compass Bowl, containing the needle and card, is carried on gimbals, so that it may at any time remain level in whatever direction the ship may roll or pitch. The bowl has a glass cover, and is fitted to carry lights to illuminate the face of the card at night. This case and stand is called the Binnacle.

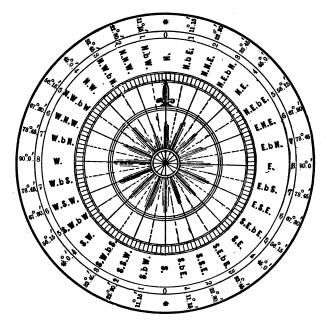
Lubber's Point. Inside the bowl is painted a black vertical line, commonly called the *lubber's point*. The centre of the compass card and this lubber's point should be in a line with the keel of the vessel, and the point marked on the card

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the ship is to be steered should be kept coincident with this point.

Points of the Compass. The compass card is divided into four quadrants by two diameters perpendicular to the other; the ends of these diameters are called north, south, east, and west, and are marked N., S., E., W.: they are termed the "Cardinal points." Each of these quadrants is divided into eight equal spaces or points; hence there are thirty-two points to the compass. These thirty-two points are in turn subdivided into half and quarter points.

The following figure will show the names of these points.



MARINER'S COMPASS.

The half and quarter points are indicated from any of the 32 points towards one of the cardinal points, thus: N. ½ E. means half a point from the north towards the east. SW. ½ W. means half a point from the southwest towards the west.

Boxing the Compass. To be able to repeat the names of these points consecutively is called boxing the compass.

The compass card is also divided into degrees for the convenience of taking bearings, and the following table will give the points, half and quarter points, with the corresponding degrees from which they can be easily converted one to the other.

	Degrees.	80
mi	Points.	0998-75503220922-44403220220226-55550
S INTO DEGREES.	S. to W.	A HARA BARA WAYA WAYA WAYA WAYA WAYA WAYA WAYA W
CONVERTING POINTS	S. to E.	QQQQQQQQQQQQQQQQQQQQQQQQQQQQQQQQQQQQ
TABLE FOR CONT	N. to W.	NNNNNNNNNNNNNNNNNNNNNNNNNNNNNNNNNNNNNN
	N. to E.	NNNNNNNNNNNNNNNNNNNNNNNNNNNNNNNNNNNNNN

According to the purpose for which the mariner's compass is especially adapted it is named the steering, standard, and azimuth compass.

Steering Compass is the one placed in the binnacle near the wheel to assist the man at the wheel in keeping the ship's head in the prescribed direction.

Standard Compass is the one placed on a particular spot on deck or above it where the local influence of the iron in the ship is the smallest and to which the steering compass is always referred.

Azimuth Compass is the one mounted on a stand in some commanding position for the purpose of taking bearings, and is provided with a pair of sight vanes for observing objects. The standard compass is usually an azimuth compass.

Variation. The direction the horizontal needle assumes when uninfluenced by external causes is called the magnetic north, and at different times and places does not coincide with the true north. The difference between these two directions measured in degrees is called variation. It is said to be easterly when the north end of the needle is drawn to the eastward, and westerly when it is drawn to the westward, of the true north. The variation is found on the chart.

Deviation is the term applied to indicate the effect produced on the compass by objects within the ship, such as the ship being built of iron, laden with iron or having certain attachments made of iron, and local influences external to the ship. Vertical iron, such as boat-davits, iron stanchions, smokestack, etc., has the greatest effect when the ship's head is north or south and least when east or west; and the horizontal pieces of iron, such as deck beams, engine shafts, etc., will affect the compass most at the four points lying between the cardinal points and least at the north, south, east, and west points.

The introduction of iron in shipbuilding has rendered the question of deviation most important, and the amount will depend upon the direction in which the ship's head lies while building; if built with her head north and south she will receive a large amount of induced magnetism from the hammering necessary and from the earth. This magnetism once driven in, may be increased or diminished by grating against piers, striking sunken rocks, or being struck by a heavy sea.

It has also been found the deviation is different when the vessel heels over on either side to what it was when she is on an even keel: in northern latitudes the compass needle is drawn to wind ward as the vessel heels over, and whenever the

vessel head is E. or W. the heeling error vanishes and is greater when it is N. or S.

The deviation changes when the ship proceeds to a different latitude, hence should be frequently ascertained and tables constructed by the process of swinging ship not only on an even keel, but also when the ship is heeled over to starboard and when heeled over to port.

To Find the Deviation. The standard compass is placed in its permanent position, and the ship is taken to some place in smooth water and caused to swing around that her head may be made to come to every point of the compass, and as she does the deviation is ascertained as follows:

I. By means of buoys the true bearings of which have been previously ascertained.

II. When in an open harbor where some fixed object at a distance of eight or ten miles can be clearly seen. Write down the points of the compass, and as the ship swings around from one point to another write down the compass bearing of the object opposite the point of the compass towards which the ship's head is directed. The mean of two bearings on east and west by compass, or the mean of all these bearings, will be the magnetic bearing of the distant object from the ship, the difference of which from each of the bearings will give the deviation for that point of the ship's head. It is thus that the majority of deviation tables are constructed.

III. When the ship is in a closed harbor and no distant object can be seen, a standard compass is taken on shore and placed in such a position as to be free from the influences of magnetic attraction, and where it may be seen. As the ship swings around the bearing of the compass on shore is observed from the ship as her head comes to each point, and at the same instant, indicated by signals, the ship's compass is observed from shore. The observations on shore are first reversed to bring them into the same direction as those taken from the ship, and are compared with the latter; the difference is the deviation. Should there be a suspicion of local attraction to the compass on shore a plane table may be used instead of the shore compass.

IV. When at sea or out of sight of land if a distant sail be in sight, advantage may be taken of a calm or light airs to swing

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SE. SE. by S. SSE. S. by E.

ship by it as in the second case or by the true bearing of the sun explained in Chapter VIII.

The deviation for the ship's head at each of the points of the compass having been obtained by any of the processes which have been described, a table of the results should be constructed, marking the deviation east when the north end of the needle has been drawn to the eastward, and west when it has been drawn to the westward, of the magnetic north. These tables should be constructed and made use of even though the compasses be or be not corrected by magnets or masses of iron as is the practice in iron ships.

The following is the form of a deviation table:

Ship's head.	Deviation.	Ship's head.	Deviation.
North.	2 20 E.	South.	2 40 W.
N. by E.	8 40 E.	S. by W.	8 50 W.
NNE.	5 40 E.	SSW.	5 50 W.
NE. by N.	6 50 E.	SW. by S.	6 00 W.
NE.	8 00 E.	SW.	6 30 W.
NE. by E.	8 10 E.	SW. by W.	7 30 W.
ENE.	7 20 E.	wsw.	7 50 W.
E. by N.	7 30 E.	W. by S.	8 10 W.
East.	6 40 E.	West.	8 00 W.
E. by S.	5 50 E.	W. by N.	7 40 W.
ESE.	4 30 E.	WNW.	6 40 W.
SE by E	8 40 TC	NW hy W	5 40 W

DEVIATION TABLE.

Leeway is an apparent error to which the compass is subjected, and is due to the pressure of the wind and surge of the sea driving the vessel to leeward, when close hauled to, of the direction by compass it is intended she should sail. The amount depends upon the lines and trim of the ship, the draft and sails used, or whether the ship be as near the wind as she will lie. Leeway is estimated in points and quarter points by observing the wake astern. If the wind is on the starboard hand the leeway is to the left, and if on the port hand it is to the right.

Course of a ship and the bearing of an object are terms used with reference to the standard compass, to the magnetic meridian, and to the true meridian. The course of the ship by

the standard compass, which is affected by both deviation and variation, is called the "compass course;" the course with reference to the magnetic meridian, or the course which would be shown by the compass on board affected by variation only and not by the deviation, is called the "correct magnetic course." The course with reference to the true meridian is called the "true course." In the same way the bearing of an object may be distinguished as the compass bearing, correct magnetic bearing, or the true bearing, as the case may be.

In any conversion from one compass course to another, or from one compass bearing to another, whether the correction is made by applying the variation or the deviation, both corrections are applied to the right if easterly, and to the left if westerly. Similarly, where the conversion is from one true course to another or from one true bearing to another, both are applied to the right if westerly, and to the left if easterly. The method will appear in the following examples.

A vessel heads by compass NNE. ½ E. The variation shown on the chart is 21° 14′ E.; find the true course.

The compass cour						
Variation E				. 21	14 00	right
The magnetic cou	rse			N. 49	21 30	E .
From table deviati	on for	NN.	E. 🛊 F	c. 6	15 00	E. or to right.
True course				. N. 55	36 30	E.
Again with the	hood		ha =	agol of	ESE	the warietien

Again with the head of the vessel at ESE. the variation was shown on the chart to be 10° 15′ W.; find the true course. From compass table ESE. is . . . S. 67° 30′ 00″ E.

Variation from chart W		10	15	00	left.
True magnetic course	S				E.
Deviation for ESE. from table E.		4	30	00	right
True course	g	73	15	00	E

The variation being given by the chart may be considered as a constant quantity, but not so with the deviation, which may vary for every point of the ship's head. The frequent use of the deviation table might result in mistakes, to avoid which, it will be better to construct another table for the convenience of the compass course or bearing to convert to the magnetic course or bearing and vice versa. The compass

course or ship's head is written in the first column, the deviation in the second as found from the observations already described, and the magnetic course in the third column, thus:

Ship's	Devia-	Magnetic	Devia-	Magnetic	
head.	tion.	Course	tion.	Course.	
North. N. by E. N. by E. N. E. by N. N. E. by E. E. by N. East. E. E. by E. SE. by E. SE. by S. SE. S. E. S. E. S. By E.	2 20 E. 3 40 E. 5 40 E. 8 10 E. 8 10 E. 7 20 E. 7 30 E. 4 30 E. 4 30 E. 2 00 E. 1 30 W. 1 30 W.	N. 2 20 E. N. 14 15 E. N. 40 85 E. N. 53 00 E. N. 54 25 E. N. 74 50 E. S. 83 20 E. S. 63 00 E. S. 52 35 E. S. 43 00 E. S. 32 45 E. S. 12 45 E.	South. 8. by W. SSW. by S. SW. by S. SW. by S. W. by S. W. by S. West. W. by N. WNW. NW. by N. NW. NW. by N. NW.	7 50 W. 8 10 W. 8 00 W. 7 40 W. 6 40 W. 5 40 W. 4 30 W.	S. 2 40 E. S. 7 25 W. S. 17 10 W. S. 27 45 W. S. 38 48 45 W. S. 59 40 W. S. 70 35 W. S. 82 00 W. N. 86 85 W. N. 61 55 W. N. 36 55 W. N. 24 50 W. N. 25 W. N. 26 55 W. N. 10 45 W.

To obtain the correct magnetic course from the compass course, look in the first column for the compass course, the second column gives the deviation when the vessel's head is on that point, and the third column will be found the magnetic course.

In order to correct any bearings taken by the compass the table is to be entered with the direction of the ship's head at that time in the first column, and corresponding thereto in the second column will be found the amount of deviation to be applied, as per example: If a ship's head is NNE, the bearing of two islands be SE, and W, by S, by the compass. In the second column of the table and opposite to NNE, the deviation is 5° 40′ E.; applying this deviation to the right the correct magnetic bearing of the two islands will be S. 39° 20′ E., and S. 83° 55′ W., or roughly in points SE, ½ E. and W. ½ S.

The Chart is used to plot the position of the ship at any time and refer it to other known objects. Its construction has especial reference to the requirements of navigation. Thus the chart may be required for coasting purposes, in which case the harbor or coast charts are used, upon which are marked with great accuracy, the rocks, shoals, local cur-

rents, nature of the tides, soundings and channels as well as the different aids to navigation and their bearings.

For off shore cruising the Mercator Chart possesses so many advantages that it is universally adopted for sea purposes.

For the purposes of navigation and in order that the relative positions of places on the earth's surface may be laid down and quickly found, certain lines are supposed to be drawn upon the sphere.

These imaginary lines of reference are called **Parallels of Latitude** and **Meridians**, and when these are known for any
given place its position upon the globe is precisely determined
by their intersection.

The extremities of the axes of the earth are called the Poles, and the great circles passing through these poles are called Meridians. It is customary with us to call that meridian which passes through Greenwich the First or Prime Meridian.

The great circle drawn around the earth at equal distance from the poles, and perpendicular to the meridians, is called the **Equator**.

The equator and the prime meridian are the first lines of reference from which latitude and longitude are measured.

Latitude. The lines of latitude run due east and west, and are small circles of the sphere drawn parallel to the equator; we may conceive one of these drawn through every place. The portion of a meridian intercepted between a place and the equator is called the latitude, and is denominated north or south as the place is north or south of the equator.

Longitude. The longitude of a place is the portion of the equator intercepted between the prime meridian and the meridian passing over the place; is east or west according as the place is situated east or west of the prime meridian.

As every circle large or small is divided into 360 parts called degrees, it will be seen the equator and poles divide every meridian into four equal parts; therefore the greatest latitude a place can have is 90 degrees, and again the prime meridian divides the parallels of latitude into two equal parts, making 180 degrees the greatest longitude a place can have. Each of these degrees is divided into 60 minutes and the

minutes into 60 seconds. The minutes of the equator and of the meridians are each nearly 6080 feet long, and are called Nantical or Sea-miles.

The parallels of latitude being small circles and decreasing in size the nearer they approach the poles, while the meridians come together at the poles, it would be difficult to construct a chart easy to use in practice. However, upon the principles of Mercator a chart is constructed upon which the meridians are represented as being parallel to each other during their whole length, and the distance between the parallels of latitude is increased in the same proportion the nearer they approach the poles. This enables a course from one place to another to be laid down by a straight line between them, and the distance is obtained from the scale to the side of the chart as nearly opposite the two places as possible.

Ali charts are engraved true north and south, east and west, and in all the charts furnished by the Hydrographic Office the true compass is engraved in various places and the bearings given are the true bearings. Lines of variation are drawn upon the chart or the variation is given marked with each compass on the chart.

Currents are marked on the chart by an arrow with two feathers pointing in the direction towards which it sets And the drift or rate per hour at which it moves is marked in knots close to the arrow.

The set of the tide is marked on the chart by an arrow feathered on one side only for the flood > and by an arrow without feathers for the ebb tide >

The tide is spoken of as flood when the water is rising, and as ebb when the water is falling; and to show when either occur, the time of high water at the full and change, that is to say at full moon and new moon, is given at the most important places on the chart. The hours are marked in Roman and the minutes in ordinary figures, thus, VII h. 50 m. For any particular spot this time of high water at the full and change may be considered practically constant. Any almanac will give the moon's age; but by a little practice it may be guessed within a day. When it looks like a D it is increasing or waxing, and when it looks like a C it is decreasing or waning.

The rise of Spring Tides or those which occur near the full and change of the moon, and the rise of the Neap Tides or those which occur near the 1st and 3d quarters of the

moon, are given in feet. Sometimes this information about the tides is given in a table on the chart.

Tides are caused chiefly by the moon, and as the moon is about 50 minutes later every 24 hours in coming over the same spot of the earth, the time of high water will be about 50 minutes later every day. In most places the tide rises twice in every 24 hours, which would make a regular interval of 12 hours between the times of successive high water, and 25 minutes additional for the retardation of the moon.

The calculations for finding the exact time of high water are puzzling, and require tables that may not be at hand. It is important to know the time, because in many channels it is only at high water that a vessel can get over the bar. First find the number of days from the last new or full moon, multiply this by 50, the number of minutes that the high tide is delayed each day, and add the product in hours and minutes to the time of high water given on the chart. A.M. or P.M., as the case may be. Or you can reckon forward the number of days to the next new or full moon, and then subtract the product from the time on the chart. The question whether you will reckon backwards or forwards depends on whether the last new or full moon, or the coming new or full moon, is furthest off. Of course you will reckon to whichever is nearest.

The time of high water obtained in this way may be depended upon within the hour, yet it may be out at times as much as two hours. The greatest error will occur during neap tides, hence by subtracting one hour from the time of high water at neap tide, will diminish this error. The following table will show how the rule works:

"	2 3 4 5	day " " "	: : : :	:	:	:	•	:	:	:	:		1 4 2 8 8 2 4 1	in. 60 80 80 80 80 80
---	------------------	--------------------	---------	---	---	---	---	---	---	---	---	--	--------------------------	---

^{*} At neap tide subtract 1 h. from time of high water.

For example. The high water at full and change at Old Point Comfort is 8.46; at what time will it be high water on the 10th June, 1888?

From any almanac we find that in June the new moon occurs on the 9th in the afternoon, and the full moon on the 23d in the afternoon. Now the 10th of June is one day after the new moon, therefore to the above table we must add 50 minutes to 8.46, which gives 9.86 P.M. as the time of high water on the 10th of June.

Again, what time will it be high water on the 20th of June? Now the 20th of June is three days before the full moon, therefore, from the above table we must subtract 2.30 from 8.46, which gives 6.16 P.M. as the time of high water on the 20th of June.

The soundings marked on the chart are reduced to mean low water, and are generally given on the plain section in fathoms (of six feet) and fractions of a fathom; and on the shaded surface in feet and fractions of a foot.

Large charts are constructed for each ocean upon a too small scale for practical purposes when near shore, but to facilitate their use they are divided into marked sections accompanied with an index chart. These sectional charts have engraved upon them at the most convenient places, divided from the rest of the chart, a plan of the most important harbors upon a scale large enough for the various marks to be indicated and the nature of the channel understood.

With the chart use is made of a pair of dividers and parallel rulers, the application of which will be shown in working some of the problems.

SIGNS AND ABBREVIATIONS MARKED ON THE CHART.

An anchorage Bk bank C cape Ch church Chan channel Cr creek Fms fathoms Ft feet or foot H W high water, full and change I island Lat latitude Long long
Lt light Lt. F light fixed Lt. F! light fixed Lt. Fl. light fixed Lt. Int. light intermittent Lt. Rev light revolving Lt. Fig. light floating Lt. Occ. light occulting Lt. Alt. light alternating L. W low water Mt mountain

CHARACTERISTIC SIGNS MARKED ON THE CHART.

)	SIMPLE EI	LEMENTS OF NAV	IGATION.
	MINO MILLE	NWOT.	WOODED MARSH
	ROOM WITH	CH CHACLAND DEPTH GOVERN	DOUBTFUL ROOMS
	Tanyo Mula odviše	OUND CHAN CHANGE	ORAVEL BANK
	SYAMP OR WARRING	BEOGET ALLOON	27 + 5 27 +
	CUPPY COAST LINE	BHORE, STEEP TO BANDY	Digitized by

GRAGE	MUD BANK,DRY	ANCHORAGE FOR LARGE VESSELS	A THE STATE OF THE
OAK	ROCKS IN SIGHT	ANCHORAGE FOR	Н Н Н Н Н Н Н Н Н Н Н Н Н Н Н Н Н Н Н
PINE	MOORING BUOV	OODAL, REEFS	
ACT ON HOH ONE	PROPERTY AND THE	& SANDDRY XT LOW WATER	BANDY BEACH
MANAGOVE	WOOM WASH	OUTTWITE GROUND	1000 年 1000 年 1000 年 1000 日 1000 日 1

EXAMPLES.

- I. The compass course is ESE., or S. 67° 30′ 00″ E. The variation and deviation 2½ points E., leeway ½ points right. What is the true course?

 Ans. S. 28° 07′ 00″ E.
- II. The compass course is SSW., the variation being 1 point easterly. Find the true course.

 Ans. SW. by S.
- III. An object bore by compass NE. by E. ½ E., the variation being 1½ westerly. Find its true bearing. Ans. NE. ½ N.
- IV. Compass course is S. and the wind is NW., giving a points leeway, variation 1 point E. and the deviation 1 point W. Find the true course.

 Ans. S.
- V. The true course is S. by W.; variation is 2 points W.; deviation is 5° W. Find compass course.

Ans. S. 62° 30' 00" E.

- VI. The true course is W. by S., and the variation is 11° 15′ E., deviation is 9° W., wind NNE., leeway of 2 points. Find the true course.

 Ans. N. 81° W.
- VII. The compass course is SSE., with variation 2 points W., and deviation 5° E., the wind on the left hand giving 3 points leeway. Find the true course.

 Ans. S. 6° 15′ E.
- VIII. The compass course is NE., and variation is 2 points E., deviation 2° E., wind on the right hand giving 3 points leeway. Find the true course.

 Ans. N. 38° 45′ E.

CHAPTER II.

PILOTING OR COASTING.

HAVING become thoroughly familiar with the instruments described, the ship is gotten underway and taken down the harbor or bay for an offing at sea. In doing this the rudest manner of navigation is used, called **Piloting or Coasting**, which requires only a local knowledge of the shore and its adjacent waters, together with the location of marks placed to aid navigation, all of which are given in the charts.

The effect of the tides and local currents along the shore is most treacherous, and may at any time cause the ship to be drifted out of the channel or into a dangerous position to some reef or shoal, to avoid which the actual position is often a matter of vital importance. A frequent cast of lead may give warning, and should be constantly kept going whenever on soundings, and carefully taken. If the ship is becalmed the ground log will indicate the direction and rate of drift.

Cross-bearings. When two known objects are in sight the ship's position is found by cross-bearings. Thus, as the ship proceeds down the channel the starting-point buoy bore per compass ENE., and a lighthouse N. 4 W., while the ship's head was NW. Enter the deviation table, which should always be at hand in a little note-book, with the ship's head NW. in the first column, and the deviation to be applied in the second column is 4° 30′ W. Applying this to the left will give the magnetic bearings; and if the variation was 5° E., apply it to the right, and the true bearings will be:

Si	tarti	ng B	uoy		Lighthouse.
By compassN.	67°	30 ′	E.	N.	8° 20′ W.
Deviation W	4°	80′	left		4° 30' left
Magnetic bearingN.	63°	00'	E.	N.	12° 50′ W.
Variation E	5°	00'	right	itized.	5° 00′ right
True bearingN.	68°	00'	E.	N	7° 50′ W.

Apply the parallel ruler to the engraved compass on the chart lying along N. 68° E. and the centre of the compass; then work the ruler until the edge touches the start buoy and draw a pencil line along its edge on the chart. Apply in like manner the N. 7° 50′ W. line to the lighthouse. Where these two lines cut each other will be the position of the vessel.

The bearings of these two points should not be too near each other, for then the lines would have a bad intersection; but if the two objects be in line, it is of great advantage, especially so when in the direction the ship is steering, as their separation will indicate a deviation from the channel.

Where the two lines cross, or the position of the ship, it is marked by a little pencil cross with the hour and date thus, $\times_{12/3}^{2P.K.}$, to identify it, which means the ship was in this position at 2 in the afternoon of March 12.

Bow and Quarter Bearing. A very simple means of finding the constant position of the ship is by what is known as the bow and quarter bearing. Take the bearing of one known object on shore when it is on the bow and measure the distance by log till it bears abeam; then the distance, should there be no current, will be the distance of the object when abeam.

Bearing of One Object. When it is impossible to get a bow and quarter bearing, such as having to change the course, the ship's position can be found by taking the bearing of the point when not in the direction the ship is sailing, and when the bearing has changed at least 3 points take a second bearing. Lay off from the given point the two bearings corrected for variation and deviation, and, after laying the parallel ruler in the direction of the true course, take the distance sailed in the dividers and move the ruler towards the given point till the distance fits exactly between the two lines and draw a pencil line. At the two points of intersection will be the first and second position of the ship.

Whenever the vessel is in the vicinity of land this method should frequently be used as a check to the influence of unknown currents.

By Sailing Directions or Chart. When the channel has long stretches winding between shoals or among islands, the sailing directions or chart gives the true or magnetic courses and bearings. Suppose they are magnetic, such as steer

NE., till a certain object bears N. by W., and then steer E. till another object bears SW. In such a case the magnetic course and bearing are given to find the compass course and bearing of the object. Look in the 3d column of the deviation table for the magnetic course, expressed in degrees and minutes.

If it be not one of the courses it will lie between two of them, and the corresponding compass course will lie between two courses in the 1st column and may be found by estimating. To find the compass bearing look in the 3d column for the magnetic course; opposite to it in the 2d column will be the deviation on that course.

Apply this deviation to the magnetic bearing to the left if the deviation is easterly and to the right if westerly.

EXAMPLE.

Suppose the chart should give directions to steer E. till a certain object bore N. by W., then steer SE. till another object bore SSW. magnetic.

In column 3, when the course was E., the deviation was between 6° 40′ E. and 7° 30′ E., or nearly ½ point E. Applying this to the left of the first course, the vessel should steer E. ½ N. by the compass till the first object bore by compass N. by W. ½ W. So from column 3 with the course SE. the deviation is between 2° 00′ E. and 3° 40′ E., or nearly ½ point E. Applying this to the left of the second course, the vessel should steer SE. ½ E. till the second object bore by compass S. by W. ¾ W.

In going around a point and no channel marked out, select several spots on the chart, the connection of which will per mit the line joining them to pass over safe soundings. With the points of the dividers on two of the spots, transfer them to the scale and measure the distance; then with the edge of the parallel ruler along the line, move it to the nearest compass, and the point over which the edge comes will be the true course; correct this for variation and deviation to get the compass course. Put the ship's head on that course and sail the distance, when the same process will be repeated.

Should the ship be shut in by a fog or snow storm for a time out of sight of land, the channel and nature of the bottom, as well as soundings by the hand or deep-sea lead, will give a close approximation to the position of the ship.

When the latitude and longitude are known, the position of the ship is plotted on the chart by laying the parallel ruler even with the nearest parallel of latitude marked on the side of the chart, and after moving it up to the given latitude draw a pencil line, which will represent the latitude of the ship; then measure with the dividers at the top and bottom of the chart the distance from the nearest meridian to the given longitude, which, set off on the parallel previously drawn with pencil, will be the ship's position.

To Verify the Deviation Table. When the vessel was swung in the harbor for deviation there might have been some local attraction unknown which would of course affect the local deviation table. To ascertain this, it is an excellent opportunity, as the vessel proceeds along the various courses in the channel, to verify the deviation table by frequent bearings of known objects on shore, or when two objects come in line. The chart will give their true bearings, and when converted to the compass bearings by the application of variation and deviation there should be no difference between this bearing and the compass; if so, the deviation is wrong and must be corrected before going to sea.

CHAPTER III.

DEAD-RECKONING.

Shaping the Course. The vessel having now arrived at the point where it becomes necessary to commence her voyage at sea, the bearing and distance to the point it is intended to take the vessel are found from the chart by laying the ruler with the edge along the two places, then transfer the ruler to the nearest compass on the chart, which will give the true bearing. Correct the true bearing for variation and deviation to the left if easterly, and to the right if westerly, for the compass course, and the ship is kept as near that course as the wind and other circumstances will admit.

With the dividers, measure the distance on the scale to the side of the chart as nearly opposite the two places as it is possible.

If islands, capes, and headlands intervene, it will be necessary to find several courses and distances in the same way. This is called *Shaping the Course*.

Taking the Departure. When just about to leave the land take the bearing of some known object, such as a lighthouse or headland, by the compass and estimate the distance by eye, or the bearing and distance of the object from the ship. This may be found by one of the processes already described. This is called Taking the Departure.

Log-slate. The opposite point to that on which the object bears is considered the first course, and the distance of the object as the first distance sailed from the place and is noted on the log-slate. This Log slate is a memorandum board or book properly ruled for the hours of the day, distance made by the log, courses steered by the compass and the direction of the wind, leeway, variation, and deviation, as well as remarks of all causes affecting the sailing of the ship.

Log-book. The other courses and distances made during the day being determined by the compass and the log are severally entered in the log-slate at the end of each hour, and afterwards copied into a book similarly ruled, called the *Log-book*.

It must be borne in mind that the standard compass is the compass from which all courses for the log-slate are taken. In steering, the course is taken from the standard compass and the man at the wheel given his course for the steering compass by a careful comparison. As the vessel proceeds on her course frequent comparisons should be made between these two compasses.

In a violent gale and heavy sea, when it would be dangerous to carry sail, it is usual to put the ship close to the wind with just sufficient sail to prevent the vessel from rolling too much. In this condition the vessel will come up and fall off, and the points to which her head comes up and falls off must be noted, and the middle point between the two taken as the course to enter in the log-slate.

If there should be a set and drift of a current it is to be entered as a course and distance, and treated the same as any course and distance.

Dead-reckoning. The process by which the position of the ship is found from the data given in the log-book is called Dead-reckoning. By means of this dead-reckoning the latitude and longitude are found, hence the position of the ship. It is usual to obtain the position at 8 A.M., 12 M. and 8 P.M. of each day, and more frequently when approaching land or danger.

The process by which this is accomplished is, first, correct the several courses in the log-book for the variation, deviation, and leeway opposite to each course. Construct a table in the Work-book, in which all data in navigation should be preserved during the entire voyage. In the first column of this table enter each true course, and in the second column the distance run on each course, found by summing up the knots and tenths sailed by the ship on each course.

Find in Table I the courses at the top or bottom of the page given in degrees, the difference of latitude and the departure corresponding to each course and distance, and place them in their respective columns; then the difference between the sums of the northings and southings will be the difference of latitude made good of the same name as the greater.

Seek in the same table until the difference of latitude and departure are found together in their respective columns; opposite to these in the distance column will be the distance made good.

At the top or bottom of the page, according as the departure is less or greater than the difference of latitude, will be found the course made good.

If the latitude of the object from which the departure was taken or the latitude of a former position be of the same name as the difference of latitude found, add them together; but if of different names take their difference; the sum or remainder will be the *latitude in* of the same name as the greater.

As departure is the lineal distance between two meridians measured upon a parallel of latitude, it is less than the difference of longitude, which is measured upon the equator; so to find the difference of longitude take the middle latitude between the two places which take as a course in Table I., and seek for the departure in the difference of latitude column; then will the corresponding distance be the difference of longitude of the same name as the departure. If the longitude of the previous

position be of the same name as the difference of longitude add them together, but if of different names take their difference; the sum or difference will be the *longitude in* of the same name as the greater.

The intersection of the latitude and longitude found on the chart will be the position of the ship, from which the bearing and distance of the port or other object can again be found. It is especially important to always find the bearing and distance of any supposed or real danger whenever the position of the ship is plotted

EXAMPLE.

When the ship was about to leave the land on July 15th, the departure was taken from Cape Henry light-house, which bore per compass NNW., distance 20 miles; afterwards sailed by the following log account:

Hours.	Knots.	Tenths.	Courses.	Wind.	Lееway.	Var.	Dev.	True Courses.	Remarks.
noon 1 2 8 4 5 6 7 8 P.M.	20 6 5 6 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	050050000	SSE. I SE. by E. SE. ESE. E. by N. "NE. Current	ENE. S. SSE.	1 pt. 2 pt. 1 pt. SW.	low	0 80 W. 8 40 E. 2 00 E. 4 80 E. 7 80 E. 8 00 E.	S. 83 00 E. S. 51 20 E. S. 51 20 E. S. 80 80 E. S. 28 00 E. N. 53 45 E. N. 53 45 E. N. 31 45 E. S. 45 00 W.	A current set the ship during the last 2 hours 1 1-2 m. an hour SW. as shown in chart. Mod. breeze, smooth see on, sail, etc.

LOG-BOOK OR SLATE-TABLE.

In this case the opposite point to the bearing of the lighthouse NNW. is SSE., which enter as the first course and the distance 20 miles as the first distance. The variation supposed to be found on the chart was 10° W., and from the deviation table for the course SSE. we find 00° 30′ W., which, applied to the left as they are both westerly, gives the true course S. 38° 00′ E.

Again, for the second course at 1 P.M. the log indicated the ship as making 5 miles the first hour and the compass course SE. by E. with the wind NE. or on the port tack, the left side; hence the leeway of one point is to the right. The variation

of 10 degrees is west or left, and the deviation from the table 3° 40′ is east or right; hence the true course is S. 51° 20′ E. in the last column, and so on with the other courses.

The drift of the current being one and a half miles per hour for the last two hours drove the ship 3 miles in the direction of the set SW. true, which enter as though the ship had sailed that the last course and distance.

Having now obtained the true courses sailed, enter them in the table of the working-book with the sum of the distances made on each course:

พก	RK	-T-4	RI	ъ.

Courses.	Distances.	DIFF. LA	TITUDE.	DEPARTURE.	
	Distances.	N.	s.	E.	w.
8. 83 00 E. 8. 51 20 E. 8. 80 30 E. 8. 82 00 E. 8. 28 00 E. 8. 45 E. N. 31 45 E. 8. 45 00 W.	20.0 11.5 6.0 5.5 15.0 5.0 8.0	8.8 4.2	16.8 7.2 5.2 4.8	10.9 8.9 8.0 2.5 12.1 2.6	2.1
		13.0	36.1 13.0	40.0 2.1	2.1
		Diff. Lat.	23.1	87.9	Departu

Course made good S. 58° E. and distance made good 44 miles.

Lat. Cape Henry Light 36° 55′ 05″ N. Long. 76° 00′ 02″ W. Difference of latitude 23′ 06″ S. Diff. Long. 47′ 00″ E.

Latitude in 36° 31′ 59″ N. Long. in 75° 13′ 02″ W.

Sum of latitudes . . . 73° 27′ 04"

Middle latitude . . 36° 48′ 30″ or 36¾″.

The first course, 33°, is found at the top of the page of Table I, and opposite to the distance of 20 the Lat. column gives 16.8 and the Dep. column gives 10.9, which place in their appropriate column in the work-table; the difference latitude under S. and the departure under E. as the ship has sailed south and

east. Do the same way with each course to the nearest degree is sufficient.

After adding up the different columns it will be seen there were more southings than northings, and their difference will give 23.1 S. as the difference of latitude made good. There are more eastings than westings, and their difference will give 37.9 E., the departure made good.

In Table I the place where these come nearest in their respective columns is opposite 44 in the distance column, which is the distance made good.

The departure being greater than the difference of latitude, the course made good is found at the bottom of the page, S. 58° E.

The latitude of Cape Henry being north and the difference of latitude made good being south we take their difference and get the latitude in 36° 31′ 59″ N., the name of the greater.

With the middle latitude 36½ as a course in Table I, the departure made good is found in the Lat. column opposite the distance 47, which is the difference of longitude of the same name as the departure, which is east, and as the longitude of Cape Henry is west we take their difference to find the longitude in 75° 13′ 02″ W., the name of the greater.

From this new position of the ship the bearing and distance of the designated place are again found, and the new course followed as nearly as possible.

From 8 P.M., the time of the last position, the ship sailed on a course by compass ESE., with the wind free, 100 miles per log until 8 A.M. the following morning; the chart showing 2 points easterly variation and a constant drift of 2 miles per hour in a true SW. direction. Find the position again. In this case there would not be any leeway.

LOG-TABLE.

Hours.	Knots.	Courses.	Wind.	Lee.	Var.	Dev.	True courses.
12	100 24	ESE. Set of	NW. the cur	0 rent	2 pts. E. SW. true.	4° 30′ E.	SE. 14 S. SW.

The variation 2 points being easterly and the deviation from the table 4° 30′ E. or nearly ½ point easterly, both are applied to the right to get the true course.

WORK-TABLE.

Courses.	Distance.	DIFF. LA	TITUDE.	DEPARTURE.	
Courses.	Distance.	N.	s.	E.	w.
S. 39 22 30 E. S. 45 00 00 W.	100 24		77.8 17.0	63.4	17.0
			94.3	63.4 17.0	17.0
		Diff. Lat.	94.8	46 4 I	Departur

Course made good S. 26° E., and 105 miles the distance made good.

In this case, the nearest the difference of latitude and departure came together in their appropriate columns in Table I. was opposite to 105, the distance made good. As the departure was less than the difference of latitude the course S. 26° E. or SSE. ½ E. was found on top of the page as the course made good.

With this middle, latitude 35%, enter Table I, and find departure in the Lat. column, and opposite to it in the distance column is 57 miles, the difference of longitude of the same name as the departure, which is east.

At noon of that day the ship was found by the log to have sailed 30 miles NE. by E. close to the wind on the starboard tack or right hand, making two points leeway. Variation by the chart 7° 30′ W.

From the deviation table the deviation on a NE. by E. course is 8° 10′ E. The leeway will be to the left, beginned by Google

Compass course NE Deviation E				56° 15′ 00″ E. 8′ 10″ to the right.
Magnetic course N. Variation W				. 64° 15′ 00″ E
True course N Or nearly N. 57° E.	•		•	. 56° 45′ 00″ E.

WORK-TABLE.

Courses.	Distance.	Diff. 1	LATITUDE.	DEPARTURE.	
	Distance.	N.	S.	E.	w.
N. 57 E.	80	16.3		25.2	
		16.8		25.2	
		16.3	Diff. Lat.	25.2	Departure.

Course made good N. 57° E., and 30 miles the distance made

Lat. left Diff. Lat.	34 °		41" 18"	N.
Lat. in Sum of Lats. Mid. Lat.		11'		N.

With the middle latitude 85 and the departure 25.2 in the Lat. column, the difference of longitude is found to be:
Diff. longitude 31'00" E.
Longitude left 74° 16'02" W.

Longitude in 73° 45′ 02″ W.

From this position the ship sailed from day to day on the following courses and distances, taken from the log-book and stated in the following table:

LOG-BOOK.

Courses.	Distances.	Wind.	Leeway in Points.	Var.	Dev.	True courses.
ENE. E by N. E by S. E. SE. ENE.		N. NNE. " Orift	11/4 2 13/4 2 true cou	15 20 W. 10 10 W. 500 E. 700 E. 700 E.	7 20 E. 7 30 E. 5 50 E. 6 40 E. 2 00 E.	o / N. 78 38 45 E. S. 81 35 00 E. S. 48 14 00 E. S. 53 50 00 E. S. 36 00 00 E. N. 67 30 00 E.

REMARKS.—The ship drifted during the time in a gale by wind and sea 80 miles SE. by compass. By current marked in chart ENE. 50 miles,

In the second course it will be seen that after variation and deviation and leeway are applied, the course is greater than 90 degrees, or we have gone through E. from the north and have come nearer S. than N.; therefore we subtract from 180 degrees, which gives the true course S. 81° 35′ E. from the South.

WORK-TABLE.

Courses.	Distances.	DIFF. LA	TITUDE.	DEPARTURE.	
	Distances.	N.	8.	E.	w.
N. 73 34 E. S. 81 35 E. S. 48 14 E. S. 53 50 E. S. 36 00 E. N. 67 30 E.	30 40 80 60 30	8.6 19.1 27.7	6.0 53.3 85.3 24.3	28.7 89.5 59.7 48.5 17.6 46.2 240.2	
		Diff. Lat.	91.2	240.2	Departure

Course made good S. 69° E. and 257 miles made good.

With the first course enter Table I with the course 73. On page with 78 at the bottom and opposite to 30 in the disstance column will be found in the Lat. column 8.8, and on page with 74 at the bottom and opposite to 30 in the distance column will be found in the Lat. column 8.3, making a difference of .5 for one degree in the course: hence for half a degree it will be one half of .5, or .2, to be subtracted from 8.8 in the first case, which will give 8.6 for the difference of latitude for the first course, which place in the column N. as northings. As there is so little difference between the departure for 73 and 74, that for either course may be used as the departure in its appropriate column under E., and so on in each course.

Lat. left 85° 13′ 59″ N.
Diff. Lat. 1° 11′ 12″ S.

Lat. in 84° 02′ 42″ N.
Sum of Lats. 69° 16′ 46″
Mid. Lat. 84° 88′ 23″

With middle latitude 34½ and the departure 240.2 in the Lat. column, the difference of longitude is found to be 291.5 in the distance column; divide by 60 and we get:

Diff. longitude 4° 51′ 30″ E. Longitude left 73° 45′ 02″ W. Longitude in . 68° 53′ 32″ W. Continue in this way until the port is reached.

If it is not convenient to find the course and distance on the chart with the parallel rulers and dividers, it may be done in the following manner. Suppose, for instance, it is desired to know the compass bearing and distance from the last position back to Cape Henry.

Lat. of Cape Henry 36° 55′ 05″ N. Lat. of last position 34° 02′ 47″ N.

Diff. Latitude 2° 52′ 18″ 60 120 52 172.8

Long. of Cape Henry 76° 00′ 02″ W. Long. last place 68° 53′ 32″ W.

Diff. Longitude 7° 06′ 30″ 60 426.5

Sum of Latitudes 70° 57′ 52′′ Middle Latitude 35° 28′ 56′′ or 85‡

The difference of longitude is too great for the distance column in the table, so divide it by 2 for convenience, and with the half of the longitude, 213.2, enter Table I, and opposite to it in the distance column for 35 and 36 will be found 174.5 and 172 3 in the latitude column; the middle latitude being nearly 35½, take the mean of these, 173.4, for the departure, which multiplied by 2 gives 346.8 for the whole departure. The whole departure and difference of latitude are too large for the table, so divide by any convenient number, say 10, which gives 17.2 diff. latitude and 34.7 departure; with these seek in Table I till they nearly agree on a course S. 63° W. and a distance of 39. Multiply this distance by 10, and we get 390 miles as the whole distance.

Hence Cape Henry bears true S. 63° W., distance 390 miles; and to get the compass bearing or course, variation and deviation must be applied. Let variation be 16° 20′ W.

True course S. 63° 00' W.

Variation W. 16° 20' apply to the right.

Magnetic course S. 79° 20' W.

Deviation W. 8° 00′ to the nearest point to the right.

Compass course S. 87° 20' W.

Or the ship will have to steer S. 87° 20' W. 890 miles to return to Cape Henry.

Ship's Track. It is customary, whenever the position of the ship is plotted, to draw a line on the chart from that position to the former one, and the lines so drawn from day to day will be the ship's track—a distinction from the *traverse* which the ship makes in her zigzag course sailing from one position to another against a head wind.

EXAMPLES.

I. Required the compass course and distance from latitude 51° 25′ N. and longitude 9° 29′ W., to latitude 49° 16′ N. and longitude 9° 29′ W. The variation is 19° 20′ W. and deviation is 3° 16′ E.

Ans. Compass course S. 16° 04′ W. Distance 129 miles.

II. A ship sails from latitude 44° 30′ N. 290 miles, when she finds her departure is 161.1. What is the true course she has sailed, the difference of latitude, and latitude in?

Ans. Course NW. by N. Diff. latitude 241.1 and Latitude in 48° 31' 06" N.

III. What is the position of the ship after sailing on the following courses (true) and distances: NNE. 40 miles; E. by S. 60 miles; SE. 70 miles; and SW. 48 miles?

Ans. Diff. lat. 58.2; dep. 89.7; course made good S. 57° 01' E.; distance 106.9.

IV. A rock was sighted in latitude 39° 40′ S., longitude 87° 15′ E., bearing NNE., distant 15 miles. Afterwards sailed: E. by S., 37 miles; ENE., 44 miles; N. ½ W., 51 miles; and ESE., 29 miles. What is the position of the ship? (The bearings and courses are true.)

Ans. Course made good N. 70° E.; distance 102 miles. Latitude in 39° 05' S.; longitude in 89° 17' E.

V. From latitude 18° 35′ S., longitude 123° 23′ E., the ship sails 225 miles SW. ½ W. by compass. What is her position? The variation is 1½ point E. and deviation is 6° 35′ W.

Ans. Latitude in 20° 24′ 06″ S.; longitude in 119° 55′ 00″ E.

VI. A danger bears by compass S. 34 E. 29 miles, variation is one point west, and deviation is 1° 50' E. What is the true bearing of the danger? The latitude of the danger is 00° 52' N. and longitude is 2° 40' E.

Ans. N. 43° 25' W., 29 miles.

CHAPTER IV.

By Observations.

The method of finding the ship's position by dead-reckoning must of course be liable to many errors, arising from the great difficulty in steering a steady course, different rates of sailing between the times of heaving the log, incorrect allowance for leeway and variation, and more frequently from the effects of the drift of the sea and unknown currents; hence it becomes necessary to determine the position by celestial observations when the opportunity offers.

The Zenith. The heavens appear to form the upper half of a hollow sphere, and this celestial surface may be conceived to be divided by imaginary circles that are made to correspond with those of the earth; thus if the axis of the earth were extended it would pass through the north and south poles of the heavens. The celestial equator is a circle in the heavens corresponding with the equator of the earth, and the celestial meridians correspond also with those of the earth; hence it will be seen that if we determine the point immediately over head, called *The Zenith*, it would be the same as finding the position of the ship on the earth. The method for finding this position differs from that of dead-reckoning in the determination of the position directly from observations of the heavenly bodies and not by a reference to some other geographical spot.

The instruments used to obtain the data necessary for the determination of the position by observations are the Chronometer and Sextant.

The Chronometer is a superior kind of watch, so constructed that its daily gain or loss by variation of temperature

is reduced to a minimum. The machinery is of such delicate construction that the greatest possible care must be taken of it both at sea and in harbor. It should never be moved from its place on board, but kept as near the same temperature as possible, and is defended from violent shocks by the case being lined with soft wool and preserved in a horizontal position by being hung on gimbals. It should be wound up every day at the same hour and the key turned steadily through each turn.

Error and Rate. The chronometers are intended to keep the mean time of Greenwich, but as none of these are perfect the *Error* should be ascertained before going to sea and also its *Daily Rate*.

The error is said to be fast or slow as the chronometer is fast or slow of Greenwich mean time. The daily rate is the change in its error in twenty-four hours, and if the instrument is going too fast the rate is said to be gaining: if too slow, losing.

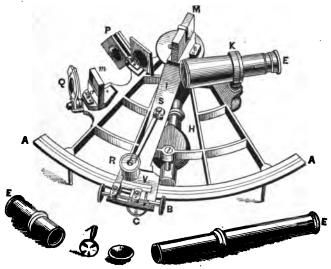
A chronometer is best rated at an observatory; but at all large sea-ports an electrical ball is dropped at a certain hour every day from a point at which it can be seen from all over the harbor. By a comparison with this the error can be found, and if taken in successive days the rate. In the absence of this some good clock-maker can be found to compare your chronometer with one of known rate and error.

After going to sea the rate is almost sure to change some; and it is not unwise, on arriving in port, to compare with the chronometers of other ships, should there be no time-ball. The difference between the two rates being divided by the interval elapsed will be what is called the sea rate.

The Sextant is an instrument used to measure the altitude of a heavenly body above the horizon, or the angular distance between objects. The description, names, and uses of the different parts may be best learned from the instrument itself, which may be found in almost any optician's store.

From the figure the names of the different parts may be seen. AA is the limb; I, the index bar; M, the index-glass, which stands upon and moves with the index-bar; m is the horizon-glass fixed to the frame, and which is only silvered on half the surface; P and Q are the shade-glasses to modify the brightness of the sun; E is the sight-tube or telescope carried by the collar K; H is the magnifying glass to assist in reading the

scale, is attached to an arm which moves upon a pivot S; B is the tangent-screw to give a small motion to the index-bar



THE SEXTANT.

when the clamp-screw is tight. C is the clamping-screw, and V is the vernier carried by the index-bar.

The limb is graduated to 120° from the zero point and to a few degrees on the opposite side of the zero point. The degrees are divided at every ten or twenty minutes, and these are subdivided by the vernier to ten or twenty seconds, thus enabling the angles to be read by estimating to five or ten seconds.

The Adjustments are four in number. I. See if the index-glass is perpendicular to the plane of the instrument by placing the index near the middle of the limb, and whilst looking in the index-glass see if the reflected limb in the glass forms an unbroken line with the limb itself; if not, make it so by means of the screws at the back of the glass.

II. See if the horizon-glass is perpendicular to the plane of the instrument, by looking through the sight-tube and the horizon-glass at the horizon and holding the instrument in a vertical position, move the index till the reflection of the horizon in the silvered part of the glass forms an unbroken line with the one seen direct, fasten the index by the clamp-screw and incline the instrument to the right or left to see whether the true and reflected horizons continue to form an unbroken line; if not, they can be made so by means of the screw at the back of the instrument.

III. See that the axis of the telescope, when screwed into the collar, is parallel to the plane of the instrument by placing two of the wires of the telescope parallel to the plane of the instrument, and then measure the distance between two objects more than 90° apart, and bring them in contact on the wire nearest the instrument; by moving the sextant slightly the two objects may be brought to the other wire; if they still be in contact the adjustment is correct, but if they separate or top one over the other, the adjustment is made by means of the screws in the collar of the telescope.

IV. See that the horizon-glass is parallel to the index glass when the zero of the vernier is opposite to zero on the limb by looking at the horizon and holding the instrument in a vertical position. Place the two zeros together and look through the horizon glass at the horizon, holding the instrument vertical. If the true horizon through the clear part of the glass appear in a straight line with the reflected in the silvered part the two glasses are parallel; if not they are made so by turning the lower screw at the back of the glass.

Index Error. If this last adjustment has not been correctly made the instrument can be used as well, but the reading will want correction for every angle measured; this correction is called the *Index Error*. This error is found by making the horizons form an unbroken line whilst holding the instrument in a vertical position, and the distance from zero on the limb to the zero on the vernier will be the index error, to be subtracted from the angles measured if zero on the vernier is to the left of zero on the limb, otherwise add. A more accurate way is by measuring the diameter of the sun on both sides of zero. If both measurements read alike there will be no index error; if they are unlike, half their difference will be the index error, to be subtracted if the measurement taken on the left of zero is larger; otherwise, to be added.

To Take an Altitude. When taking an altitude of the sun

it is customary to bring the sun's lower limb in contact with the horizon, but if the lower limb is obscured the upper limb can be used. As no level or plumb-line can be used in taking the altitude the sextant should be held as nearly perpendicular as possible, and when the reflected image is brought down to the horizon by moving the index by hand clamp it there, and while sweeping the horizon the image will appear to form a curve; use the tangent-screw till the limb just touches the horizon at the lowest part of the curve.

The altitude when thus taken on the meridian enables us to find the latitude, and when not taken on the meridian furnishes the means of finding the time of the ship and thence the longitude. This altitude above the sea horizon is called the Apparent Altitude and must be corrected to reduce it to the True Altitude. These corrections are: dip, index error, refraction, parallax, and semi-diameter.

The Dip is the depression of the sea horizon below the level of the eye, and will depend upon the elevation of the eye above the level of the sea; should be subtracted from the apparent altitude because it makes the altitude appear more than it really is. The dip is given in Table II.

Refraction is due to the earth's atmosphere, which bends the rays of light passing through it into a position more nearly vertical and thus enabling us to see a heavenly body when really below the horizon. The effect then of refraction is to make the heavenly body appear higher than it really is; hence the correction for refraction must be substracted from the apparent altitude. This correction depends upon the altitude of the heavenly body being most when near the horizon and nothing when in the zenith. The refraction is given in Table II.

Parallax is a correction to be added to the apparent altitude to make it what it would have been if observed at the centre of the earth. The parallax decreases with the altitude, being most when in the horizon and nothing when in the zenith. Parallax is given in Table II.

Semi-diameter is the correction to be applied to obtain the altitude of the centre of the object. If the lower limb of the sun was used it should be added to the apparent altitude and subtracted when the upper limb is used. The semi-diameter of the sun may be taken at 16'.

CHAPTER V.

TO FIND THE LATITUDE.

Astronomical Date. In finding certain data from the tables the astronomical date is used, which begins 12 hours behind the *civil date*, and is counted from noon to noon, or 24 hours, whereas the civil date commences at midnight and is divided into two parts of 12 hours. Suppose the day is what is ordinarily called the 4th July, and it wants 2 hours to noon, it would be 10 Am. of the 4th July civil date, but astronomically it is July 3d, 22 hours.

To Find the Latitude. The latitude of a place, being its distance from the equator measured on the meridian, must correspond with the distance from the celestial equator to the As the zenith is right overhead, it is 90 degrees from the horizon; hence, if the celestial equator were visible in the heavens, it would only be necessary to take its altitude, which subtracted from 90 would give the latitude. As we cannot see the equator, some heavenly body is taken whose distance from the equator is known. In case of the sun, it appears to move during the year in a path inclined to the equator at an angle of 23 degrees and 28 minutes, crossing the equator twice during the year, once in March and again in September, reaching its farthest north in June and farthest south in December. distance at any time from the equator measured on a meridian is called its Declination, north when it is north of the equator. and south when south of it.

The declination is given in Table III for each month when the sun is on the meridian of Greenwich; and as the declination is constantly changing, the difference for one hour is also given in the table.

To find the declination at any time, obtain the astronomical date, and take from Table III the declination opposite the day of the month; now multiply the difference for one hour by the longitude in time, which is one hour for every 15 degrees, and, if the declination be increasing, add in west but subtract in east longitude. If the declination be decreasing, subtract in west but add in east longitude.

The Meridian Altitude of the sun is the greatest it will acquire during the day, and as it crosses the meridian it is necessary to commence taking its altitude a little before, and keep its image in contact with the horizon till it begins to fall. Correct this altitude to find the true altitude according to the principles previously explained, and to avoid any mistakes it would be best to prefix the signs of addition and subtraction, + and -, to the known corrections and those that are found in Table II. These corrections may be written in a separate form, and applied one to the other according to their several signs for a whole correction to be added or subtracted as the sign implies.

Meridian Zenith Distance. As the zenith is 90 degrees from the horizon, subtracting this true meridian altitude from 90 will give the distance of the sun from the zenith while on the meridian, or the meridian zenith distance. This meridian distance mark north when the sun bears south, or south when it bears north.

Now with the meridian zenith distance given and the declination known, the latitude is found by adding them together if they are of the same name, or taking their difference if of different names. The latitude will be of the same name as the greater.

EXAMPLES.

At sea, June 21, 1887, in longitude 60° W., the observed altitude of the sun's lower limb was 40° 04′; sun bearing south; index correction 3′ 00′ (add); height of the eye 20 feet. Find the latitude.

In Table III, with the year at the top and the day of the month at the left of the page, we find the declination under June to be 23° 27' N., and the corresponding difference for one hour to be zero. This difference for one hour multiplied by four hours, the longitude (60 divided by 15), gives for the correction to the declination nothing; hence the true declination is 23° 27' 00" N.

The observed altitude, 40° 04′, having been corrected as before explained, the true altitude is found to be 40° 17′ 85″, which subtracted from 90 gives the meridian zenith distance 49° 42′ 25″, which is marked north as the sun bore south.

The declination and meridian zenith distance having the

same name, we take their sum and find the latitude to be 72° 09' 25" N.

For the sake of convenience it is always best to have a particular form for all problems in which the data are written and the result obtained; besides it tends to preserve neatness in the navigation book, and facilitates an easy means of comparison with other results.

The form in this case should be:

At sea June 1, 1886, in longitude 44° 40′ W., the observed altitude of the sun's lower limb was 72° 14′ 10″; sun bearing south; index error + 3′ 45″; height of the eye 22 feet. Find the latitude.

Longitude 44° 40′ W. is 3 hrs. 14 m. 40 s. W., or 3 hrs. nearly.

At sea June 25, 1886, in longitude 59° 15' E. (3 h. 57 min.), the observed altitude of the sun's upper limb was 60° 23' 14"; sun bearing north; index error -2' 21"; height of the eye 30 feet. Find the latitude.

Obs. Alt. 60° 23′ 14″	S. D 16' 00"
Corr. $-24 12$	I. C 2 21
	Ref. — 33
True Alt. 59 59 02	Dip - 5 22
90 00 00	Par. + 4
M. Z. D. 30 00 58 S.	
True Dec. 23 24 15.8 N.	Corr. — 24 12
Latitude 6 86 42.2 S.	
Dec. 23° 24′ 00″ N.	Hr. Diff. 4"
Corr. 15.8	Long. 3.95 hrs.
True Dec. 23 24 15.8 N.	Corr. + 15".80

At sea October 3, 1887, in longitude 67° 30′ W., the observed meridian altitude of the sun's lower limb was 40° 23′ 50″; sun bearing N.; index correction + 1′ 30″; height of the eye 18 feet. Find the latitude.

Obs. Alt. 40° 23′ 50″	8. D. $+16'$ 00'
Corr. $+12\ 20$	I. $C. + 1 80$
	Ref 1 07
True Alt. 40 86 10	Dip - 4 11
90 00 00	Par. + 08
M. Z. D. 49 23 50 S.	Corr. $+12 20$
True Dec. 4 00 21 S.	
Latitude 53 24 11 S.	
Dec. 3° 56′ 00′′ S.	Hr. Diff. 58"
Corr. + 4 21	Long. 4.5 hrs.
True Dec. 4 00 21 S.	290
	232
	901//0
	261''0
•	Corr. + 4' 21"

At sea Feb. 21, 1888, in longitude 45° W. the observed meridian altitude of the sun's lower limb was, 55° 43° 10"; sun

bearing S.; index correction -2' 10"; height of the eye 19 feet. Find the latitude.

Obs. Alt. 55° 43′ 10″ Corr. + 8 59	S. D. + 16' 00" I. C 2 10 Ref 40
True Alt. 55 52 09 90 00 00	Dip - 4 16 Par. + 5
90 00 00 M. Z. D. 34 07 51 N. True Dec. 10 35 18 S.	Corr. + 8 59
Latitude 23 32 33 N. Dec. 10° 38′ 00″ S. Corr. — 2 42	Hr. Diff. 54" Long. 3 hrs.
True Dec. 10 35 18 S.	162" Corr 2' 42''

At sea Jan. 23, 1888, in longitude 4 hours and 12 minutes E., the observed meridian altitude of the sun's lower limb was 77° 15′ 30″; sun bearing N.; index correction -3′ 10″; height of the eye 19 feet. Find the latitude.

8. D. + 16' 00"
I. C 3 10
Ref 0 13
Dip - 4 16
Par. + 0 02
Corr. + 8 23
•
Hr. Diff. 35"
Long. 4.2 hrs.
70
170
147".0
Corr. + 2' 27"

At sea April 20, 1888, in longitude about 40° 15′ W ; the observed meridian altitude of the sun's lower limb was 63°

01' 30"; sun bearing N.; index correction -3' 10''; height of the eye 19 feet. Find the latitude.

Obs. Alt. 63° 01′ 30′′	8. D. + 16' 00"
Corr. + 8 09	I. C 3 10
	Ref 0 29
True Alt. 63 09 39	Dip - 4 16
90 00 00	Par. + 0 04
M. Z. D. 26 50 21 S. True Dec. 11 48 18 N.	Corr. + 8 09
Latitude 15 02 08 S. Dec. 11° 46′ 00″ N. Corr. + 2 18	Hr. Diff. 51" Long. 2.7 hrs.
True Dec. 11 48 18 N.	187".7
•	Corr. $+2'$ 17".7

CHAPTER VI.

To FIND THE LONGITUDE.

THE earth in its revolution about its axes from west to east once in twenty-four hours causes the sun to pass over 360 degrees in that time, which is equal to 15 degrees per hour. As longitude is measured on the equator in degrees, minutes, and seconds, we have at once the connection between it and time, or 15° is equivalent to one hour, 15' to one minute, and 15" to one second. As the motion of the sun is from east to west, apparently, it follows that all places east of us will have the sun on their meridian before it comes to ours, therefore it will be later there than at our place; and all places to the westward of us will have the sun on their meridian after it. has passed ours, therefore it will be earlier there than at our place. Now, it has been stated, the first meridian, from which all longitudes are reckoned, is the one passing over Greenwich; hence the difference of time between Greenwich and any place is the longitude of that place. To find the longitude, then, of any place would be to find the time of the place and apply it to the Greenwich time.

As the sun, which is supposed to mark the days and hours by its passage in the heavens, is irregular in its motion, it is necessary to take into consideration, besides the two modes of counting dates, two kinds of time—apparent time and mean time.

Apparent Time is that shown by the sun, estimating the apparent noon the moment the sun passes the meridian, and if it were possible to determine that moment with accuracy at sea, we could then obtain the apparent time at ship; but the length of the days would vary as much as half an hour during the year if they were determined by the sun's passage over the meridian.

Mean Time. As it is impossible to construct watches or chronometers to show this apparent time, we make use of what is called mean time, which makes the days of uniform length throughout the year, and is therefore sometimes in advance of the time shown by the sun and sometimes behind it. This is the time shown by all well-regulated watches and chronometers.

Equation of Time. There is sometimes a difference of a quarter of an hour between this apparent and mean time. This difference is called the equation of time, and is given in Table IV at Greenwich noon for each day of the month, and must be applied to the apparent time according to the instructions given at the top of the column, in order to obtain the mean time. This equation of time found in Table IV must be corrected for the Greenwich time. In Table IVa, under the daily variation at the top and opposite the hour of Greenwich at the side, the number of seconds will be found to apply to the equation of time found in Table IV to obtain the correct equation of time.

The method of obtaining the apparent time at sea, and thence the mean time, is by observing the altitude of the sun, taken either in the forenoon or afternoon when it is rising or falling fastest, or when bearing nearly east or west, noting the time by watch at the same instant.

The preliminary steps in solving this problem will consist in finding the following data: the correct Greenwich date expressed astronomically, the true altitude of the sun, latitude of the place, and the polar distance of the sun.

The Greenwich date is found by comparing the watch with

the chronometer, which will give the time shown by the chronometer when the observation was taken; apply the error and rate of the chronometer and the Greenwich mean time is obtained.

The true altitude is found by correcting the observed altitude for semi-diameter, index correction, refraction, dip, and parallax in the same manner as explained for correcting the meridian altitude.

The latitude of the place is found by dead-reckoning from the last position to the time of observing the altitude. It is sometimes the practice to observe an altitude in the morning for time and delay working till noon, when the meridian altitude gives the latitude which is worked back by dead-reckoning to the time of taking the observation.

The polar distance is the distance of the sun from the north pole when the observation is taken in north latitude, and its distance from the south pole when taken in south latitude.

Take from Table III the declination corresponding to the Greenwich date, and multiply the difference for one hour by the Greenwich time, which apply as before explained to obtain the true declination.

As the declination is the distance of the sun from the equator and the equator is 90° from the poles, it follows that the declination subtracted from 90 if of the same name as the latitude, or added if of a contrary name, will give the polar distance.

Having thus found the correct altitude, latitude, and polar distance, the apparent time of observation may be found by the following method and the use of Table V. In this table, if the sine or cosine sought is marked at the top of the page, the title, hour A.M. or P.M., is also found at the top, and the contrary if the sine or cosine is marked at the bottom.

Add together the altitude, latitude, and polar distance and take half their sum; from this half sum subtract the altitude and note the remainder. Take from Table V the secant of the latitude, the cosecant of the polar distance (rejecting 10 in the index), the cosine of the half sum, and the sine of the remainder; add these together and take half the sum, which seek for in the column of sines, and opposite to it will be the corresponding apparent time.

Take from Table IV the equation of time corresponding to the Greenwich date, corrected for Greenwich time by Table IVa, and apply it to this apparent time according to the directions at the top of the column, and we shall obtain the mean time of the observation. Take the difference between this and the Greenwich time, and the result is the longitude cast when the Greenwich time is the least, and west if the Greenwich time is greater than the time of the place.

EXAMPLE.

On Nov. 9, 1889, in the forenoon, the observed altitude of the sun's lower limb was $22^{\circ} 29' 20''$; height of the eye 17 feet; index correction +2' 45''; watch time of observation $8^{\rm h} 51^{\rm m} 57^{\rm s}$ A.M.; slow of chronometer time $4^{\rm h} 54^{\rm m} 15^{\rm s}$; chronometer correction $-2^{\rm m} 12^{\rm s}$; with latitude by dead-reckoning 35° North. Find the longitude.

PREPARATION OF DATA.

		22.20			DAIM.	
W. Time 8 th	51 ^m	57•	A.M.	,	Obs. Alt. 2	32° -29′ 20′′
C.—W. 4	54 1	15			S. D.	+ 16 00
		_			I. C.	+ 245
C. Time 1	46	12	P.M.		Ref.	- 2 20
C. Corr	2	12			Dip	— 4 02
					Par.	+ 8
G. M. T. 1	44 (00	P.M.		True Alt. 2	2 41 51
Dec.	17°	00	00"	S.	D	iff. 1⁴ 43″
Corr.	+	- 1	18		G. M.	T. 1.7
True Dec.	17	01	13	s.	Co	orr. 78.1
	90	00	00		01	+ 1′ 18″
Pol. Dist.	107	01	13			•
		8	olu	TIO	N.	
Alt.	22°	41′	51"			
Lat.	35	00	00		sec	0.08664
Pol. Dist.	107	01	18		cosec	0.01945
Sum	164	43	04			
Half Sum	82	21	32		cos	9.12374
Alt.	22	41	51			
Rem.	59	39	41		2)	9.93604 19.16587 9.58298
					pill	0.00000 ∪

Local App. Time 8h 59m 58 A.M. Equation of Time - 16

Local M. Time 8 43 57 A.M.

Gr. M. Time 1 44 00 P.M.

Diff. Time 5 00 03

Longitude 75° 00′ 45″ W.

Equation of Time, Table IV, - 16m 02º Daily Variation 6ª Correction, Table IVa, -1

Equation of Time - 16 01.

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About 8 A.M. April 3, 1888, in latitude 20° 45' S. and east longitude, the observed altitude of the sun's lower limb was 24° 37′ 10"; index correction + 2' 20"; height of the eye 19 feet: watch time of observation 7h 57m 07.5; slow of chronometer time 5^h 57^m 24^e; chronometer correction - 3^m 38^e. Find the longitude.

PREPARATION OF DATA.

W. Time 7b 57m 07.5	Obs. Alt. 24° 37′ 10″
C.—W. 5 57 24	S. D. + 16 00
	I. C. + 2 20
C. Time 1 54 31.5	Ref. — 2 06
C. Corr. — 3 38	Dip - 4 16
	Par. + 0 08
G. M. T. 8d 13 50 58.5	True Alt. 24 49 16
Dec. 5° 35′ 00″	N. Hr. Diff. 57"
Corr. $+1306$	G. M. T. 13.8 hrs.
True Dec. 5 48 06	N 786.6
90 00 00	Corr. + 18' 06".6
Pol. Dist. 95 48 06	
80	LUTION.
Alt. 24° 49′ 1	6''
Lat. 20 45 0	0 sec 0.02913
Pol. Dist. 95 48 0	6 cosec 0.00223

Sum 141 22 22

Half Sum 70 Alt. 24	0 41 11 4 49 16	cos	9.51948
Rem. 45	5 51 55	sin	9.85594
		2)	1 9.4 0678
Local App. Time 7h 5	7 ^т 17° а.м.	sin ¯	9.70339
Equation of Time +	3 00		
Local M. Time 8 0	0 17 A.M.		
Gr. M. Time 1 5	0 53.5 а.м.		
Diff. Time 6 0	9 23.5		
Longitude 92° 2			

Equation of Time, Table IV, + 3^m 10ⁿ
Daily Variation 18ⁿ.

Correction, Table IVa, - 10

Equation of Time + 3 00

About 8 a.m. Feb. 21, 1888, in latitude 24° 10′ N. and west longitude, the observed altitude of the sun's lower limb was 21° 44′ 10″; index correction -2′ 10″; height of the eye 19 feet; watch time of observation 8^h 01^m 12^s; slow of chronometer time 3^h 04^m 07^s; chronometer correction + 7^m 35^s. Find the longitude.

PREPARATION OF DATA.

W. Time 8h 01m 12s A.M.	Obs. Alt. 21° 44′ 10″
C.—W. 3 04 07	S. D. + 16 00
C. W. 0 04 01	I. C. — 2 10
C. Time 11 05 19 A.M.	$\mathbf{Ref.} \; - \; 2 \; 25$
C. Corr. + 7 85	Dip - 4 16
	Par. + 0.08
G. M. T. 22d 23 12 54	
or	True Alt. 21 51 27
21st — 0h.79	
Dec. 10° 38′ 00″ S.	Hr. Diff. 54"
Corr. $+43$	G. M. T. -79
True Dec. 10 38 43 S.	Corr. + 42.66
90 00 00	
	Digitized by Google
Pol. Dist. 100 38 43	Digitized by GOOGTC

SOLUTION.

Alt.	21	° 51	27''		
Lat.	24	10	00	sec	0.03983
Pol. Dist.	100	38	43	cosec	0.00754
Sum	146	40	10		
Half Sum	73	20	05	cos	9.45754
Alt.	21	51	27		
Rem.	51	28	38,	sin	9.89340
•				2)	19.39881
Local App. Time 7 Equation of Time				t. sin	9.69915
			_		

Local M. Time 8 13 46 A.M. Gr. M. Time 11 12 54 A.M.

Diff. Time 2 59 08 Longitude 44° 47′ 00″ W.

Equation of Time, Table IV, + 18^m 53ⁿ
Daily Variation 0ⁿ.
Correction, Table IVa, 0

Equation of Time + 13 53

On April 3, 1888, in the forenoon, in latitude 29° 42′ 30″ S. and east longitude, the observed altitude of the sun's lower limb was 22° 41′ 30″; index correction — 2′ 30″; height of the eye 24 feet; watch time of observation 8h 06m 20•.5; slow of chronometer time 8h 08m 14•; chronometer correction — 6m 19. Find the longitude.

PREPARATION OF DATA.

W. Time	8h 06m	20.5 а.м.	Obs. Alt. 22° 41′ 30″
c w.	8 08	14	S. D. + 16 00
			I. C 2 30
C. Time	4 14	34 .5	Ref 2 19
C. Corr.	- 6	19	Dip - 4 48
			Par. + 08
G. M. T. 2d	16 08	15.5	·
or			True Alt. 22 48 01
$3d - 7^{h}.86$.			Digitized by GOOSIC

Dec. 5° 85′ 00″ N. Corr 7 28	Hr. Diff. 57" G. M. T. — 7.86
True Dec. 5 27 32 N. 90 00 00	Corr. 448.02 or - 7' 28"
Pol. Dist. 95 27 32	
SOLUTIO	on.
Alt. 22° 48′ 01″	
Lat. 29 42 30	sec 0.06120
Pol. Dist. 95 27 32	cosec 0.00198
Sum 147 58 08	
Half Sum 73 59 01	cos 9.44077
Alt. 22 48 01	
Rem. 51 11 00	$ \begin{array}{c} sin & \underline{9.89162} \\ 2)19.39557 \end{array} $
Local App. Time 8h 00m 43 A.M.	$\sin \overline{9.69778}$
Equation Time $+3$ 15	
Local M. Time 8 03 58 A.M.	
Gr. M. Time 4 08 15.5 A.M	:
Diff. Time 3 55 42.5 Longitude 58° 55′ 87″ E.	
Equation of T	ime, Table IV, 🕂 3ª 1

Equation of Time, Table IV, + 3^m 10^s
Daily Variation 18^s.

Correction Table IVa, + 5

Equation of Time + 3^s 15

CHAPTER VII.

A SUMNER.

Ir has already been said the sun should be observed for time when bearing nearly east or west, for then the altitude cannot only be observed with more accuracy and the time noted more exactly when the sun is rising or falling the last, est, but the longitude can be found without the necessity of the latitude being accurately known; in fact an uncertainty of two or three degrees in the latitude would not make much difference in the time derived from the observation.

As the sun begins to move away from the east or west points the error in the latitude begins to affect the longitude more and more, until at north or south a very slight difference in the latitude makes a great difference in the longitude.

The sun can only pass the east or west points when its declination is of the same name as the latitude; but when they are of contrary names the sun cannot bear east or west, but will come nearer to those points at rising or setting, at which time the low altitude is too much affected by the excessive refraction. In either case clouds and other causes will often interfere to prevent the observation being taken at or near the proper bearing; hence it is plain the latitude should be accurately known.

Now it will often happen that a meridian altitude for latitude cannot be had for several days, while at the same time dead-reckoning must be relied upon to work the latitude up to the time of the observation, from which an error is sure to follow. It remains, then, to show what use can be made of the sun to find the position of the ship when the sun occupies a place neither east nor west nor on the meridian. This brings us now to the most important problem in navigation, and one which is universally used at sea, called "a summer."

This method consists in working the observation, when the latitude is uncertain, with two assumed latitudes, the one a little greater and the other a little less than the latitude we are supposed to be in, by which one observation for time enables us to find the bearing of land, and two observations, between which the sun has changed its bearing, will give us both the latitude and longitude provided the chronometer is right or its error and rate are known.

Circles of Equal Altitudes. At any given instant the sun is vertically above some point on the earth's surface. At this spot an observer with a sextant would find the true altitude of the sun's centre to be 90 degrees. If, however, the observer should shift his position away from the sun, its distance from his zenith would of course become greater and its altitude less. He would then be situated upon a small circle

the centre of which would be the spot under the sun. All persons on that circle would have the sun at an equal alti-Finally, when he came to the horizon, all points on the circle would have the sun in the horizon. These circles of equal altitudes cut the various parallels of latitude and meridians at different angles. Near the east and west points the circles run up and down nearly with the meridians; so that if the observer were at the east or west points of the circle it would make little difference whether the latitude were exact or not, for there the longitude remains nearly the same for a long distance in latitude. Near the north and south points the circles run nearly east and west with the parallels of latitude; so that if he were at one of those points of the circle, a very slight difference in the latitude would make a great difference in the longitude. Hence it follows if an observer had a certain altitude we see that different latitudes would put him at different points of his circle of equal altitudes. and that these points would differ in longitude, at first slowly when near east or west, and then more rapidly as the point approached north or south.

Line of Position. As the circles are so large, compared with the difference between the latitudes which are used, this portion of the circle may be regarded as a straight line, which line is called a line of position, and is always at right angles to the bearing of the sun.

To obtain this line of position in actual practice, assume a latitude which is 10 to 30 minutes greater than that by dead-reckoning and a latitude 10 to 30 minutes less, and from each of these work out the observation for time. From the two resulting longitudes and the latitude of each, plot the positions on the chart and connect them by a straight line; we shall then have a line on which the ship is somewhere.

If this line runs parallel to the coast, its distance is approximately known, and the bearing of some known point on shore or a cast of the lead will give the position on the line. If the line on the chart be extended till it meets a point of land, it shows the bearing of that point. Although the exact distance of this point is unknown, yet we have only to sail on this line till the point is reached. Thus it is seen how with one observation the ship may be kept out of the danger whose bearing or distance is not exactly known.

If, after the sun has changed its bearing not less than three points,—but the nearer to eight points the better,—we should take another observation, it will give, by working in the same manner, a second line of position, which must cross the first one at some point, as they are each at right angles to the sun at the moment of observation. If the ship has not changed her position between the observations, the point of intersection of the two lines of position will be the position of the ship. But in practice the ship is very seldom stationary between the observations, and to find her position at the moment of the last one, lay off on the chart from the first line of position the course and distance made good between the two observations. and draw a parallel line to this first line of position; then the ship would be somewhere on the parallel line after having sailed a certain distance in a given direction. As the ship is also on the second line of position, its intersection with the parallel line will be the position of the ship at the moment of taking the second observation.

If the two lines of position do not intersect, the latitudes used were not far enough apart, and the lines must be prolonged till they do meet.

EXAMPLES.

On Nov. 9, 1889, in the forenoon, in latitude 34° 40′ N. by dead-reckoning, observed the altitude of the sun's lower limb 22° 29′ 20″; watch time of observation 8^h 51^m 57^s A.M., slow of chronometer time 4^h 54^m 15^s ; chronometer correction -2^m 12^s ; height of the eye 17 feet; index correction $+2^o$ 45'. Find the line of position. Assume the latitudes 34^o 10' and 35^o 10' N.

PREPARATION OF DATA.

W. Time 8h 51m 57 A.M.	Obs. Alt. 22° 29′ 20′′
C.—W. 4 54 15	S. D. +16 00
	I. C. + 2 45
C. Time 1 46 12 P.M.	Ref 2 20
C. Corr 2 12	Dip - 4 02
	Par. + 8
Gr. M. T. 1 44 00 P.M.	True Alt. 22 41 51
Dec. 17° 00′ 00″ S.	Diff. 1 hr. 43"
Corr. $+1$ 18	G. M. T. GOOR

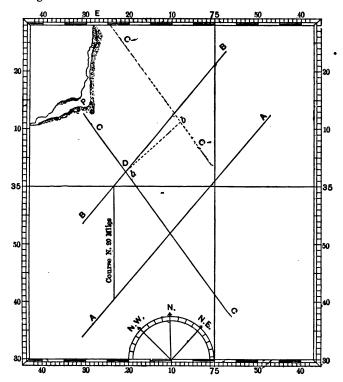
True Dec.	17 01 13 S.		Corr.	73".1		
	90	00	00		or	1′ 13′′
Pol. Dist.	107	01	13			

SOLUTION.

Alt. 22° 41′ 51″	•		
Lat. 34 10 00	sec 0.08228		
Pol. Dist. 107 01 13	cosec 0.01945		
Sum 163 53 04			
Half Sum 81 56 32	cos 9.14669		
Alt. 22 41 51	sin 9.93417		
Rem. 59 14 41			
	2)19.18259		
Alt. 22° 41′ 51″	sin 9.59129		
Lat. 35 10 00	sec 0.08752		
P. D. 107 01 13	cosec 0.01945		
Sum 164 53 04			
Half Sum 82 26 32	cos 9.11901		
Alt. 22 41 51			
Rem. 59 44 41	sin 9.93641		
	2)19.16239		
	sin 9.58119		
L. A. T. 8h 56m 16a	L. A. T. 9h 00m 43s		
Eq. T. -16 01	Eq. T 16 01		
L. M. T. 8 40 15 A.M.	L. M. T. 8 44 42 A.M.		
G. M. T. 1 44 00 р.м.	G. M. T. 1 44 00 P.M.		
Diff. T. 5 03 45	Diff. T. 4 59 18		
or	or		
Longitude 75° 56′ 15″ W.	Longitude 74° 49′ 30″ W.		

Plot these two positions on the chart and connect them by a straight line which gives a line of position AA, and if the

observation was good and the chronometer right, the ship is on this line somewhere. Although the exact position on the line is not known, its direction affords an accurate knowledge of the least possible distance the ship can be from the point of danger P.



After determining the line of position by the forenoon observation, the ship was headed due north, but at noon a meridianaltitude for latitude could not be got, and the latitude by dead-reckoning being too uncertain, another observation was taken about 4 P.M., the ship having made good 20 miles in the interval. The observed altitude of the sun's lower limb was 17° 44′ 10″; watch time of observation 4^h 04^m 58° P.M., slow of

chronometer time 4^h 12^m 20^s ; chronometer correction -2^m 12^s ; height of the eye 17 feet; index correction +2' 45''. Find the second line of position and the position of the ship. The latitude by dead-reckoning being 35° N., assume the latitudes 34° 30' and 35° 30' N.

PREPARATION OF DATA.

W. Time 4 ^h 04 ^m 53 ^s	Obs. Alt.	17° 44′	10"
C.—W. 4 12 20	8. D.	+ 16	00
	I. C.	+ 2	45
C. Time 8 17 13 P.M.		- 3	
C. Corr. -2 12	Dip	- 4	02
	Par.	+	.8
Gr. M. T. 8 15 01 P.M.	Tr. Alt.	17 56	00
Dec. 17° 00′ 00″ S.	Diff.	1 hr.	43"
Corr. + 6 54	G. M. T.	8	25
True Dec. 17 06 54 S.	Corr.	354".	.75
90 00 00		+6'	54 ′′
Pol. Dist. 107 06 54			

SOLUTION.

Alt.	17°	56'	00"		
Lat.	34	30	00	sec	0.08401
P. D.	107	06	54	cosec	0.01968
Sum	159	82	54		
Half Sum	79	46	27	COS	9.24927
Alt.	17	56	00		
Rem.	61	50	27	sin	9.94529
				2)	19.29825
				sin	9.64912
Alt.	17°	56′	00"		
Lat.	35	3 0	00	sec	0.08931
P. D.	107	06	54	cosec	0.01968
Sum	160	32	54		

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Half Sum 8	0 16	27	cos	9.22737	
Alt. 1	7 56	00			
Rem. 6	32 20	27	sin	9.94730	
			2)	19.28366	
			sin	9.64183	
L. A. T. 3h 3:	1m 47•		L. A. T.	8h 28m	00•
Eq. T16	3 01		Eq. T.	— 16	01
L. M. T. 8 15	5 46	P.M.	L. M. T.	3 11	 59 р.м.
G. M. T. 8 15	01	P.M.	G. M. T.	8 15	01 р.м.
Diff. T. 4 59	15		Diff. T.	5 03	02
Longitude 74° 4	18' 45'	' W .	Longitude	75° 45′	30" W.

From any point on the line of position AA, set off the true course north, and the distance 20 miles made good in the interval, and through the spot draw the parallel line BB. Then plot the two positions by the P.M. observation on the chart, and connect them by a straight line which will give a second line of position CC. The point D where it cuts the parallel line BB will be the position of the ship at the moment of the second observation.

Had there been no other line of position, CC prolonged would give the bearing of the point of land or danger P; and though its distance would not be accurately known, the soundings might give it: hence the danger could be avoided by shaping a course in a direction away from the line of position.

Should it be intended to dodge the point of land and make a port E on the other side, draw a parallel line C'C' to CC through E, and with the dividers measure the shortest distance bb between CC and C'C'; run that distance on a course perpendicular to CC; then by changing the course in the direction of C'C' the vessel will make the port E right ahead.

Had it been possible to obtain a meridian altitude for latitude, we could have laid off from the first line of position the course and distance made good from the time of observation to noon, and then drawn a parallel to AA. The spot where

the noon latitude cut the parallel would have been the position of the ship at noon.

It will be seen by an inspection of Table V that the cosine of 90 degrees and the sine of zero degrees are indeterminate; hence the nearer the half sum approaches 90 degrees or the remainder zero, the more indeterminate or uncertain the longitude obtained will be.

This will occur when the sun is near the meridian. Should the half sum exceed 180 degrees, or be less than the latitude, the assumed latitudes will be beyond the circle of equal altitudes, and other latitudes must be taken nearer the one that will give a resulting longitude.

CHAPTER VIII.

ERROR OF THE COMPASS.

THE error to which the compass is constantly subjected, being compounded of variation and deviation, must necessarily be an ever-changing quantity. In some localities the variation is nearly stationary, but in others there is an annual change more than likely not corrected on the chart, and there are parts of the world where a trifling change in the position of the ship means a comparatively large change in the amount of the variation. The deviation table, as constructed in port, is liable to many changes after the vessel goes to sea. It is not uncommon, after a straight run for several days, to find the deviation change fully half a degree for every degree of alteration in the compass course, and in some instances the compass will jump a point or two without an alteration of the ship's head. This is due to a change of heel, loose iron placed near the compass, boat davits turned in that were before swung out, or the many causes mentioned in the first chapter. From this it will be seen nothing but constant watchfulness of the behavior of the compass can ensure safety; to this end the error of the compass is frequently determined.

The compass bearing of the sun is taken and the true bearing for the same instant is calculated, the difference between

the two being the error, and is marked E. or W. according as the compass bearing falls to the left or right of the true bearing.

Should the error be found to change much, it would be advisable to head the vessel so as to get the error on every few points in that half of the compass most likely to be used during the next few days, and especially so if approaching land.

There are three ways of finding the true bearing of the sun at sea: by lines of position, by an amplitude, and by an observed altitude.

By Line of Position. The most simple method of determining the true bearing of the sun is by the lines of position plotted on the chart and sufficiently accurate for all purposes in navigation.

It has been said the sun always bears at right angles to the line of position: so at any point on the line of position draw a perpendicular and refer it to the true compass on the chart. The direction of this perpendicular is the true bearing of the sun; comparing this with the compass bearing at the time of taking the observation from which the line of position was derived, will give the error.

By an Amplitude. When the sun is rising or setting, its distance from the E. or W. points of the horizon is called its amplitude.

As refraction causes the sun to appear higher than it actually is, and its effect is greatest when the sun is in the horizon, being about equal to the apparent diameter of the sun, the bearing should not be taken for an amplitude when the centre appears in the horizon, but when it is a little more than its diameter plus the dip above the horizon.

Take from Table III the declination of the sun for the Greenwich date and correct it for the Greenwich time. Add together the sine of the declination and the secant of the latitude; from Table V the sum (rejecting 10 in the index) is the sine of the true amplitude, marked E. at rising and W. at setting, and N. or S. as the declination is N. or S. Should the compass amplitude and the true be of the same name, their difference will be the error; if of different names, their sum will be the error for the course the ship is heading. If this error be to the right of the variation on the chart, the deviation will be easterly; if to the left, westerly.

EXAMPLE.

At sea Nov. 27, 1887, in latitude 40° 27' N., longitude 20° 07' W., about 4° 43^m P.M., the observed bearing of the sun at setting was W. 17° S.

L. M. T. 4^b 43^m P.M. Dec. 21° 08′ S. Long. 1 20 W. Corr. — 2.42

G. M. T. 6 03 P.M. True Dec. 21 05 18 S. sin 9.55597 Latitude 40 27 N. sec 0.11863

sin 9.67460

Diff. 1 hr. 27"

G. M. T. 6^h

Corr. — 162 or 2' 42"

True amplitude W. 28° 13 S.

Compass " W. 17 S.

Error 11 13 W.

If the variation by chart was 10° W. the deviation would be 1° 18' W. for the point of the ship's head.

By an Observed Altitude. At the time of taking the altitude for time take also the bearing of the sun by compass, and note the heading of the ship; also the heel, and whether to port or starboard.

The preparation of the data in this problem is the same as that for finding the time by observation, and it is usual to combine the two. To find the true bearing, add together the true altitude, latitude, and the polar distance; take the difference between the half sum and the polar distance, and note the remainder. Then add together the secant of the altitude, secant of the latitude (rejecting 10 in each index), cosine of the half sum, and the cosine of the remainder; half the sum of the four quantities will be the cosine of half the true bearing, which, being doubled, will give the true bearing reckoned from the north in north latitude and the south in south latitude.

EXAMPLES.

We will take the first example used in finding the time, and combine the two problems to illustrate the form used in practice.

PREPARATION OF DATA.

W. Time 8^h 51^m 57^a A.M. Obs. Alt. 22° 29′ 20″ C. – W. 4 54 15 S. D. + 16 00 00 00

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C Time 1 48 19

C. Time 1 46	12	,			Kef. —	2 20	
C. Corr. — 2	12	;			Dip -	4 02	
·				•	Par. +	8	
Gr. M. T. 1 44	00	P.	м.		Alt. 22 4		•
Dec.	17°	00	' 00 ''	S. Di	ff. 1 hr. 4	13''	
Corr.	+	1	18	G.	M. T. 1	.7	
True Dec.	17	01	13	S. Co	rr. 731		
	90	00	00	or -	+ 1' 18"		
				-	,		
Pol. Dis.	107	01	13				
		80	LUI	ION.			
Alt. 22° 41′	51''				se	c 0.03	500
Lat. 35 00	00		8	ec 0.08664	se se	c 0.08	664
Pol. Dis. 107 01	13		cos	ec 0.01 94 5	;		
Sum 164 43	04						
Half Sum 82 21	32		c	os 9.12374	co	s 9 .12	374
1st Rem. 59 39	41		8	in 9.93604	Į.		
2d Rem. 24 39	41				co	s 9.95	846
				2)19.16587	2	(19.20)	384
			8	in 9.58298	i co	s 9.60	192
Local App. Time 8h	KOm F	ξQ:	. W	Helfoft	ruo hooris	or BB°	98'
Docar App. Time o	,	ν.	А.Щ.	Hall Of 6	i de bearn	ig oo	20
				True b	earing N	. 132°	52' E.
Local App. Time 8h	59™ l	58•	A.M.		earing N		
Equation of Time-					earing N		
Local M. Time 8	43	<u>-</u> 57	A.M.	Com. I	Error	2	22 E.
	44 (00	P.M.				
		_					
Diff. Time 5	00	08					

It will be seen from the above example that as it requires very little more work in the solution of the problem for time to obtain the compass error, it is always best to take the bearing of the sun by compass at the same instant the altitude is taken for time and combine the two, as shown in examples.

Longitude '75° 00' 45" W.

On April 3, 1888, in the forenoon, in latitude 29° 42' 30" S. and east longitude, the observed altitude of the sun's lower

limb was 22° 41′ 30″; bearing per compass S. 89° E.; index correction -2′ 30″; height of the eye 24 feet. Watch time of observation 8^h 06^m $20^o.5$; slow of chronometer time 8^h 08^m 14°; chronometer correction -6^m 19^o . Find the longitude and error of the compass.

PREPARATION OF DATA.

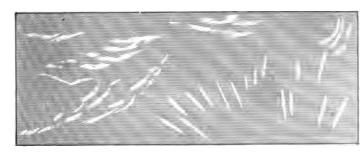
I ILLII AILATION	OF DAIA.
W. Time 8h 06m 20s.5 A.M.	Obs. Alt. 22° 41′ 30″
C. — W. 8 08 14	S. D. + 16 00
	I. C 2 30
C. Time 4 14 34.5 A.M.	Ref 2 19
C. Corr. $-6 19$	Dip - 4 48
	Par. + 08
G. M. T. 2d 16 08 15.5	•
or	True Alt. 22 48 01
$3d - 7^{h}.86$	
Dec. 5° 35′ 00″ N.	Hr. Diff. 57"
Corr. -728	G. M. T 7.86
	
True Dec. 5 27 32 N.	Corr. 448.02
90 00 00	or
D-1 Di-+ 05 07 99	— 7' 28"
Pol. Dist. 95 27 82	
SOLUTIO	on.
Alt. 22° 48′ 01″	sec 0.03533
Lat. 29 42 30 sec	e 0.06120 sec 0.06120
Pol. Dist. 95 27 32 cosec	0.00198
d 140 PO 00	
Sum 147 58 03	
Half Sum 73 59 01 cos	9.44077 cos 9.44077
1st Rem. 51 11 00 sin	9.89162
2d Rem. 21 28 31 ·	cos 9.96875
2)	19.39557 2)19,50605
sin	9.69778 cos 9.75302
Local App. Time	8h 00m 43* A.M.
Equation Time	
<u>-</u>	
Local M. Time 8	•
Gr. M. Time 4	l 08 155 а.м.
Diff. Time	S 55 42.5
Longitude 58	5. 55' 37" Pritized by Google

Eq. Time Table, IV., $+3^{m}$ 10	Half of true bearing 55°	, 30,	37''	'
Daily Variation 18 ^s			2	
Correction, Table IVa, 5				
	True bearing S. 111	01	14	E.
Equation of Time + 3 15	Compass bearing S. 89			E.
	-		—	
	Compass error 22	01	14	W.

CHAPTER IX.

CAUSES THAT AFFECT NAVIGATION AT SEA.

Clouds. The general appearance of the clouds tends greatly to assist the navigator in foretelling the state of the weather; and according to their form they are divided into three classes, called cirrus, cumulus, and stratus. There are four other forms in which these are blended, known as cirro-cumulus, cirrostratus, cumulo-stratus, and nimbus. Though it is easy to distinguish the first three classes when their forms are well characterized, it is often very difficult to accurately designate the blended forms, as some observers will call cirro-stratus what others would designate cumulo-stratus.

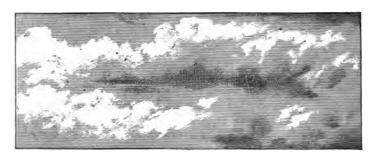


CIRRUS.

The Cirrus are composed of thin filaments, resembling a brush, and at times woolly hair or slender network.

are the most elevated clouds, and their appearance often precedes a change of weather. In summer they announce rain; in winter, frost or snow.

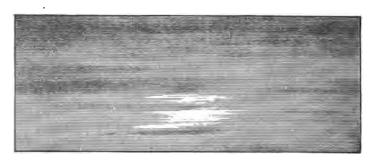
The Cumulus appear in the form of a hemisphere resting on a horizontal base; sometimes these hemispheres rest one



Commune.

upon the other, and form those great clouds which accumulate on the horizon, and look like distant mountains covered with snow. They predict warm southerly winds.

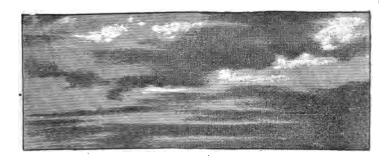
The Stratus are the horizontal bands, which form fre-



STRATUS.

quently at sunset, and, combining with the other two forms, indicate what might be expected in the state of the weather—moisture.

Cirro-cumulus appear as a number of little round, fleecy clouds, and foretell heat.



CIRRO-CUMULUS.

Cirro-stratus are composed of little bands of filaments, more compacted than those of the cirrus, and not so high, of a gravish tint, and hardly ever fail to form rain.



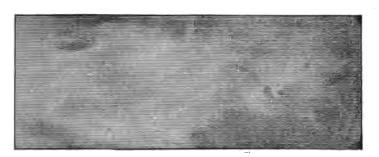
CIRRO-STRATUS.

Cumulo-stratus are formed from the cumulus clouds becoming more dense, or heaped together. If they appear in the morning, rainfall may occur, but will cease near noon as a rule; and when they form about noon, rain may follow, but will cease towards evening.



CUMULO-STRATUS.

Nimbus are the dense black clouds with gray-fringed edges, and are variously composed of the other forms, mainly



NIMBUS.

of the compacted cumulus, and are always accompanied by rain, wind, or storms.

Storms and Currents are most uncertain causes that endanger the position of the ship at sea, and should, be carefully guarded against.

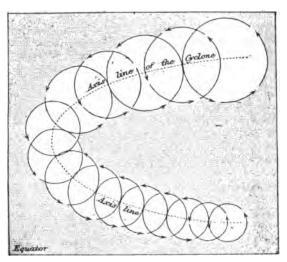
Storms. Wind is air in motion caused by difference of temperature, and the direction is designated by the point of the compass from which it blows. When this difference of temperature is great the motion of the wind is exceedingly heightened, and in some cases in the region of a mountainous

coast it rushes suddenly down with almost irresistible force. The wind blowing in great violence in one direction is called a straight-line gale. The most severe gales met with, however, at sea, are commonly known as revolving storms. variously called hurricanes, typhoons, and cyclones, according to the locality in which they blow. These revolving storms have two mofions-one in a circle like a whirlwind, and the other a forward movement on a curved track. Knowing these two movements, the problem then to be considered in relation to the safety of the ship is . 1st. Ascertain the character of the storm and locate its centre 2d Determine which half of the storm-centre the ship is in. 3d. The direction in which the storm is moving. 4th. What to do with the ship to escape the centre, or take advantage of the fair winds.

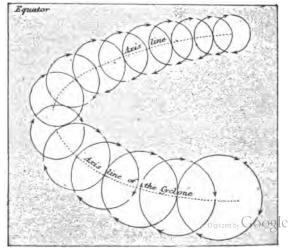
The character of the storm is indicated by the weight of the atmosphere, and as heat and moisture are the principal causes of the variation in the weight of the atmosphere, it follows that the temperature and degree of moisture should be known at the time of observation. The barometer is an instrument for measuring the weight, the thermometer gives the temperature, and the hygrometer the degree of moisture in the air.

The Barometer. There are various forms of the barometer, but the one best suited for observations is the mercurial, consisting of a brass tube about 33 inches in length, the extremity of which is inserted into a small cistern. In order to maintain the mercury in the cistern at the same level, the cistern is constructed partly of leather. By means of a screw at the bottom, the surface of the mercury in the cistern may be so adjusted as to have it always at the place from which the The upper part of the tube is cut through scale commences. so as to exaose the column of mercury. Attached to one side of this opening is a scale graduated in inches and parts; and inside this slides a small tube carrying a vernier, which is moved up or down by a small thumb-screw. A thermometer is attached to the barometer to indicate the temperature of the mercury in the cistern. When suspended for use the barometer should hang freely in a vertical position, exposed in the shade where no local heat or cold is liable to affect it.

[NORTHERN HEMISPHERE]



[SOUTHERN HEMISPHERE]



THE TWO MOTIONS OF A CVCION

Whenever opportunity offers, the barometer should be compared with a standard, and the corrections noted.

A want of absolute information as to the mean level of the mercury will not prevent advantage being taken of barometrical observations in practical navigation; yet it is best to know the mean level at the position of the observer. Monthly charts issued by the Hydrographic Office of the Navy Department, a branch office of which is located at all large maritime cities in the United States, gives the mean level of the barometer at a great many positions in the Atlantic and a few in the Pacific Ocean. In the absence of these charts, the following table, according to Maury, is most reliable for each parallel of latitude in the North Atlantic, from the equator to seventy degrees North.

North latitudes.	Height of barometer.	North latitudes.	Height of barometer.	North latitudes.	Height of barometer.
Equator. 5° 10 15 20	Inches. 29.918 29.910 29.941 29.989 30.052	25 80 35 40 45	Inches, 80.119 30.182 30.162 30.111 30.052	50 55 60 65 70	Inches. 30.001 29.989 29.878 29.839 29.800

The Thermometer is an instrument founded on the principle that most bodies expand by heat and contract by cold. Its construction differs from the barometer in having the tube closed at both ends. There are three descriptions of thermometers in common use, constructed on the same principle, but differing in the division of their respective scales. Fahrenheit's thermometer is the one generally used in America, and is marked from melting ice at 32 degrees to boiling water at 212 degrees, the interval being divided into 180 equal parts. The same graduation is extended downwards to zero and below. The bulb should be kept dry, and exposed in the shade to the open air.

The Hygrometer is simply a thermometer with the bulb wrapped in a little muslin bag, or a kind of wick reaching from it into a small cistern of water from one to three inches away. The difference in the reading of the wet and dry thermometers gives the evaporating power of the air, upon

which depends the amount of moisture present. The thermometer and hygrometer should be enclosed in a case having a lattice front.

Approach of a Storm. The indications of the approach of a storm are: a restless state of the barometer; a hard gray sky or one having a greenish tint; a blood-red or bright-yellow sunset: a heavy swell, and a thick, lurid appearance of the sky. in connection with a general threatening condition of the weather. No great storm ever sets in with a steady rising barometer, and it will blow a storm whenever the barometer rises or falls suddenly. The barometer will not rise much in front of a slowly moving storm, but the banking up of air on the border in front of a rapidly moving storm will often cause it to rise suddenly. A very rapid fall of the barometer after fairly entering the storm may be regarded as evidence of a very violent storm of small diameter, while a gradual fall would indicate the contrary. In the North Atlantic, anywhere between the equator and 30 degrees north latitude. when the barometer is observed to fall at the rate of .02 of an inch per hour and to reach a point from .2 to .3 below the mean level, precautions should be taken against the approaching storm. Gales will last a longer or shorter time, and are foretold twelve hours at least and sometimes twenty-four hours in advance, according as the rise or fall of the barometer is more or less rapid. A northerly wind will produce a high or rising barometer, and a southerly wind a low or falling barometer; hence, the barometer being very high, with northerly winds, a sudden fall accompanied by rise of the thermometer indicates that the wind will back with great force to the southward. Should the barometer be very low, a sudden rise with a falling thermometer predicts a change of wind from the SW. to the NW. and a northerly gale. In winter a sudden fall of the barometer and the thermometer towards the freezingpoint indicates snow. Off the coast of the United States the region traversed by the Gulf Stream is remarkable for its high temperature and for squally and uncertain weather, especially in winter. When the winds from W. to SW. blow a gale the heat of the atmosphere reaches its extreme, while beyond the northern and eastern limits of the storm is extremely cold. Should a storm be blowing from the NE

and the barometer begin to fall with a rise of the thermometer, the wind will haul to the E. and SE.; but should the barometer suddenly rise more, with a falling thermometer, the wind is liable to shift suddenly and with great force to the NW., and come out clear and cold.

To Locate the Centre. When facing the wind the centre of the storm will bear eight points to the right in the northern or eight points to the left in the southern latitudes: because in the northern portion of the globe the wind within the storm revolves from the right to left or left-handed, and in the southern part the wind revolves from the left to right or right-handed. Hence, when north of the equator, at the west point of the storm-circle the wind is north and the centre bears east; and south of the equator, at the west point of the stormcentre the wind is south and the centre bears east. barometer falls at the rate of .03 of an inch per hour and gets from .4 to .5 below the mean level, the indication is that the centre of the storm is about two hundred miles off; with an hourly fall of .05 to a point .78 of an inch below the mean level, the vessel may be considered about one hundred miles With a fall of .09 to 1.5 per hour below the mean level. the vessel will be very close to the centre, if not in it. the barometer begins to rise again, at first very quickly and afterward with a more moderate movement, the centre of the storm will be travelling away from the ship, and the danger is over.

Semicircles of the Storm. The storm-circle is divided into two equal parts by the storm track, and that portion on the right side looking in the direction of the track is termed the right semicircle, while that portion to the left is called the left semicircle.

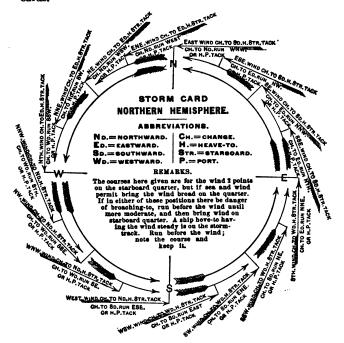
In the right semicircle the change of wind will be to the right, and in the left semicircle the change will be to the left; therefore the first change of wind will indicate which half of the storm-circle the ship is in. Should the vessel be directly on the track of the storm or near it on either side there would be no perceptible change of wind, but a falling barometer would indicate the vessel was in front and a rising barometer in rear of the storm.

Direction of Storm Track. The approximate direction in which the storm is moving may be found by plotting on

the chart the position of the ship and centre of the storm on two or more bearings as the wind changes, using the distance of the centre by barometer, and keeping an accurate account of the distance made by the ship in the interval.

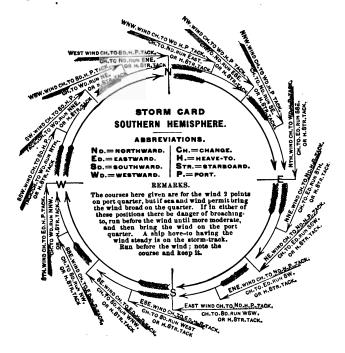
To Avoid the Centre. Having ascertained the above data, it becomes necessary now to determine what to do with the ship to escape the centre or place the vessel in a position to incur the minimum amount of danger or take advantage of the fair winds as the case may be.

The rules to be observed are given in the following storm-



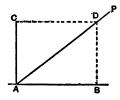
Currents. A current is a progressive motion of the water, occasioned by prevailing winds and differences of temperature and density, and causes all floating bodies to move in the direction of its set. The set is that point of the compass towards

which the waters run, and its drift is the rate it runs per hour. The effect of a constant or prevalent wind produces what is called a drift current, is generally shallow, and hardly ever exceeds half a mile per hour with a good breeze. The accumulation of the drift into a collective mass by the intervention of some obstacle produces what is called a stream current. It takes the direction imposed by the obstacle, and in many cases is a deep, powerful stream, not unlike a river in the ocean. These two forms of current cause a constant circulation to be going on in the waters of the globe, and are usually marked on



the charts with the set and drift given. As they are liable to vary in both speed and direction and temporary eddies not marked on the chart, their existence and influence may be found by a comparison between the position by dead-reckoning and that by observation, corroborated by a change in the temperature or density of the water.

Current Sailing. With the set and drift of a current known, it can be allowed for in the following manner: Draw a line



AB on the chart in the direction of the set, and from the position of the ship A lay off on this line AB equal to the hourly drift, taking the measurement from any convenient scale, say an inch to the mile. With the same scale at A erect a perpendicular to AB, and lay off on this perpendic

ular AC equal to the vessel's speed per hour; draw CD parallel to AB, and BD parallel to AC. In order then to make good the intended course AD, and keep the objective point P constantly on the same line of bearing, the vessel will have to steer in the direction of AC. The scale on the chart will be found too small to give a working size to the figure; however, it can be used by multiplying the drift of the current and the rate of the vessel by some convenient number.

Icebergs. The currents from the polar regions bring with them great quantities of floating ice, and the presence of these icebergs constitutes a very serious danger to navigation. The latitudes in which these floating islands are to be met with are generally marked on the chart, and when in those regions no precaution should be neglected to discover them before the danger becomes too great.

A large iceberg will denote its presence, even on the darkest night, by a sort of whiteness or halo known as "ice blink." The echo of a gun or steam-whistle is liable to detect the presence of an iceberg; and should one be to windward, the temperature of the air would indicate its proximity. The temperature of the water cannot be relied upon as a means of detecting the presence of ice.

Should a being be discovered, always endeavor to pass on the weather side on account of the loose pieces drifting more rapidly.

CHAPTER X.

AIDS TO NAVIGATION.

When the vessel on her course leaves the deep water and comes upon soundings, the fact is at once known by a change in the temperature of the water and the blue appearance of the sea changing to a decided green color. The evidence of approaching shore is seen in the presence of birds, floating objects, nature of the swell of the sea, and the sense of smell. The land is first seen in an outline resembling a thick cloud, but which can hardly be mistaken.

In making the proper point or working the way into port assistance is afforded in the nature of the shore, complexion of the land, and configuration of the coast-lines, as well as any isolated tree, church spire, windmill or prominent mountain.

In addition to these, all maritime countries have established a well-concerted series of landmarks as aids to navigation, such as light-houses, light-vessels, buoys, beacons, and fogsignals.

Light-houses. The light-house is not only a house or tower especially adapted for showing a light at night, but serves as a landmark by day. They are sufficiently diversified by different characteristics to properly define their respective positions.

As we approach the shore from seaward the most salient points of the coast-line are marked by first-class light-houses having the greatest power and range. They are planted so close to each other as to prevent the vessel from getting within any outlying danger, except in a dense fog, without catching sight of one or more of them. They give warning of the position of the vessel, and enable any errors to be corrected before the ship shall have approached too near the coast for safety.

The secondary capes, reefs, and sand-banks, to which it is prudent to give a good offing, are marked by second- and third-class light houses, and the range is regulated by the distance at which it is necessary to see them. During thick weather



SEA-COAST LIGHT-HOUSE AT CURRITUCE BEACH, NORTH CAROLINA.

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the range of the first-class lights is greatly diminished in power and extent when those of the second class assist to fill up the vacancy thus caused in the primary illumination. Lights of these classes are also placed to mark the mouths of rivers and the entrance to ports only accessible by narrow channels, and to point out the exact course which should be steered.

Near the port or anchorage a small harbor light is placed upon one or each of the banks, piers, or breakwater as a guide to a good berth. Many of these small lights belonging to tidal harbors are not exhibited until the tide has reached a certain determined height.

Order of Lights. In the United States the lights are divided into six orders. Lights of the first order are those established to give warning of the approach to land; those of the second, to mark the secondary points or headlands along the sea coast and the approach to bays and sounds; third-order, lights are used in bays that are of considerable width and intricacy, and for the coast of lakes; lights of the fourth, fifth, and sixth orders mark the most prominent points, headlands, or shoals in the long bays, sounds, or obstructions in rivers, and piers or wharves.

Character of Lights. In addition to the division of lights according to their position for illumination, provision is made for their easy distinction so as to not mislead by a close resemblance of one to the other. To this end lights are divided into several distinctive characters—the fixed, revolving, flush or intermittent, and double light on one or two towers.

The Fixed Light is one which exhibits a regular and steady appearance, and is not subject to any change.

The Revolving Light gradually increases to a maximum and diminishes to a minimum until wholly extinguished at equal intervals of half a minute, one, two, or three minutes, and sometimes thrice a minute. It is produced by the revolution of a three- or four-sided frame having large reflectors grouped on each side, with their axes parallel.

The revolving light is subdivided into other classes, such as revolving white, revolving red and white, revolving red with two whites, or revolving white with two reds, obtained by the revolution of a frame whose sides present red and white lights in succession.

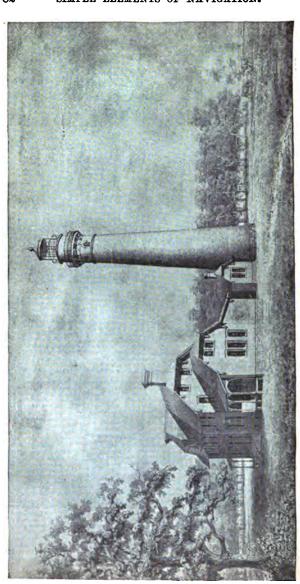


LIGHT-HOUSE ON ALLIGATOR REEF, FLORIDA REEFS.



BUG LIGHT.

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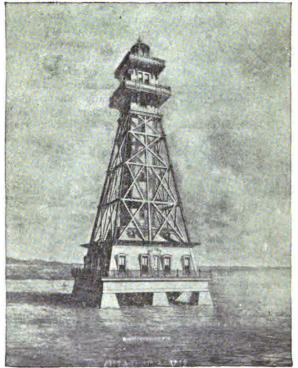
The Flash or Intermittent Light is one in which the ray suddenly appears, remains visible for a moment, and afterwards is again suddenly eclipsed for a brief interval. This is due to the perpendicular motion of circular shades in front of the reflector by which the light is alternately revealed and hidden. This light and the revolving light are sometimes combined to form the revolving flash light.

The Double Lights are seldom used except where a leading line is needed as a guide for taking some narrow channel or avoiding some danger. They are generally exhibited from two towers, one of which is higher than the other, and produce marked characteristic distinction or serve as a range to avoid danger. In the first case the distance between the lights is such as to prevent the two being blended into or supposed to be one lightt within the limits of their ranges. In the second case they are so arranged they will be seen to separate the moment of departure from the straight range line they are placed to mark. Frequently a very small are is illuminated by one light which can be seen before encountering danger.

Colored Lights. Another means of distinguishing the various lights is in their color: some are red, with an intense ruddy-like splendor; others white, and some blue or green. However, colored lights should be observed with caution, as the use of coloring matter reduces in great proportions the intensity of the light; and the atmospheric conditions sometimes determine the color, which may lead to mistake as to the real color of the light. It has been observed that during foggy weather white lights become of a reddish color or tinge; green appears to approach in color or become white; and blue lights are not visible or change to so pale a violet tint as to be mistaken for white. But if there be two lights of different color, such as red and white, one becomes intensely red and the other a red tinge, both preserving their distinctive character. green were in place of red, the two lights would appear to be red and white without a marked difference in color. Some heavy fogs, however, allow all the luminous rays to pass through them equally without coloring them, and only have the effect of diminishing their intensity. With equal intensity, the red light will be seen farther than the white light; but if the two are used, the white light will cease to be visible before the red light.

The electric light possesses a great distinction of color, but very little superiority in penetrating power in thick weather, and at any time is blinding, or its distance hard to ascertain.

Range of Lights. The distance at which a light may be seen depends upon its intensity and height above the sea or its luminous and geographical range. The luminous range de-



CRAIGHILL'S CHANNEL RANGE LIGHTS .- HIGH LIGHT.

pends upon the state of the atmosphere and the acuteness of the eye of the observer.

The geographical range depends upon the height above the level of the sea, upon the curvature of that part of the earth's surface at which it is placed, and upon the value of atmospheric refraction.

In the United States the heights of all light-houses are given in the lists and nautical books for mean low-water, together with range corresponding to different heights above the level of the sea both for the focal point and the eye of the observer. In some countries the tables are made out with reference to the level of the highest water.



CRAIGHILL'S CHANNEL RANGE LIGHTS.-LOW LIGHT.

By a reference to the chart, light list, and sailing directions a minute description and sketch of all light-houses will be found, their position accurately noted, the character and brilliancy of the light, the order or class, bearings on which the light is visible or obscured, height of the centre of the lantern above the high-water level or mean low tide; height also of the building from the base to the vane, and its form, color, and other peculiarities.

Light-ships. The seas adjacent to the coast are sometimes interspersed with extensive shoals and shifting sandbanks, upon which it is impossible to erect light-houses. Nor can those already built upon the mainland be made serviceable in directing vessels their way through the narrow channels running in all directions, distant perhaps fifteen or twenty miles off the coast.

In approaching the sea immediately surrounding these dangers, light-ships or floating lights are used to indicate the exact points to be avoided. They also serve as beacons against variable currents and reefs which are hidden at certain hours by the high tide.

Each light-ship, like the light-house on shore, is distinguished by its own peculiar aspect, various characteristics, and certain differences in telling not only one from another, but also from any neighboring light-house.

How appear. When seen at some distance a light-ship closely resembles during the day an ordinary vessel, but upon approaching near a great difference between the two is seen. The short stout masts are without sails, and surmounted by large balls, cages, or other marks.



LIGHT-SHIP.

In Great Britain the hulls of light-ships are painted red and black. In the United States they are painted such color and in such a way as the Light-house Board may designate, with the name of the station painted on the sides and the number of the vessel on the stern.

At night these vessels are provided with one or more lights, and are distinguished by their number and position as well as characteristic distinction—such as single or double fixed lights, revolving lights with varying intervals of darkness between the beams, or with colored beams alternating with white, or colored beams only.

When two lights are used, it is usually the custom to place one higher than the other.

Few instances are on record of a light-ship having broken loose from her moorings. If, however, the ship should be driven from its place by the force of the elements, so that its light may become a source of danger, means are provided for signalling by flags or the firing of a gun. No one except those belonging to the light-ships is ever permitted to live on board or to remain at night, unless necessarily detained by stress of weather, or wrecked persons who may be compelled to take temporary refuge on board.

Buoys are the next very important marks that contribute greatly as aids to navigation. They are exceedingly numerous, and are invaluable as guiding marks by day through narrow channels and warning marks for isolated dangers. They are not very serviceable at night, being unilluminated; however, buoys have been lit in many instances by the application of compressed gas confined within the buoy; and it has been proposed to connect them with wires all around the coast, and to light them simultaneously with electricity.

Distinction. Their chief elements of distinction are the form, size, and color, which may be supplemented by the addition of a shape—such as globe, diamond, triangle, etc.—mounted on top of the mast fixed in the head of the buoy.

Names of Buoys. The names of the various forms are so unsettled, that but few persons can accurately state what constitutes the characteristic of each. However, the descriptive titles of buoys are: the nun, can, conical, convex, spiral, drum, cylinder, spherical, spar, mast, and cask. These terms are found to vary at different places, and are employed to give

exactly opposite indications; also, intimations conveyed by colors vary at different places: hence, reference to name or disposition of colors is apt to lead to some confusion.

In France a uniform system of coloring is used, and on each is painted either the entire or abridged name of the rock or bank that it marks; those belonging to the same channel are numbered serially, commencing to seaward. Those to mark the starboard side are painted red, having a white crown a little below the summit, and bear the even numbers. Those to mark the port side are painted black, and bear odd numbers. Those which may be left indifferently on either side are painted with horizontal stripes alternately red and black, bear names, but no numbers. The red and black are varied, as circumstances require, by painting in white designs of checks, vertical bands, etc.

In England the entrances to channels or turning-points are marked by conical buoys with or without staff, and globe or triangle, cage, etc. Single-colored can-buoys, either red or black, mark the starboard side, and buoys of the same shape and color, either checkered or vertical-striped with white, mark the port side. Other distinctions are used, when required, by the employment of conical buoys with or without staff, globe, or cage, globes being on the starboard side and cages on the port hand. Where a middle ground exists in a channel, each side of it is marked by a buoy of the color in use in that channel, but with annular bands of white, and with or without staff, diamond, or triangle. In case of its being of such extent as to require intermediate buoys, they are colored as if on the side of a channel. At times the outer buoy is marked by a staff and diamond, and the inner end by a staff and triangle. Wrecks are marked by green nun-buoys placed on the wreck next to mid-channel, with "Wreck" painted thereon; also two balls or two lights, as the case may be.

Each buoy is marked with a running number, and the name of the locality where it belongs.

In the Netherlands, with few exceptions, white buoys must be left on the starboard hand on entering the channel from seaward, and black buoys on the port hand. Outside buoys, and those indicating where the division of a channel begins, are painted red. In Belgium the same system prevails. In Norway and Sweden a white stake with a broom turned upwards denotes that the shoal lies to the north or east of the mark. A black stake with a broom turned downwards denotes that the danger lies to the south or west of the mark. A stake with white and black hor zontal stripes, surmounted by a ball or a pole with a cross at the top, may be passed on either side.

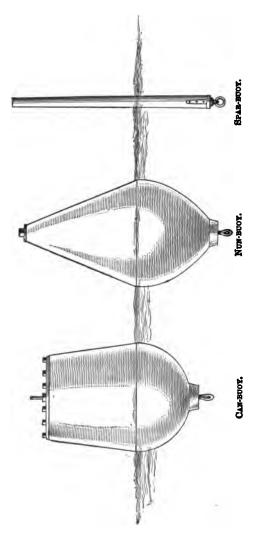
In Russia the system is nearly the same as in Norway, with this addition for the open sea: a red broom open upwards on a red pole means that the danger lies to the north; a black broom open downwards on a white pole means that the danger lies to the south. Two black brooms on a black and white checkered pole mean that the danger lies to the west; and a black pole with cross at the top surmounted by a ball means that a vessel can pass on all sides.

In the United States the largest descriptions of buoys are used to mark approaches to channels, seaward bars, and isolated shoals or other obstructions to navigation which lie at considerable distance from the coast. First and second class buoys mark the approaches to, the obstructions in, and to point out and mark the limits of channels leading to the principal ports or harbors along the coast.

They also mark the channels and obstructions adjacent to the coast and those in the large bays and sounds. Second and third class buoys mark the approaches to, and channels and obstructions of, the lesser harbors and bays. Nun and can buoys liable to danger or to be swept away by floating ice are removed on the approach of freezing weather, and sparbuoys put in their places. Small spar-buoys mark channels and obstructions in shoal-water navigation.

Special buoys, such as spherical and cask buoys, colored and numbered, are used to mark special localities. All buoys are placed in the best position to mark obstructions or define channels, and float as high and as nearly upright as possible during the strongest wind and tide. White serial numbers, as large as the class of buoy will permit, are placed on four sides of red and black buoys, and other distinguishing marks are made to show as prominently and at as great a distance as possible.

Different channels in the same bay, sound, river, or harbor are marked as far as practicable by different descriptions of buoys.



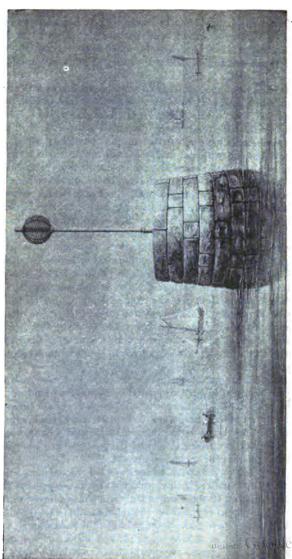
The main channel is marked by nun-buoys; can-buoys indicate secondary channels, and spar-buoys minor channels. When there is but one channel, nun-buoys properly colored and numbered are placed on the starboard side and can-buoys on the port side.

On entering the channel from seaward red buoys with even numbers are placed on the starboard side of the channel, and must be left on the starboard hand in passing in. Black buoys with odd numbers are placed on the port side of the channel, and must be left on the port hand in passing in. Buoys painted with red and black horizontal stripes without numbers are placed on rocks or other obstructions with channels on either side of them, and may be left on either hand in passing in. Buovs painted with black and white vertical stripes without numbers are placed in mid-channel, and must be passed close to avoid danger. Buoys to mark abrupt turning-points in channels or obstructions requiring a specific and permanent mark are fitted with staves surmounted by balls. cages, triangles, or other distinctive marks, the color indicating which side they shall be passed. Yellow buovs without numbers are used to mark any danger at a quarantine station.

The bearings from one mid-channel buoy to another in the order of passing to other buoys or objects, the name of the station or position occupied, the color, number, description, class, depth of water at mean low tide, kind of bottom, and such other marks to aid navigation will be found in the proper column of the buoy list.

Beacons are small but durable structures of timber, masonry, or iron, placed on low, outstretching points of land, rocks and sand-banks, shoals or elsewhere, which at certain times of the tide are hidden from view, in estuaries and broad parts of rivers. They serve as leading marks through certain channels for the avoidance of special dangers, and as a guide for entering harbors or anchorage ground.

Every beacon set up has some especial characteristic, so that it may be recognized, being usually surmounted with a characteristic head in the form of a globe, diamond, cross, or triangle. Beacons are painted in such a manner that the color will cause them to be well defined upon the background, and those on sides of channels are painted the same as buoys. Some of these beacons are provided with a ladder leading up



BEACON ON SEA-FLOWER REEF, L. I. SOUND.

to a refuge cage above the high-water mark, capable of holding several persons. As a general rule, beacons are not lighted up at night; yet several arrangements have been devised for lighting beacons on detached rocks which are inaccessible during rough weather.

Sound-signals. The various marks so far dealt with are those which depend upon the sense of sight only; but when sight is unavailing, the sense of hearing naturally suggests itself when sound-signals have to be used as aids to navigation, especially during fogs, mists, and snow-storms. These sound-signals are, with certain modifications: sirens, trumpets, steam-whistles, bell-buoys, whistling-buoys, bells struck by machinery, cannons, rockets, and gongs.

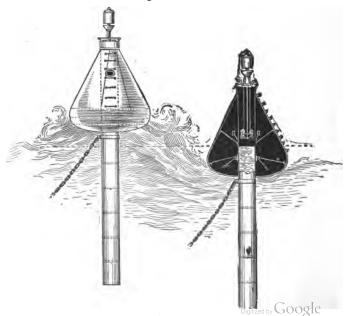
Gongs are sometimes used on light-ships and for close quarters, having an effective range of about 500 yards. They are of most use in harbors, short channels, and like places, where a long range would be unnecessary.

Rockets are used in light-houses as a signal where it would be impossible to mount large pieces of apparatus. It frequently happens that the sound-signal intended to be heard at a certain distance is obstructed or deflected by intervening obstacles; the rocket in this case overcomes the difficulty. The charge, usually of gun-cotton, is fitted to the head, and the whole projected to the height of perhaps 1000 feet, when the charge is exploded, and sound scattered in all directions, with greater effect than the report of a gun. Some of these rockets have been heard at a distance of twenty-five miles.

Cannon are used for various purposes in connection with signalling. The minute-gun at sea indicates that the vessel is in distress, and that assistance is required. On some light-ships the cannon is used to attract attention of shipwrecked life-boats. They are also used as warning signals on head-lands and dangerous points on a coast, as aids to navigation in foggy weather, as well as for signalling in accordance with an arranged code. Owing to the short duration of sound, the use of the cannon is not so great as it once was, as the observer, either through lack of attention or otherwise, may not hear unless prepared for it, the sound being liable to be quenched by local sounds, or even obliterated by a puff of wind. The interval between each shot was formerly fifteen

minutes, but recently it has been altered to ten; owing, however, to the severe labor and risks accompanying it, this interval is of considerable irregularity.

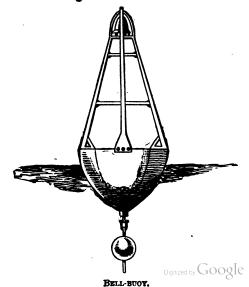
Bells are in use at every light-station, and at many they are run by machinery actuated by clockwork. These bells weigh from 300 to 3000 pounds. The sound of a bell is curiously fluctuating, and the vibrations of the largest bells are not of sufficient intensity to yield a sound capable of overcoming opposing influences, even of a slight nature, and the effective range is at times very doubtful. However, it has been shown by experiments that the range of bell sounds can be increased with the rapidity of the stroke; it has also been somewhat increased by the use of iron reflectors. By this it will be seen that the bell is only used, like the gong, for short distances, and is not efficient for fog-signals on the sea-coast. Owing to rough weather, the noises of the surf will drown the sound to seaward altogether.



COURTENAY'S WHISTLING-BUOY,

The Whistling-buoy, devised by Mr. Courtenay, is extensively employed in various parts of the world. It has a powerful whistle fixed at the top, and sounded automatically by the action of the sea, on the passage of any wave or undulation, which will cause the instrument to rise and fall six inches or more. It will emit a sound that can be heard distinctly from one to fifteen miles,—a mournful sound, which, though of great aid to navigation, is most obnoxious to those who live within ear-shot. They can be used on shoals, where a light-ship is needed but could not live; and are well suited for broken and turbulent waters, as the rougher the sea the louder their sound: they are also employed for roadsteads and the open sea.

The Bell-buoy consists of a buoy with a bell so attached that it will cause the bell to strike as the buoy is moved from side to side by the action of the sea. Like the whistling-buoy, the bell-buoy sounds the loudest when the sea is roughest, but is adapted to shoal water, where the whistling-buoy could not ride. It is preferred for harbors, rivers, and other places where the sound range needed is short.



Steam-whistles for signalling in a fog are the same instruments ordinarily used on steamboats and locomotives. They have been heard at distances, varying with their diameter, of from three to twenty-five miles.

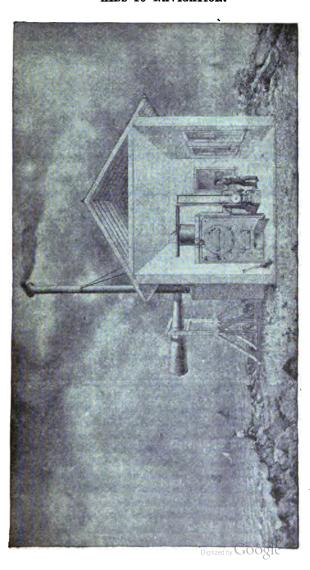
The Trumpet comes next in order, and is simply a horn that is capable of making shricks which can be heard at a great distance, and is superior to the whistle, having greater penetrating effect.

The Siren is beyond all doubt the most powerful fog signal in use, and when operated under a pressure of seventy pounds of steam can be heard, under favorable circumstances, from twenty to thirty miles. Its density, pitch, and penetration render it dominant over noises after all other signal sounds have succumbed, especially under meteorological conditions unfavorable to the transmission of sound.

The trumpet, siren, and whistle are capable of such arrangement that the length of blast and interval and the succession of alternating are such as to identify the location of each, so that the position may be determined by the sound. Double sirens of different pitch are sometimes used. There are in addition to these, in various parts of the world, several sound-signals made by utilizing natural orifices in cliffs, through which the waves drive the air in such force and velocity as to produce the sound required.

Sound-signals constitute a large factor in the safety of navigation, and it is necessary that every signal should have its own characteristic to particularly indicate itself, as a lighthouse is made to proclaim its own individuality by some distinguishing feature. The effect of different atmospheric conditions upon the transmission of sound is very marked, and it has been found by repeated trials that the sound range varies on clear, calm days; hence the minimum range should always be taken as the guide when running by sound. A most important phenomenon, affording confidence in sound-signalling when a light is rendered ineffectual, is the fact that a foggy atmosphere appears to be a highly favorable condition for the transmission of sound; while rain, hail, and snow offer no obstruction, but, on the contrary, have the effect of assisting the passage of sound.

It will be seen from the above that a vessel coming to the coast from beyond the sea will pick up the proper coast-light



in fair weather, and in thick weather the fog-signal, and take either as a point of departure and feel the way to the harbor light or fog-signal in the port, thence to a safe anchorage, with comparative security.

CHAPTER XI.

REGULATIONS FOR PREVENTING COLLISIONS AT SEA.

THE laws of all Maritime Nations require a strict observance of the following rules and regulations for the prevention of collisions at sea.

"ART. 1. In the following rules every steamship which is under sail and not under steam is to be considered a sailing-ship, and every steamship which is under steam, whether under sail or not, is to be considered a ship under steam.

"RULES CONCERNING LIGHTS.

- "ART. 2. The lights mentioned in the following articles numbered three, four, five, six, seven, eight, nine, ten, and eleven, and no others, shall be carried in all weathers, from sunset to sunrise.
- "ART. 3. A sea-going steamship, when under way, shall carry—
- "(a) On or in front of the foremast, at a height above the hull of not less than twenty feet, and if the breadth of the ship exceeds twenty feet, then at a height above the hull not less than such breadth, a bright white light, so constructed as to show a uniform and unbroken light over an arc of the horizon of twenty points of the compass, so fixed as to throw the light ten points on each side of the ship, namely, from right ahead to two points abaft the beam on either side, and of such a character as to be visible on a dark night, with a clear atmosphere, at a distance of at least five miles.
- "(b) On the starboard side a green light, so constructed as to show a uniform and unbroken light over an arc of the horizon of ten points of the compass, so fixed as to throw the light from right ahead to two points abaft the beam on the starboard

side, and of such a character as to be visible on a dark night, with a clear atmosphere, at a distance of at least two miles.

- "(e) On the port side a red light, so constructed as to show a uniform and unbroken light over an arc of the horizon of ten points of the compass, so fixed as to throw the light from right ahead to two points abaft the beam on the port side, and of such a character as to be visible on a dark night, with a clear atmosphere, at a distance of at least two miles.
- "(d) The said green and red side-lights shall be fitted with inboard screens projecting at least three feet forward from the light, so as to prevent these lights from being seen across the how.
- "ART. 4. A steamship when towing another ship shall, in addition to her side-lights, carry two bright white lights in a vertical line, one over the other, not less than three feet apart, so as to distinguish her from other steamships. Each of these lights shall be of the same construction and character, and shall be carried in the same position, as the white light which other steamships are required to carry.
- "ART. 5. (a) A ship, whether a steamship or a sailing-ship, which from any accident is not under command, shall at night carry, in the same position as the white light which steamships are required to carry, and if a steamship, in place of that light, three red lights in globular lanterns, each not less than ten inches in diameter, in a vertical line, one over the other, not less than three feet apart, and of such a character as to be visible on a dark night, with a clear atmosphere, at a distance of at least two miles, and shall by day carry in a vertical line, one over the other, not less than three feet apart, in front of but not lower than her foremast-head, three black balls or shapes, each two feet in diameter.
- "(b) A ship, whether a steamship or a sailing-ship, employed in laying or in picking up a telegraph cable, shall at night carry, in the same position as a white light which steamships are required to carry, and if a steamship, in place of that light, three lights in globular lanterns, each not less than ten inches in diameter, in a vertical line, over one another, not less than six feet apart. The highest and lowest of these lights shall be red, and the middle light shall be white, and they shall be of such a character that the red lights shall be visible at the same distance as the white light. By day she shall carry, in a

vertical line, one over the other, not less than six feet apart, in front of but not lower than her foremast head, three shapes not less than two feet in diameter, of which the top and bottom shall be globular in sphae and red in color, and the middle one diamond in shape and white.

- "(c) The ships referred to in this article when not making any way through the water shall not carry the side-lights, but when making way shall carry them.
- "(d) The lights and shapes required to be shown by this article are to be taken by other ships as signals that the ship showing them is not under command, and cannot therefore get out of the way. The signals to be made by ships in distress and requiring assistance are contained in article twenty-seven.
- "ART. 6. A sailing-ship under way or being towed shall carry the same lights as are provided by article three for a steamship under way, with the exception of the white light, which she shall never carry.
- "ART. 7. Whenever, as in the case of small vessels during bad weather, the green and red side-lights cannot be fixed, these lights shall be kept on deck, on their respective sides of the vessel, ready for use, and shall, on the approach of or to other vessels, be exhibited on their respective sides in sufficient time to prevent collision, in such manner as to make them most visible, and so that the green light shall not be seen on the port side nor the red light on the starboard side. To make the use of these portable lights more certain and easy, the lanterns containing them shall each be painted outside with the color of the light they respectively contain, and shall be provided with proper screens.
- "ART. 8. A ship, whether a steamship or a sailing-ship, when at anchor, shall carry, where it can best be seen, but at a height not exceeding twenty feet above the hull, a white light, in a globular lantern of not less than eight inches in diameter, and so constructed as to show a clear, uniform, and unbroken light, visible all round the horizon at a distance of at least one mile.
- "ART. 9. A pilot vessel, when engaged on her station on pilotage duty, shall not carry the lights required for other vessels, but shall carry a white light at the mast-head, visible all round the horizon, and shall also exhibit a flare-up light

or flare-up lights at short intervals, which shall never exceed fifteen minutes. A pilot vessel, when not engaged on her station on pilotage duty, shall carry lights similar to those of other ships.

"ART. 10. Open boats and fishing-vessels of less than twenty tons net registered tonnage, when under way and not when having their nets, trawls, dredges, or lines in the water, shall not be obliged to carry the colored side-lights; but every such boat and vessel shall in lieu thereof have ready at hand a lantern with a green glass on the one side and a red glass on the other side, and on approaching to or being approached by another vessel such lantern shall be exhibited in sufficient time to prevent collision, so that the green light shall not be seen on the port side nor the red light on the starboard side.

"The following portion of this article applies only to fishing-vessels and boats when in the sea off the coast of Europe lying north of Cape Finisterre:

- "(a) All fishing-vessels and fishing-boats of twenty tons net registered tonnage or upward, when under way and when not having their nets, trawls, dredges, or lines in the water, shall carry and show the same lights as other vessels under way.
- "(b) All vessels when engaged in fishing with drift-nets shall exhibit two white lights from any part of the vessel where they can be seen. Such lights shall be placed so that the vertical distance between them shall not be less than six feet and not more than ten feet, and so that the horizontal distance between them, measured in a line with the keel of the vessel, shall be not less than five feet and not more than ten feet. The lower of these two lights shall be the more forward, and both of them shall be of such a character and contained in lanterns of such construction as to show all round the horizon, on a dark night, with a clear atmosphere, for a distance of not less than three miles.
- "(c) All vessels when trawling, dredging, or fishing with any kind of drag-nets shall exhibit, from some part of the vessel where they can be best seen, two lights. One of these lights shall be red and the other shall be white. The red light shall be above the white light, and shall be at a vertical distance from it of not less than six feet and not more than twelve feet; and the horizontal distance between them, if any, shall not be more than ten feet. These two lights shall be of

such a character and contained in lanterns of such construction as to be visible all round the horizon, on a dark night, with a clear atmosphere, the white light to a distance of not less than three miles and the red light of not less than two miles.

- "(d) A vessel employed in line-fishing, with her lines out, shall carry the same lights as a vessel when engaged in fishing with drift-nets.
- "(e) If a vessel when fishing with a trawl, dredge, or any kind of drag-net, becomes stationary in consequence of her gear getting fast to a rock or other obstruction, she shall show the light and make the fog-signal for a vessel at anchor.
- "(f) Fishing-vessels and open boats may at any time use a flare-up in addition to the lights which they are by this article required to carry and show. All flare-up lights exhibited by a vessel when trawling, dredging, or fishing with any kind of drag-net shall be shown at the afterpart of the vessel, excepting that if the vessel is hanging by the stern to her trawl, dredge, or drag-net they shall be exhibited from the bow.
- "(g) Every fishing-vessel and every open boat when at anchor between sunset and sunrise shall exhibit a white light, visible all round the horizon at a distance of at least one mile.
- "(h) In a fog a drift-net vessel attached to her nets, and a vessel when trawling, dredging, or fishing with any kind of drag-net, and a vessel employed in line-fishing with her lines out, shall, at intervals of not more than two minutes, make a blast with her fog-horn, and ring her bell alternately."

Attention is called to paragraphs "a" and "c" of this article, which have not been adopted by foreign governments.

Paragraph "a" has been modified by the British Government to read as follows, viz.

"All fishing vessels and fishing-boats of twenty tons net registered tonnage or upwards, when under way and when not required by the following regulations in this article to carry and show the lights therein named, shall carry and show the same lights as other vessels under way."

Paragraph "c" has been omitted.

But these two provisions apply only to "fishing-vessels and boats when in the sea off the coast of Europe lying north of Cape Finisterre."

"ART. 11. A ship which is being overtaken by another

shall show from her stern to such last-mentioned ship a white light or a flare-up light.

"SOUND SIGNALS FOR FOG, AND SO FORTH.

- "ART. 12. A steamship shall be provided with a steam-whistle or other efficient steam sound-signals, so placed that the sound may not be intercepted by any obstructions, and with an efficient fog-horn, to be sounded by a bellows or other mechanical means, and also with an efficient bell. (In all cases where the regulations require a bell to be used, a drum will be substituted on board Turkish vessels.) A sailing-ship shall be provided with a similar fog-horn and bell.
- "In fog, mist, or falling snow, whether by day or night, the signals described in this article shall be used as follows, that is to say:
- "(a) A steamship under way shall make with her steamwhistle or other steam sound-signal, at intervals of not more than two minutes, a prolonged blast.
- "(b) A sailing-ship under way shall make with her foghorn, at intervals of not more than two minutes, when on the starboard tack one blast, when on the port tack two blasts in succession, and when with the wind abaft the beam three blasts in succession.
- "(c) A steamship and a sailing-ship when not under way shall, at intervals of not more than two minutes, ring the bell.

"SPEED OF SHIPS TO BE MODERATE IN FOG, AND SO FORTH.

"ART. 13. Every ship, whether a sailing-ship or a steamship, shall in a fog, mist, or falling snow go at a moderate speed.

"STEERING AND SAILING RULES.

- "ART. 14. When two sailing-ships are approaching one another so as to involve risk of collision, one of them shall keep out of the way of the other as follows, namely:
- "(a) A ship which is running free shall keep out of the way of a ship which is close-hauled.
- "(b) A ship which is close-hauled on the port tack shall keep cut of the way of a ship which is close-hauled on the starboard tack.

- "(c) When both are running free, with the wind on different sides, the ship which has the wind on the port side shall keep out of the way of the other.
- "(d) When both are running free, with the wind on the same side, the ship which is to windward shall keep out of the way of the ship which is to leeward.
- "(e) A ship which has the wind aft shall keep out of the way of the other ship.
- "ART. 15. If two ships under steam are meeting end on, or nearly end on, so as to involve risk of collision, each shall alter her course to starboard, so that each may pass on the port side of the other. This article only applies to cases where ships are meeting end on, or nearly end on, in such a manner as to involve risk of collision, and does not apply to two ships which must, if both keep on their respective courses, pass clear of each other. The only cases to which it does apply are when each of the two ships is end on, or nearly end on, to the other; in other words, to cases in which by day each ship sees the masts of the other in a line, or nearly in a line, with her own, and by night to cases in which each ship is in such a position as to see both the side-lights of the other. It does not apply by day to cases in which a ship sees another ahead crossing her own course, or by night to cases where the red light of one ship is opposed to the red light of the other, or where the green light of one ship is opposed to the green light of the other, or where a red light without a green light, or a green light without a red light, is seen ahead, or where both green and red lights are seen anywhere but ahead.
- "ART. 16. If two ships under steam are crossing so as to involve risk of collision, the ship which has the other on her own starboard side shall keep out of the way of the other.
- "ART. 17. If two ships, one of which is a sailing ship and the other a steamship, are proceeding in such directions as to involve risk of collision, the steamship shall keep out of the way of the sailing-ship.
- "ART. 18. Every steamship, when approaching another ship so as to involve risk of collision, shall slacken her speed, or stop and reverse, if necessary.
- "ART. 19. In taking any course authorized or required by these regulations, a steamship under way may indicate that

course to any other ship which she has in sight by the following signals on her steam-whistle, namely:

- "One short blast to mean 'I am directing my course to starboard.'
- "Two short blasts to mean 'I am directing my course to port."
 - "Three short blasts to mean 'I am going full speed astern."
- "The use of these signals is optional, but if they are used the course of the ship must be in accordance with the signal made.
- "ART. 20. Notwithstanding anything contained in any preceding article, every ship, whether a sailing-ship or a steamship, overtaking any other shall keep out of the way of the overtaken ship.
- "ART. 21. In narrow channels every steamship shall, when it is safe and practicable, keep to that side of the fairway or mid-channel which lies on the starboard side of such ship.
- "ART. 22. Where by the above rules one of two ships is to keep out of the way, the other shall keep her course.
- "ART. 23. In obeying and construing these rules due regard shall be had to all dangers of navigation, and to any special circumstances which may render a departure from the above rules necessary in order to avoid immediate danger.

"NO SHIP, UNDER ANY CIRCUMSTANCES, TO NEGLECT PROPER PRECAUTIONS.

"ART. 24. Nothing in these rules shall exonerate any ship, or the owner, or master, or crew thereof, from the consequences of any neglect to carry lights or signals, or of any neglect to keep a proper lookout, or of the neglect of any precaution which may be required by the ordinary practice of seamen or by the circumstances of the case.

"RESERVATION OF RULES FOR HARBOR AND INLAND NAVIGA-TION.

"ART. 25. Nothing in these rules shall interfere with the operation of a special rule, duly made by local authority, relative to the navigation of any harbor, river, or inland navigation.

- "SPECIAL LIGHTS FOR SQUADRONS AND CONVOYS.
- "ART. 26. Nothing in these rules shall interfere with the operation of any special rules made by the Government of any nation with respect to additional station and signal lights for two or more ships of war or for ships sailing under convoy.
- "ART. 27. When a ship is in distress and requires assistance from other ships or from the shore, the following shall be the signals to be used or displayed by her, either together or separately, that is to say:
 - "In the daytime-
 - "First. A gun fired at intervals of about a minute.
- "Second. The international code signal of distress indicated by N. C.
- "Third. The distant signal, consisting of a square flag, having either above or below it a ball, or anything resembling a ball.
 - "At night-
 - "First. A gun fired at intervals of about a minute.
- "Second. Flames on the ship (as from a burning tar-barrel, oil-barrel, and so forth).
- "Third. Rockets or shells, throwing stars of any color or description, fired one at a time, at short intervals."

TABLES.

EXPLANATION OF TABLES.

Table I contains the difference of latitude and departure corresponding to distances not exceeding 300 miles, and for courses to every degree of the compass.

The manner of using this table is explained in the different problems of dead-reckoning.

Table II gives the refraction, dip of the horizon, and the sun's parallax in altitude; the application of these is explained in the text under the definition of each on page 39.

Table III gives the declination of the sun to the nearest minute for every noon at Greenwich from the year 1886 to 1901, and this table will answer for some years beyond that period, without any material error. This declination may be reduced to any other meridian in the following manner: Take from the table the declination of the same date as the local date and mark it + when north and - when south, and apply a correction equal to the "difference for one hour," multiplied by the hours and part of an hour of the longitude, adding or subtracting the correction as the sign in the table indicates; for a time after noon if the longitude is west, for a time before noon if the longitude is east.

EXAMPLE. At a place in longitude 81° 15′ W. on April 15, 1887, find the declination. Longitude 81° 15′ W. $= + 5^{\text{h}}.42$.

Had this longitude been east, we should get, longitude 81° 15' E. = -5° .42.

To find the declination for a given mean time at a given place proceed as follows: From the given mean time find the astronomical time, and the corresponding Greenwich date. Take from the table the declination for the nearest preceding mean time date, and the corresponding difference for one hour, noting the sign of each. Multiply the difference for one hour by the hours and parts of an hour of the remaining Greenwich time, and apply the correction according to the signs, adding if they are alike, and subtracting if they are unlike. If the given Greenwich time is nearer a following than a preceding date, it may be convenient to interpolate back from the following date.

EXAMPLE. At a given place in longitude 81° 15' W. on April 15, 1887, 10 A.M., find the declination.

Local astronomical time 14^d 22^h 00^m Longitude + 5 25
Greenwich mean time 15 3 25

Table IV contains the equation of time for every noon at Greenwich, and is to be reduced to any other hour by means of Table IVa. Thus, suppose the equation of time was required for Feb. 21, 1888, at 10 a.m., corresponding to Feb. 20th, 22 hours, Table IV gives the equation of time for Feb. 20th, 14^m 00^s, and for the 21st, 13^m 53^s; the difference between the two is a daily decrease of 7^s. Now enter Table IVa, and with 7 at the top and 22 at the side, the corresponding 6 in the column is the number of seconds to subtract from 14^m 00^s to give the required equation of time, 13^m 54^s. This 6 seconds would have been added had the equation of time been increasing. The equation of time thus found is to be applied to the apparent time, as stated at the head of the column in Table IV. To obtain the apparent time from the mean time, the equation of time is applied opposite to the heading in Table IV.

Table V contains the quantities that are convenient for finding the time, or the total error of the compass, by an altitude of the sun. To find the sine, secant, etc., for the degrees, minutes, and seconds of the date occurring in the problems, look for the degrees at the bottom of the page when

between 45° and 185°, otherwise at the top, the minutes being found in the column marked M., which stands on the side of the page on which the degrees are marked; and if the degrees are found at the top, the names, hour, sine, secant, etc., must also be found at the top; and if the degrees are found at the bottom, the names, hour, sine, secant, etc., must be found at the bottom. Opposite to the minutes will be found the sine, secant, etc., in the columns marked sine, secant, etc., respectively. Now, with the number of seconds in the left-hand column under M., take out the number in the nearest column marked "Diff.," which add to the sine, secant, etc., if increasing, or subtract if decreasing.

Thus, to find the cosine of 80° 20′ 20″, with 80° at the top of the page and opposite to 20' under M. in the column marked cosine. will be found 9.93606. Now, with 20" in the left column of M., we find opposite in the nearest column of "Diff." the figure 2 to be subtracted from the cosine as it is decreasing, which gives the correct cosine, 9.98604. Should it be desired to find the degrees, minutes, and seconds corresponding to this cosine, we search in the column of cosines for the nearest figures to those given, which will be in the column under 30°, and opposite to the nearest number in the column M. corresponding to 30, will be found 20. Take the difference between the given number and the nearest in the column. which is 2. Now, with this 2, look in the nearest column of "Diff.," and as there are several numbers marked 2, take the middle one, opposite to which, in the left-hand column under M., will be found 16 or 30° 20' 16", sufficiently near for all practicable purposes.

The method of finding the hours, minutes, and seconds corresponding to the sine, etc., is fully given in the text on finding the longitude.

Table I. DIFFERENCE OF LATITUDE AND DEPARTURE, 1°-45°.

D	IFFI	EREI	NCE (OF L	ATI	rude	AND	DE	PARTU	JRE	FOR	. 1°.	
at.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	1
1. 0	0.0	61	61.0	1, I 1, 1	121	121.0	2. I	181	181.0	3. 2	241	241.0	7
2, 0	0.0	62	62.0		22	122, 0	2. 1	82	182. 0	3 2	43	242.0	١ ٠
3.0	0, 1	63	63.0	1. 1	23	123.0	2, 1	83 84 85 86	183.0	3.8	43	243.0	١ ٠
4.0	0.1	64	64.0	1, 1	24	124.0	2. 2	. **	184.0	3.2	44	244.0	٠
5. O	0.1	65	65.0	1.1	25	125.0	2.2	85	185. 0	3.2	45 46	245.0	١.
6,0	0.1	66	66.0	1, 2	26	126.0	2, 2	86	186. 0	3. 2	46	245.0	
Z: 0	0.1	67	67.0	1.2	27	127.0	2, 2	87 88	187. 0	3-3	47	247.0	١.
8.0	0.1	68	68.0	1.2	28	128.0	2, 2		188. o	3.3	47 48	248.0	١.
0.0	0.2	I 6o∣	69.0	1.2	20	120.0	2.2	l &₀	189.0	3.3	40	249.0	١.

	1.0	0.0	61	61.0	1, 1	121	121.0	2. I	181	181.0	3. 2	241	241.0	4.2
3	2, 0	0.0	62	62.0	1. 1	22	122.0	2. 1	8a 83	182.0	3 2	43	242.0	4.8
3 4	3.0 4.0	0, I 0, I	63 64	63.0 64.0	I. I I. I	23	123. 0 124. 0	2. I 2. 2	83	183, 0 184, 0	3.2	43	243.0	4.2
1 3	\$. 0 6. 0	0. I	65	65. 0 66. 0	1. 1	25 20	125. 0 126. 0	2, 2	3438	185.0	3.2	45 46	245. 0 246. 0	43
ş	8.0	Q.I	66	66.0	1. 2	26	126.0	2, 2	86	186. 0	3. 2	46	240.0	4-3
7	7.0	0. I 0. I	67 68	67. o 68. o	I. 2 I. 2	27 28	127. 0 128. 0	2, 2	87 88	187. o 188. o	3. 3 3. 3	47 48	247. 0 248. 0	43 43
اۋا	9.0	0.2	60	69.0	1. 2	20	129.0	2.3	89	189.0	3.3	49	249.0	43
10	10.0	0, 2	70	70.0	1, 2	30	130.0	2, 3	9ó	190.0	3.3	50	250, 0	4.4
11	11.0	0. 2	71	71.0	1.2	131	131.0	2, 3	191	191.0	3-3	25I 52	251.0	44
12 13	12.0 13.0	0.2	72 73	72. 0 73. 0	1. 3 1. 3	32 33	132. Q 133. O	2.3	92 93	192. 0 193. 0	3. 4 3. 4	53	252. 0 253. 0	44
14	14.0	0.2	74	74.0	1.3	34	134.0	2, 3	94	194.0	3.4	54	254.0	4.4
15 16	15.0	0.3	75	75. 0 76. 0	1. 3	35 36	135.0	2, 4	95 96	195.0	3.4	55 56	255. 0 256. 0	4.5
10	16.0	0.3	70	70.0	1.3	30	136.0	2.4	90	196. o 197. o	3. 4 3. 4	50	250.0	4.5 4.5
17	17. 0 18. 0	0.3	77 78	77. o 78. o	1.4	37 38	137. 0 138. 6	2.4	97 98	198.0	3-5	57 58	258.0	45
19	19.0	0.3	79	79.0 80.0	1.4	39	139.0	2.4	99	199.0	3. 5 3. 5	59	259.0	45
20	20.0	0.3		81.0	1.4	40	140, 0	2.4	102	200.0	3.5	261	260.0	4.5
2 [22	21.0 22.0	0.4	81 82	82,0	1.4	141	141. 0 142. 0	2. 5 2. 5	03	201. 0	3. 5 3. 5	62	261.0 262.0	i 6
23	23.0	0.4	81	83.0	1.4	43	143.0	2.5	03	203.0	3.5	63	261.0	L 6 I
24	24.0	0.4	84	84.0	1.5	44	144.0	2,5	04	204.0	3.6	64.I	264.0	4.6
25 26	25.0 20.0	0.4	85 86	85. o 86. o	1.5	45	145.0 146.0	25	oş oğ	205.0	3.6	65 66	265. 0 266. 0	4.6 4.6
27 28	27.0 28.0	0.5	87 88	87.0	1.5	13	147.0	2.6	97	207. 0	3.6 3.6	67 68	267. 0	47
		0. 5		88.o	1.5	48	148.0	2,6		208.0	3.6		268, o	4.7
29 30	30.0	0.5	89 90	89.0 90.0	1.6	49 50	149. 0 150. 0	2.6	10	209. 0 210. 0	3.6	69 70	269. 0 270. 0	4.7 4.7
31	31.0		91	91.0	1,6	151	151.0	2.6	211	211.0	3.7	271	271.0	4.7
32	32.0	0.5	92	92.0	1.6	52	152.0	2.7	12	212.0	3.7	72	272. 0	4.7
33	33.0	0.6 0.6	93	93.6	1.6	53	153.0	2.7	13	213.0	3.7 3.7 3.8 3.8 3.8	73	273.0	4.8 4.8
34	34.0	0.6	94	94.0	1.7	54	154.0	2.7	14	314.0	3.7	74	274. 0 275. 0	4.8
35 36	35.0 30.0	0.6	95 96	95.0 96.0	1. 7	55 56	155.0 156.0	2,7	15 16	215.0 216.0	3.8	75 76	275. 0 276. 0	4.8
37 38	37. 0 38. 0	0.6	97 98	97. 0 98. 0	1.7	57 58	157.0	2.7	17	217.0	3.8	77	277.0	4.8
30	30.0	0.7 0.7	99	59.0	1.7	1 %	150.0	2.8	19	210.0	3.8 3.8	70	278.0	4.9
40	40.0	0.7	100	100, 0	1.7	59	160.0	2,8	20	220, 0	3.8	79 80	270.0 280.0	49
41	41.0	0.7	101	101.0	1.8	161	161.0	2, 8	221	221.0	3.9	281	251.0	49
42	42.0	0.7 0.8	03	102.0	1.8	62 63	162. 0 163. 0	2. 8 2. 8	22	223.0	3.9 3.9	8a 83	282. 0 283. 0	4.9
43 44	43.0 44.0	a.8	2	104 0	1.8	I 64	164.0	2.0	1 24	224.0	3.9	82	284.0	4.9 5.0
45	45.0	0.8	ુ	105.0	1.8	65	165. 0 166. 0	2.9	25 26	225. 0 220. 0	3.9	84 85 86	284.0	5.0
46	46.0	0.8		106, 0 107. 0	1.8	66	166.0	2.9	26	220.0	3.9	86	286, o 287, o	5.0
47	47.0	0.8	27	108.0	1.9	67 68	167. 0 168. 0	2.9	27 28	227. 0 228. 0	4.0	87 88	288.o	1 60
49	49.0	0.9	99	109.0	1.9	69	169.0	2.9	29	229.0	4.0	89	289.0	5.0 5.1
50	50.0	0.9	10	110.0	1.9	70	170.0	3.0	30	230.0	4.0	90	290.0	5.1
51 52	51, 0 52, 0	0.9	111	111.0	1.9	72	171.0	3.0 3.0	231 32	231.0 232.0	4.0	291 92	291. 0 292. 0	5. 1 5. 1
5.3	53.0	وة	13	113.0	1.0	73	173.0	3.0	33	233.0	1 7	93	293.0	
54	54.0	0.9	14	114.0	2.0	74	174.0	3.0	34	834.0	4.1	94	294.0	5.1
55 56	55. 0 56. 0	1.0	15	115.0	2,0	75	175.0	3. I 3. I	35	235.0 236.0	4:	95 96	295.0 290.0	5. I 5. 2
57	57.0	1.0	17	117.0	2.0	7	177.0	3.1	37 38	237. 0 238. 0	1 7:	97	207.0	5.2
57 58	58.0	1.0		118.0	2.1	78	177.0	1.1		238.0	4.2	97 98	298.0	5.8
59	59.0	1.0	19	119.0	1 1 1 2 1	123	179. 0 180. 0	3.1	39	239. 0 240. 0	4.3	300	300.0	5.2 5.2
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Dist.	Dep.	Lat	Dist.	Dep.	Lat.	Dist.	Dep	Lat.	Dist.	Dep.	Let.	Dist.	Dep.	Lat.
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DIFFERENCE OF LATITUDE AND DEPARTURE FOR 2°.

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Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Let	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	1.0	0.0	61	61.0	2. 1	121	120.9	4.2	181	180.9	6.3	241	240.9	8.4
	- 3.0 3.0	a I	63	62. 0 63. 0	2. 2 2. 2	22	121. 9 122. 9	4-3	82	181. 9 182. 9	6.4	42	241.9	8.4
3 4	40	0.1	64	64.0	2.2	23 24	123.9	43	83 84	183.9	6.4	43 44	242.9 243.9	8.5
5	50	0.5	65 66	65.0 66.0	2.3	33	124.9	1 4 4	85 86	184.0	6.3		244.9	8. 5 8. 6
	ã.o	0.2	66	66.0	2.3	25 26	126. 9	4.4	86	185. 9	66566	45 46	245. 9 240. 8	8.6
7	7.0	0.3	67 68	67.0 68.0	2.3	27 28	126. 9	4.4	87 88	186. 9	6.5	47 48	246. 8	8, 6
و	9.0	0.3	69	69.0	2.4	20	127. 9 128. 9	4.5	89	187. 9 188. 9	6.6	48	247. 8 248. 8	8. 7 8. 7
10	10,0	0.3	70	70.0	2.4	30	129.9	1 2 2	90	189.9	6.6	49 50	249.8	8.7
11	11.0	0.4	71	71.0	2.5	131	130.9	45	191	190. 9	6.7	251	250. 8	8, 8
12	12. 0	0.4	72	72.0	2.5	32	131.9	40	92	191.9	6.7 6.8 6.8	52	251.8	8.8
13	13.0	0.5	73	73.0	2.5	33	132.9	4.6	93	192. 9	6.7	53 -	252. 8	8.8
14	P4.0	مة	74	74.0	2.6	34	133. 9	4.7	94	193. 9	0.8	54	253.8	8.9
15	16.0	0.5	75	75.0 76.0	2.7	35 36	134.9	47 47 48 48	95 96	194.9	6.8	55 56	254.8	8.9 8.9
17 18	17.0 18.0	1 0.6	77	77.0	2, 7	37	135. 9 136. 9	4.8	97 98	195. 9 196. 9	6.0	57	255. 8 256. 8	9.0
		0.6	78	78.0	2.7	37 38	137. 9 138. 9	4.8		197. 9 198. 9	6.0	57 58	257. 8 258. 8	9.0
19	19.0	0.7	72	79.0 80.0	3.8	39	138. 9	4.9	99	198.9	6.9	59	258.8	9.0
20	20.0	0.7	81	80. 0 81. 0	2.8	40	139.9	4.9	200	199.9	7.0	861	259.8	9. 1
21	21. 0 22. 0	0.7	82	81.0 82.0	2.8	43	140. 9 141. 9	4.9 5.0	201 02	200 9 201. 9	7.0	261 62	260. 8 261, 8	9. I 9. I
23	23 0	0.8	83	82.9	2.9	43	142.0	₹.0	03	202.9	7. 1	63	262. 8	9.1
24	24.0	0.8	8ă	82.0	8.9	44	142.9 143.9	5.0	04	203.9	7.1	64	262.8	9.2
25 26	25. 0 26. 0	0.9	85 86	84.0	2.0	45	144.9	5. 1 5. 1	95 96	204.9	7. 8	65 66	264.8	0.3
	26.0	0.9	80	85.9 86.9	3.0 3.0	146	145. 9 146. 9	5. 1	06	205.9	7. 2	66	265.8 266.8	9.3 9.3
27 28	27. 0 28. 0	1.0	87 88	87.9	3. 1	47	140.9	5. 1 5. 3	27	200.9	7.2	67 68	200.8	9.3
29	29.0	1.0	89	88.9	3. i	49	147. 9 148. 9	l €.a	9	207. 9	7.3 7.3	60	267. 8 268. 8	9.4
30	30.0	1,0	90	89.9	3. 1	50	149.9	5. 2	IÓ	239.9	7.3	70	269.8	9.4
31	31.0	1. 1	91	90.9	3. 2	151	150.9	5-3	211	210.9	7.4	271	270.8	9-5 9-5
32	32.0	1. 1	92	91.9	3. 2	52	151.9	5.3	12	211.9	7.4	72	271.8	9.5
33 34	33. 0 34. °	1.2	93 94	92. 9 93. 9	3.2	53 54	152. 9 153. 9	2.3	13 14	212.9	7.4	73	272. 8 273. 8	9.5
35	35.0	1. 2	95	94.9	2.3	33	144.0	5.3 5.4 5.4	iš	214.0	7.4	74 75 76	274.8	9.6
35 36	35. u 36. o	1.3	95 96	95.9 96.9	3- 3 3- 4	55 56	155. 9 156. 9	\$-4 \$-5	15 16	215. 9 216. 9	7.5	76	275.8 276.8	0.6
37 38	37. o 38. o	1.3	97	96.9	3-4	57 58	156.9	5-5	17 18	216.9	7. 6 7. 6	77 78	276.8	9.7
39	39.0	I. 3	98 99	97. 9 98. 9	3.4 3.5	50	157. 9 158. 9	5. 5 5. 5	19	217.9	7.6	70	277. 8 278. 8	9.7
40	40.0	1:4	100	99.9	3.5	59	159.9	5. 5 5. 6	20	219.9	7.7	79	279.8	0.8
41	41.0	1.4	101	100.9	25	161	160. 0	5.6	221	220. 9	7. 7	281	280. 8	9,8
42	42.0	I. 5	02	101.9	3.6	62	161.0	6.7	22	221.9	7.7	82	281.8	9.8
43	43.0	1.5	03	102, 9	3.5 3.6 3.6 3.7	63	162. 9	\$ 7 \$ 7 \$ 8	23	222. 9	7. 7 7. 7 7. 8 7. 8	83	282.8	9.9
44	44.0 45.0	1. § 1. 6	04 04	103.9	3.0	64	163. 9 164. 9	5.7	24	223.9 224.9	7.8	84 8c	283. 8 284. 8	9.9 9.9 10.0
45 46	46.0	1.6	05 06	105.0	2,7	65 66	165.9		25 26	225.0	7.0	85 86	284, 8	10.0
47 48	47.0	1.6	97 08	105. 9 100. 9	3.7 3.7 3.8	67 68	1 100. a	5.8 5.9	27 28	220.0	7.9 7.9	87 88	286.8	10.0
	45.0	1.7		107.9	3.8		167. 9 168. 9	5.9		227. 9 228. 9	8.0	88	287. 8 288. 8	10, 1
49 50	49. 0 50. 0	1.7	10	100.9	3.8	69 70	169.9	5.9 5.9	39 30	229.9	8.0	89 90	288. 8 289. 8	10. 1
51	51.0	1.8	111	110.0	3.9	171	170.0	6.0	231	230.9	8, 1	291	290. 8	10, 2
52	52. 0	1.8	12	111.9	3.9	72	171.9	6.0	32	231.0	8,1	92	291.8	10. 2
53 54	53.0	1.8	13	112.9	3.9	73	172.9	6.0	33	232.9	8. I 8. I	93	292. 8	10, 2
54	54.0	1.9	14	113.9	4.0	74	173.9	6.1	24	233.9	8.2	94	293.8	10. 3
55 56	55. 0 56. 0	1.9 2.0	15 16	114.9	4.0	75	174.9	6.1	35 36	234.9	8.2 8.2	95 96	294. 8	10. 3
57	57.0	2.0	17	110.9	40	77	175.9 176.9	6.2	37	235. 9 236. 9		97	295. 8 296. 8	10. 4
57 58	58.0	2.0	18	117. 0	4.1	77	177.9	6.2	37 38	237. 9	8.3 8.3	97 98	297. 8 298. 8	10.4
59	59. 0 60. 0	2. I	19	118.9	4.8	79	178.9	6.8	39	237. 9 238. 9	8.3	99	298.8	10.4
∞	60.0	2.1	20	119.9	4.8	80	179.9	6.3	40	239. 9	8.4	300	299, 8	10. 5
Diet.	Dep.	Let.	Dist.	Dep.	Lat	Dist.	Dep.	Lat	Dist.	Dep.	Lat	Dist.	Dep.	Lat.
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DIFFERENCE OF LATITUDE AND DEPARTURE FOR 3°.

1.	Dist.	Lat	Dep.	Dist.	Let	Dep.	Dist.	Lat	Dep.	Dist	Lat	Dep.	Dist.	Lat	Dep.
2 2 0 0.1 62 66.9 3.2 22 121.8 6.4 83 181.8 9.5 42 241.7 12.7 12.7 4 4.0 0.2 64 63.9 3.3 23 122.8 6.4 83 181.8 9.5 42 241.7 12.7 12.5 5.5 0.0 3.3 65 65.9 3.5 25 125.8 6.5 84 183.7 9.6 44 243.7 12.5 6.6 0.6 0.3 66 65.9 3.5 25 125.8 6.5 85 183.7 9.6 44 243.7 12.8 8 8.0 0.4 68 67.9 3.5 25 125.8 6.6 86 183.7 9.7 45 244.7 12.8 8 8.0 0.4 68 67.9 3.6 28 127.8 6.7 88 187.7 9.8 48 247.7 12.9 9.9 0.5 69 68.9 3.6 28 127.8 6.7 88 187.7 9.8 48 247.7 13.0 10 10.0 0.5 70 68.9 3.6 28 127.8 6.7 88 187.7 9.8 48 247.7 13.0 10 10.0 0.5 70 68.9 3.6 28 127.8 6.7 9.8 188.7 9.9 40 244.7 13.0 10 10.0 0.5 70 68.9 3.6 28 127.8 6.7 9.8 188.7 9.9 40 244.7 13.0 10 12.0 0.6 77 70.9 3.7 131 131 130.8 6.8 89 188.7 9.9 10 250.7 13.1 12 12.0 0.6 77 77.9 3.8 32 131.8 6.9 12.8 187.7 18.2 18.7 19.7 10.0 52 249.7 13.1 12 12.0 0.6 77 77.9 3.8 32 131.8 6.9 12.8 18.7 19.9 19.7 10.0 52 249.7 13.1 12 12.0 0.6 77 74 73.9 3.8 33 132.8 7.0 93 191.7 10.0 52 249.7 13.1 13 13.0 0.7 73.7 19.9 3.8 33 132.8 7.0 93 192.7 10.5 53 183.7 13.2 13.1 13.1 13.1 13.1 13.1 13.1 13.1	Dist.		200	-		Deb.	Dia.					Deb.	Dist.	LAL	_
3 0 0 0 6 63 60 0 3 0 3 0 3 123.8 8 6.5 8 83 182.7 9.6 44 241.7 12.8 6.5 0 0.3 65 64 9 3.4 22.1 124.8 6.5 85 184.7 9.7 45 244.7 12.8 6 6.6 8.7 12.8 183.7 9.6 44 241.7 12.8 12.8 12.8 12.8 12.8 12.8 12.8 12.8						3.2		120, 8	6.3		180, 8	9.5			
4 4.0 0.2 64 63.9 3.3 24 123.8 6.5 84 183.7 9.6 44 243.7 12.8 6.6 0.0 0.3 66 65.9 3.5 27 126.8 6.5 86 185.7 9.7 45 245.7 12.9 8 8.0 0.4 68 67.9 3.5 27 126.8 6.6 86 185.7 9.7 45 245.7 12.9 8 8.0 0.4 68 67.9 3.6 28 127.8 6.6 8.6 185.7 9.7 45 245.7 12.9 9.0 0.5 66 68.9 3.6 29 128.8 6.6 8 91 185.7 9.8 47 247.7 13.0 10.1 0.0 0.5 70 65.9 3.7 30 129.8 6.68 9.8 188.7 9.9 40 247.7 13.0 10.1 0.0 0.5 70 65.9 3.7 30 129.8 6.68 9.8 188.7 9.9 40 247.7 13.0 11.0 0.5 17.7 20.9 3.7 31 13.1 3.0 0.6 71 77.9 3.7 13.1 13.8 6.9 92 191.7 10.0 25 247.7 13.0 13.1 13.0 0.6 71 77.9 3.7 13.1 13.8 6.9 92 191.7 10.0 25 25.7 13.2 13.1 13.0 0.7 73.7 2.9 3.8 32 131.8 6.9 92 191.7 10.0 25 25.5 13.7 13.2 13.1 0.0 0.7 73.7 2.9 3.8 33 132.8 7.0 93 192.7 10.1 153 25.7 13.2 13.1 13.0 0.7 73.7 7.9 3.8 33 132.8 7.0 93 192.7 10.1 153 25.7 13.2 13.1 13.0 0.7 73.7 7.9 3.8 33 132.8 7.0 93 192.7 10.1 153 25.7 13.2 13.1 10.0 0.8 77.7 7.9 3.0 3.5 13.8 7.0 19.1 190.7 10.2 25 25.7 13.3 15.1 15.0 0.8 77.7 7.9 4.0 30 135.8 7.1 97 190.7 10.3 55 25.7 13.3 15.1 10.0 0.8 77.7 7.9 4.0 30 135.8 7.1 97 190.7 10.3 55 25.6 13.5 15.0 0.9 77.7 7.9 4.0 30 135.8 7.1 97 190.7 10.3 55 25.6 13.5 13.5 15.0 0.9 77.7 7.9 4.1 3.8 13.8 7.2 97 190.7 10.3 55 25.6 13.5 13.5 13.0 0.9 7.7 7.9 4.1 3.8 13.8 7.2 99 190.7 10.3 55 25.6 13.5 13.5 13.0 0.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7					62.0			121.0	6.4	82	182.7	2.5		241. 7	
7	4	4.0	0, 2	64	63.9	3-3	24	123.8	16.5	84	182.7	9.6	44	243. 7	12.8
7	5	5.0		25	64.9	3.4	25	124.8	6.5	35	184.7	9.7	45	244.7	
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26. 0	24	24.0	1.3	I 8∡	83.9	4.4	44	143. 8	7. \$	04	203. 7	10. 7	64	263.6	13.0
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22 28.0 1.5 83 87.9 4.6 43 147.8 7.7 05 207.7 10.9 68 207.0 14.9 29 29.0 1.5 89 88.9 4.7 49 148.8 7.8 09 208.7 10.9 69 206.6 14.1 20.9 69 206.6 14.1 20.9 11.0 270 265.6 14.1 20.9 20.0 20.8 1.0 96 20.0 20.8 20.9 11.0 270 265.6 14.1 20.0 27.0 11.0 270 265.6 14.1 20.0 27.0 11.0 270 265.6 14.2 20.0 27.0 11.0 270 265.6 14.2 20.0 27.0 11.0 270 265.6 14.2 20.0 27.0 11.0 270 265.6 14.2 20.0 27.0 11.0 270 270.6 14.2 27.0 11.0 270.		27.0	1.4	87	86.9	4.6	47	146.8	7.7	07	206.7	10, 8	67	266.6	14.0
39 30.0 1.6 90 89.9 4.7 50 149.8 7.9 10 200.7 11.0 270 269.6 14.1 31 31.0 1.6 91 99.9 4.8 151 151.8 8.0 13 211.7 11.1 272 271.6 14.2 33 33.0 1.7 93 93.9 9.9 9.4 153.8 8.0 13 211.7 11.1 72 272.6 14.3 34 34.0 1.8 99.9 9.9 9.4 153.8 8.1 13 212.7 11.2 72 72.6 14.3 35 35.0 1.8 99.9 9.9 9.5 155 154.8 8.1 15 214.7 11.2 72 72.6 14.3 37 9.0 1.9 99.9 9.5 5.0 155 154.8 8.1 11 211.7 11.3 77 27.6 14.2 38 </td <td></td> <td></td> <td>1.5</td> <td></td> <td>87.9</td> <td>4.6</td> <td></td> <td>147.8</td> <td>7. 7</td> <td></td> <td>207. 7</td> <td>10.9</td> <td></td> <td>267.6</td> <td>14.0</td>			1.5		87.9	4.6		147.8	7. 7		207. 7	10.9		267.6	14.0
31 31.0 1.6 91 90.9 4.8 151 150.8 7.9 211 210.7 11.0 271 270.6 14.2 233 33.0 1.7 93 99.9 4.8 52 151.8 8.0 13 211.7 11.1 172 271.6 14.2 33 33.0 1.7 93 99.9 4.9 53 152.8 8.0 13 211.7 11.1 172 271.6 14.3 35 35.0 1.8 95 94.9 5.0 55 153.8 8.1 15 214.7 11.2 74 273.6 14.3 35 35.0 1.8 95 94.9 5.0 55 153.8 8.1 15 214.7 11.3 77 275.6 14.3 36 35.0 1.9 90 95.9 5.0 55 153.8 8.1 15 214.7 11.3 77 275.6 14.4 31.7 11.3 75 274.6 14.5 27.5 27.5 27.5 27.5 27.5 27.5 27.5 27			1.8		80.9			140.8	7.0		200. 7	11.0			14.1
33 3.0 1.7 93 6.9.4 9 53 152.8 8.0 13 212.7 11.1 P 73 275.6 14.3 35 35.0 1.8 95 94.9 5.0 55 154.8 8.1 15 214.7 11.2 74 275.6 14.3 35 35.0 1.8 95 94.9 5.0 55 154.8 8.1 15 214.7 11.3 77 275.6 14.4 315.7 11.2 74 275.6 14.4 35.5 35.0 1.9 90 95.9 5.0 55 155.8 8.2 17 21.5 214.7 11.3 77 275.6 14.4 315.7 11.3 75 274.6 14.4 315.7 11.3 75 274.6 14.4 315.7 11.3 75 274.6 14.4 315.7 11.3 75 275.6 14.4 315.7 11.3 75 274.6 14.4 315.7 11.3 75 274.6 14.4 315.7 11.3 75 275.6 14.4 315.7 11.3 75 275.6 14.4 315.7 11.3 75 275.6 14.4 315.7 11.3 75 275.6 14.4 315.7 11.3 75 275.6 14.4 315.7 11.4 75 275.6 14.4 315.7 11.4 75 275.6 14.4 315.7 11.4 75 275.6 14.4 315.7 11.4 75 275.6 14.4 315.7 11.4 75 275.6 14.4 315.7 11.4 75 275.6 14.4 315.7 11.4 75 275.6 14.4 315.7 11.4 75 275.6 14.4 315.7 11.4 75 275.6 14.5 315.7 11.4 315.7 11.4 315.7 11.4 315.7 11.5 315.7 11.4 315.7 11.5 315	31	31.0	1.6	91	90.9	48	151	150.8			210. 7		271	270.6	14. 2
34 34 0 1.8 94 93.9 4.9 54 153.8 8.1 14 213.7 11.2 17 27.6 14.3 153 153.5 13.6 1.8 95 94.9 5.0 55 154.8 8.1 15 214.7 11.3 17, 27.6 14.4 13.3 17, 27.6 14.4 13.3 17, 27.6 14.4 13.3 17, 27.6 14.5 14.5 11.3 17, 27.6 14.5 14.5 13.3 17, 27.6 14.5 14.5 13.3 17, 27.6 14.5 14.5 13.5 13.5 13.5 13.5 13.5 13.5 13.5 13	32		1.7		91.9	4.8		151.8	8.0					271.6	14.2
33 3.0 1.8 95 94-9 5.0 5 154-8 8.1 15 214-7 11.3 77 27.6 14-6 36 30.0 1.9 90 95.9 5.0 55 155.8 8.2 17 215.7 11.3 77 27.5 6 14-6 37 36.9 1.9 97 95.9 5.1 55 155.8 8.2 17 215.7 11.3 77 27.5 6 14-5 38 37.9 2.0 98 97.9 5.1 58 157.8 8.3 18 217.7 11.4 77 27.5 6 14-5 39 38.9 2.0 99 95.9 5.2 50 158.8 8.2 17 21.5 7 11.4 77 27.5 6 14-5 40 39.9 2.1 100 95.9 5.2 50 158.8 8.3 19 215.7 11.4 77 27.5 6 14-5 41 40.9 2.1 101 100.9 5.3 161 160.8 8.4 221 220.7 11.6 28 12.5 6 14-6 42 41.9 2.2 101 101.9 5.3 62 161.8 8.5 22 221.7 11.6 28 12.6 6 14-8 43 42.9 2.3 03 102.9 5.4 63 162.8 8.5 22 221.7 11.6 28 12.6 6 14-8 44 43.9 2.3 04 103.9 5.4 64 163.8 8.5 23 222.7 11.6 28 12.6 6 14-8 44 43.9 2.4 05 104.9 5.5 66 165.8 8.5 22 222.7 11.7 83 28.6 6 14-8 45 44.9 2.4 05 104.9 5.5 66 165.8 8.7 222.7 11.8 86 28.6 6 15.0 45 44.9 2.4 05 105.9 5.5 66 165.8 8.7 222.7 11.8 86 28.6 6 15.0 47 46.9 2.5 07 105.9 5.7 68 166.8 8.7 222.7 11.8 86 28.6 6 15.0 48 47.9 2.5 08 105.9 5.5 66 165.8 8.7 222.7 11.8 86 28.6 6 15.0 49.9 2.6 10 105.9 5.5 66 165.8 8.8 29 222.7 11.9 88 28.6 6 15.1 49 40.9 2.6 10 105.9 5.5 66 165.8 8.8 29 222.7 11.9 88 28.6 6 15.1 51 50.9 8.7 111 110.8 5.8 171 170.8 8.8 292.7 12.0 90 289.6 6 15.2 51 50.9 8.7 111 110.8 5.8 171 170.8 8.9 231 231.7 12.1 291 290.6 15.3 51 50.9 8.7 111 110.8 5.8 171 170.8 8.9 231 231.7 12.1 291 290.6 15.3 51 50.9 1.7 12 11 11.8 5.9 73 172.8 9.0 33 23.7 12.1 291 290.6 15.3 51 50.9 1.7 12 11.8 5.9 73 172.8 9.0 33 23.7 12.1 291 290.6 15.3 51 50.9 1.7 111 110.8 5.8 171 170.8 8.9 231 231.7 12.2 39 290.6 15.3 51 50.9 2.7 111 11.8 5.9 73 172.8 9.1 33 231.7 12.2 39 290.6 15.3 51 50.9 3.0 17 111.8 5.9 73 172.8 9.1 33 231.7 12.2 39 290.6 15.3 51 50.9 3.0 17 111.8 5.9 73 172.8 9.1 33 231.7 12.2 39 290.6 15.5 51 50.9 3.1 19 18.8 6.2 79 175.8 9.3 37 235.7 12.4 99 290.6 15.5 51 55.9 3.1 19 11.8 6.2 79 175.8 9.3 37 235.7 12.4 99 290.6 15.5 52 50.9 3.1 120 118.8 6.2 79 177.8 9.3 37 235.7 12.4 99 290.6 15.5 52 50.9 3.1 120 118.8 6.2 79 177.8 9.4 40 239.7 12.5 98 296.6 15.5 52 50.9 3.1 120 118.8 6.2 79 177.8 9.4 40 239.7 12.5 98	33	34.0	1.8		93.9	4.9	54	152.8	8, 1	14	213.7	11.2	74	273.6	
37 36.9 1.9 97 96.9 5.1 5 150.8 8.2 17 18.0.7 11.4 77 276.0 14.5 38 38.3 18 210.7 11.4 77 276.0 14.5 38 38.3 18 210.7 11.4 78 277.0 14.5 39 38.9 2.0 99 96.9 5.2 50 158.8 8.3 19 218.7 11.5 70 278.6 14.5 39 38.9 2.0 199.9 5.2 50 158.8 8.4 221 220.7 11.5 20 278.6 14.0 14.0 14.0 19.2 11.1 10.1 100.9 5.3 161 160.8 8.5 122 220.7 11.6 281 280.6 14.0 14.0 14.0 19.2 11.5 10.1 10.1 10.1 10.1 10.1 10.1 10.1	35	35.0	1.8	95	94.9	5.0	55	154.8		15	214.7	11.3	75	274.6	
38 37.9 2.0 98 97.9 5.1 58 157.8 8 33 18 217.7 11.4 78 277.6 14.5 49 39.9 2.0 99 98.9 5.2 59 158.8 8.3 18 217.7 11.5 70 276.6 14.6 40 39.9 2.1 107 100.9 5.3 60 159.8 8.4 20 219.7 11.5 20 276.6 14.7 21 41.9 2.2 02 101.9 5.3 62 161.8 8.5 22 22 221.7 11.6 281 280.6 14.7 21 41.9 2.2 02 101.9 5.3 62 161.8 8.5 22 22 221.7 11.6 281 280.6 14.7 241.9 2.2 02 101.9 5.3 62 161.8 8.5 22 22 221.7 11.6 281 282.6 14.8 44 43.9 2.3 03 102.9 5.4 63 162.8 8.5 22 221.7 11.6 281 282.6 14.8 44 43.9 2.3 04 103.9 5.4 63 162.8 8.5 22 221.7 11.6 281 282.6 14.8 44 43.9 2.3 04 103.9 5.4 64 163.8 8.6 24 223.7 11.7 83 283.6 14.8 44 43.9 2.4 05 104.9 5.5 65 164.8 8.6 24 223.7 11.7 83 283.6 14.9 45 44.9 2.4 05 104.9 5.5 65 164.8 8.6 24 223.7 11.9 85 283.6 14.9 44 47.9 2.5 08 107.9 5.7 68 167.8 8.6 27 222.7 11.8 86 285.6 15.0 48 47.9 2.5 08 107.9 5.7 68 167.8 8.7 20 225.7 11.8 86 285.6 15.0 09.49 9 2.6 09 108.9 5.7 69 168.8 8.7 20 225.7 11.9 88 287.6 15.0 09.49 9 2.6 10 109.8 5.8 70 169.8 8.8 28 22.27, 7 11.9 88 287.6 15.1 50.9 49.9 2.6 10 109.8 5.8 70 169.8 8.8 29 228.7 12.0 80 288.6 15.1 50.9 27 12 11.8 5.9 9 72 171.8 9.0 231 230.7 12.0 80 288.6 15.1 50.9 27 12 11.8 5.9 9 72 171.8 9.1 32 230.7 12.0 90 288.6 15.5 54.9 2.8 11.1 10.8 5.9 9 72 171.8 9.1 32 230.7 12.0 90 288.6 15.3 53 52.9 2.8 13 12.8 5.9 72 171.8 9.1 32 230.7 12.0 90 289.6 15.5 54.9 2.9 16 11.8 6.1 70 175.8 9.2 30 232.7 12.0 30 289.6 15.3 55 54.9 2.9 10 11.8 6.1 70 175.8 9.2 30 235.7 12.2 90 291.6 15.3 55 54.9 2.9 10 11.8 6.1 70 175.8 9.2 30 235.7 12.4 90 291.6 15.5 55 54.9 2.9 10 11.8 6.2 79 171.8 9.2 30 235.7 12.4 90 291.6 15.5 55 54.9 3.0 18 117.8 6.2 79 177.8 9.3 38 233.7 7 12.2 99 291.6 15.5 55 54.9 3.0 18 117.8 6.2 79 177.8 9.3 38 233.7 7 12.2 99 291.6 15.5 55 54.9 3.0 18 117.8 6.2 79 177.8 9.3 38 233.7 7 12.2 99 291.6 15.5 55 54.9 3.0 18 117.8 6.2 79 177.8 9.3 38 233.7 7 12.2 99 291.6 15.5 55 54.9 3.0 18 117.8 6.2 79 177.8 9.3 38 233.7 7 12.2 99 295.6 15.5 55 54.9 3.1 19 11.8 6.2 79 177.8 9.3 38 233.7 7 12.2 99 295.6 15.5 55 54.9 3.1 19 11.8 6.2 79 177.8 9.3 38 233.7 7 12.	30	30. 0 26. 0		%°	95.9	5.0	50	155.8			215.7	11.3	70	275.6	
39 38.9 2.0 99 98.9 5.2 59 153.8 8.3 19 218.7 11.5 70 279.6 14.0 40.9 2.1 101 100.9 5.3 101 150.8 8.4 221 220.7 11.5 28 279.6 14.0 40.9 2.1 101 100.9 5.3 101 150.8 8.5 22 220.7 11.6 281 286.6 14.5 43 42.9 2.3 03 102.9 5.4 63 162.8 8.5 22 220.7 11.6 281 286.6 14.5 44.9 2.4 05 10.9 5.5 62 104.8 8.5 22 220.7 11.6 28 281.6 14.5 44.9 2.4 05 10.9 5.5 62 104.8 8.6 25 224.7 11.6 82 281.6 14.5 44.9 2.4 05 10.9 5.5 65 104.8 8.6 25 224.7 11.7 84 285.6 14.9 40 45.9 2.4 05 10.9 5.5 66 165.8 8.7 22.2 22.7 11.7 84 285.6 14.9 40.9 5.5 06 165.8 8.7 22.2 22.7 11.8 86 285.6 14.9 40.9 2.5 07 105.9 5.5 66 165.8 8.7 22.2 22.7 11.8 86 285.6 14.9 40.9 2.5 07 105.9 5.5 66 165.8 8.7 22.2 22.7 11.8 86 285.6 15.1 10.0 10.0 10.0 10.0 10.0 10.0 10.0	38	37.9	2.0		97.9	5. I	58	157. 8	8.		217.7	11.4	78	277.6	14.5
41 40.9 2.1 101 100.9 5.3 161 160.8 8.4 221 220.7 11.6 281 250.6 14.5 41.9 2.2 03 101.9 5.3 62 161.8 8.5 22 23.7 11.6 281 250.6 14.5 43 42.9 2.3 03 102.9 5.4 63 162.3 8.5 22 23.7 11.7 83 256.6 14.8 44 43.9 2.3 04 103.9 5.4 64 163.8 8.6 24 223.7 11.7 83 256.6 14.8 44 43.9 2.4 05 104.9 5.5 65 164.8 8.6 24 223.7 11.7 83 25.6 14.8 45 45.9 2.4 05 105.9 5.5 65 164.8 8.6 24 223.7 11.8 85 25.6 16.9 16.9 16.9 16.9 16.9 16.9 16.9 16	39	38.9			98.9	5.2	59	158.8	8.3			11.5	79	278.6	
23 41.9 2.3 03 101.9 5.3 62 151.8 8.5 22 221.7 11.6 83 281.6 14.8 43 42.9 2.3 03 102.9 5.4 63 163.8 8.5 23 222.7 11.7 83 283.6 14.8 44 43.9 2.3 04 103.9 5.4 64 163.8 8.6 24 223.7 11.7 83 283.6 14.9 45 44.9 2.4 05 104.9 5.5 65 164.8 8.6 24 223.7 11.7 83 283.6 14.9 45 45.9 2.4 06 105.9 5.5 66 165.8 8.7 26 222.7 11.8 85 283.6 14.9 47 45.9 2.5 08 107.9 5.7 68 167.8 8.7 26 222.7 11.8 85 283.6 15.0 48 47.9 2.5 08 107.9 5.7 68 167.8 8.7 26 222.7 11.8 85 283.6 15.0 94.9 2.6 09 108.9 5.7 69 168.8 8.7 26 222.7 11.9 87 285.6 15.0 94.9 2.6 09 108.9 5.7 69 168.8 8.8 28 22.7 11.9 87 285.6 15.0 94.9 2.6 09 108.9 5.7 69 168.8 8.8 28 22.7 11.9 88 287.6 15.1 95.0 49.9 2.6 09 108.9 5.7 69 168.8 8.8 29 282.7 12.0 89 285.6 15.1 15.0 9.7 11.9 11.8 5.9 9 12.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15									8.4						
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50 49.9 2.6 10 109.8 5.8 70 169.8 8.9 30 229.7 12.0 90 289.0 15.2 15.0 90 289.0 15.2 15.0 90 289.0 15.2 15.0 90 289.0 15.2 15.0 90 289.0 15.2 15.0 90 2.7 12 11.8 5.9 72 171.8 9.0 32 23.1 23.0 7 12.1 291 292.6 15.3 15.3 52.9 2.8 13 122.8 5.9 72 171.8 9.1 34 233.1 7 12.1 291 292.6 15.3 15.3 52.9 2.8 13 122.8 5.9 73 172.8 9.1 34 233.7 12.2 93 294.6 15.3 15.5 4.9 2.9 1.5 14.8 6.0 74 173.8 9.1 34 233.7 12.2 93 294.6 15.3 15.5 4.9 2.9 15.1 14.8 6.0 75 174.8 9.2 35 234.7 12.2 93 294.6 15.4 15.5 4.9 2.9 15.1 14.8 6.0 75 174.8 9.2 35 234.7 12.3 95 294.6 15.4 15.5 4.9 2.9 15.7 15.8 15.2 15.2 15.2 15.2 15.2 15.2 15.2 15.2		42.9	2.3		102.9	5.4	63	162,8	8.5			11.7	83	282. 6	14.8
50 49.9 2.6 10 109.8 5.8 70 169.8 8.9 30 229.7 12.0 90 289.0 15.2 15.0 90 289.0 15.2 15.0 90 289.0 15.2 15.0 90 289.0 15.2 15.0 90 289.0 15.2 15.0 90 2.7 12 11.8 5.9 72 171.8 9.0 32 23.1 23.0 7 12.1 291 292.6 15.3 15.3 52.9 2.8 13 122.8 5.9 72 171.8 9.1 34 233.1 7 12.1 291 292.6 15.3 15.3 52.9 2.8 13 122.8 5.9 73 172.8 9.1 34 233.7 12.2 93 294.6 15.3 15.5 4.9 2.9 1.5 14.8 6.0 74 173.8 9.1 34 233.7 12.2 93 294.6 15.3 15.5 4.9 2.9 15.1 14.8 6.0 75 174.8 9.2 35 234.7 12.2 93 294.6 15.4 15.5 4.9 2.9 15.1 14.8 6.0 75 174.8 9.2 35 234.7 12.3 95 294.6 15.4 15.5 4.9 2.9 15.7 15.8 15.2 15.2 15.2 15.2 15.2 15.2 15.2 15.2	45	44.9	2.4	%	104.9	3.4	65	164.8	I 8.6	25	224. 7	11.8	85	284. 6	14.9
50 49.9 2.6 10 109.8 5.8 70 169.8 8.9 30 229.7 12.0 90 289.0 15.2 15.0 90 289.0 15.2 15.0 90 289.0 15.2 15.0 90 289.0 15.2 15.0 90 289.0 15.2 15.0 90 2.7 12 11.8 5.9 72 171.8 9.0 32 23.1 23.0 7 12.1 291 292.6 15.3 15.3 52.9 2.8 13 122.8 5.9 72 171.8 9.1 34 233.1 7 12.1 291 292.6 15.3 15.3 52.9 2.8 13 122.8 5.9 73 172.8 9.1 34 233.7 12.2 93 294.6 15.3 15.5 4.9 2.9 1.5 14.8 6.0 74 173.8 9.1 34 233.7 12.2 93 294.6 15.3 15.5 4.9 2.9 15.1 14.8 6.0 75 174.8 9.2 35 234.7 12.2 93 294.6 15.4 15.5 4.9 2.9 15.1 14.8 6.0 75 174.8 9.2 35 234.7 12.3 95 294.6 15.4 15.5 4.9 2.9 15.7 15.8 15.2 15.2 15.2 15.2 15.2 15.2 15.2 15.2	46	45.9	2.4	oč	105.9	5. Ş	66	165.8	8.7	26	225. 7	11.8	86	285, 6	15.0
50 49.9 2.6 10 109.8 5.8 70 169.8 8.9 30 229.7 12.0 90 289.0 15.2 15.0 90 289.0 15.2 15.0 90 289.0 15.2 15.0 90 289.0 15.2 15.0 90 289.0 15.2 15.0 90 2.7 12 11.8 5.9 72 171.8 9.0 32 23.1 23.0 7 12.1 291 292.6 15.3 15.3 52.9 2.8 13 122.8 5.9 72 171.8 9.1 34 233.1 7 12.1 291 292.6 15.3 15.3 52.9 2.8 13 122.8 5.9 73 172.8 9.1 34 233.7 12.2 93 294.6 15.3 15.5 4.9 2.9 1.5 14.8 6.0 74 173.8 9.1 34 233.7 12.2 93 294.6 15.3 15.5 4.9 2.9 15.1 14.8 6.0 75 174.8 9.2 35 234.7 12.2 93 294.6 15.4 15.5 4.9 2.9 15.1 14.8 6.0 75 174.8 9.2 35 234.7 12.3 95 294.6 15.4 15.5 4.9 2.9 15.7 15.8 15.2 15.2 15.2 15.2 15.2 15.2 15.2 15.2	47	47.0	2,5	1 %	100.9	5.0	87	167.8	1 8 8	27	220. 7		88	287. 6	
50 49.9 2.6 10 109.8 5.8 70 169.8 8.9 30 229.7 12.0 90 289.0 15.2 15.0 90 289.0 15.2 15.0 90 289.0 15.2 15.0 90 289.0 15.2 15.0 90 289.0 15.2 15.0 90 2.7 12 11.8 5.9 72 171.8 9.0 32 23.1 23.0 7 12.1 291 292.6 15.3 15.3 52.9 2.8 13 122.8 5.9 72 171.8 9.1 34 233.1 7 12.1 291 292.6 15.3 15.3 52.9 2.8 13 122.8 5.9 73 172.8 9.1 34 233.7 12.2 93 294.6 15.3 15.5 4.9 2.9 1.5 14.8 6.0 74 173.8 9.1 34 233.7 12.2 93 294.6 15.3 15.5 4.9 2.9 15.1 14.8 6.0 75 174.8 9.2 35 234.7 12.2 93 294.6 15.4 15.5 4.9 2.9 15.1 14.8 6.0 75 174.8 9.2 35 234.7 12.3 95 294.6 15.4 15.5 4.9 2.9 15.7 15.8 15.2 15.2 15.2 15.2 15.2 15.2 15.2 15.2		48.9	2.6	9		5.7	69	168.8	8.8	29	228.7	12.0	89	288. 6	15. I
51 9 2, 7 12 111.8 5.9 72 171.8 9.10 32 231.7 12.1 93 291.6 15.3 53 52.9 2.8 13 112.8 5.9 73 172.8 9.1 33 32.7 12.2 93 292.6 15.3 54 53.9 2.8 14 113.8 6.0 74 173.8 9.1 34 233.7 12.2 94 293.6 15.3 55 4.9 2.9 15 114.8 6.0 75 174.8 9.2 35 234.7 12.3 95 294.6 15.4 55 54.9 2.9 16 115.8 6.1 76 175.8 9.2 36 235.7 12.4 96 293.6 15.4 55 55.9 2.9 16 115.8 6.1 76 175.8 9.2 36 235.7 12.4 96 295.6 15.5 57 56.9 3.0 18 117.8 6.1 77 175.8 9.3 38 235.7 12.4 95 295.6 15.5 58 57.9 3.0 18 117.8 6.2 78 177.8 9.3 38 233.7 12.4 97 295.6 15.5 59 23.9 3.1 19 118.8 6.2 78 177.8 9.4 38 23.3 235.7 12.5 98 297.6 15.5 60 59.9 3.1 19 118.8 6.2 78 177.8 9.4 40 239.7 12.5 98 297.6 15.7 05 25.9 3.1 19 118.8 6.3 80 179.8 9.4 40 239.7 12.5 99 295.6 15.7 05.8 05.9 13.1 20 119.8 6.3 80 179.8 9.4 40 239.7 12.6 300 299.6 15.7 05.1						5.8			8,9						
55	51		2.7			5.8		170.8	8.9				291		
55	53	52.9	2.8		112,8	5.9	73	172.8	9.1	33	232, 7	12, 2	93	292.6	15, 3
57 56.9 3.0 17 116.8 6.1 7 176.8 9.3 37 236.7 12.4 97 296.6 15.5 58 57.9 3.0 18 117.8 6.2 78 177.8 9.3 37 236.7 12.5 98 297.6 15.6 59 58.9 3.1 19 118.8 6.2 79 178.8 9.4 39 238.7 12.5 98 297.6 15.6 60 59.9 3.1 20 119.8 6.3 80 179.8 9.4 40 239.7 12.6 300 299.6 15.7 Dist. Dep. Lat. Lat. Dist. Dep. Lat.	1 (4	53.9	2,8	14	113.8	6.6	74	173.8	9.1	34	233- 7.		94	293.6	15.4
57 56.9 3.0 17 116.8 6.1 7 176.8 9.3 37 236.7 12.4 97 296.6 15.5 58 57.9 3.0 18 117.8 6.2 78 177.8 9.3 37 236.7 12.5 98 297.6 15.6 59 58.9 3.1 19 118.8 6.2 79 178.8 9.4 39 238.7 12.5 98 297.6 15.6 60 59.9 3.1 20 119.8 6.3 80 179.8 9.4 40 239.7 12.6 300 299.6 15.7 Dist. Dep. Lat. Lat. Dist. Dep. Lat.	55	54.9	2.9	1 15	114.8	6.1	75	174.8	0.2	35	234. 7	12, 3	3	294. 0	15.5
58 57.9 3.0 18 117.8 6.2 78 177.8 9.3 33 237.7 12.5 98 297.0 15.6 29 58.9 3.1 19 118.8 6.2 79 178.8 9.4 39 238.7 12.5 99 296.6 15.0 60 59.9 3.1 20 119.8 6.3 80 179.8 9.4 40 239.7 12.6 300 299.6 15.7 Dist. Dep. Lat. Att. Dist. Dep. Lat.	57	56.9	3.0	17	116.8	6.1	77	176.8	9.3	37	236. 7	12, 4	97	206. 6	15.5
60 59.9 3.1 20 119.8 6.3 80 179.8 9.4 40 239.7 12.6 300 299.6 15.7 Dist. Dep. Lat.	58	57.9	3.0		117.8		78		9.3	38	237. 7	12.5		297. 6	
Dist. Dep. Lat.	8	59.9	3.1				86	179.8	9.4		239. 7	12.6		299.6	15.7
		-				1.00	F24		7.00	Dia	Den	7.00	Dist	Den	Tat
	-	Deb.			Deb.	1		1 July			Dehr				

DIFFERENCE OF LATITUDE AND DEPARTURE FOR 4°.

Diet.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Let.	Dop.	Diet.	Lat.	Dep.	Dist.	Lat.	Dep.
-	1.0	0.1	61	60, 9 61, 8	4.3	121	120. 7	8.4	181	180, 6	12, 6	241	240.4	16, 8
	2.0	0.1	68	61.8	4-3	22	121.7	8.5	82	181.6	12.7	42	241.4	16.9
3	3.0	0.2	63	62.8	4.4	23	122. 7	8.6	83	182, 6	12, 8	43	242.4	17.0
4	40	0.3	64	63. 8 64. 8	4.5	24	123. 7 124. 7	0.0	84	183. 6 184. 5	12.8	44	243.4	17. 0 17. 1
ş	5.0 6.0	0.3	65	66.8	45	25 26	124. 7 125. 7	8. 7 8. 8	85 86	185.5	13.0	45 46	244. 4 245. 4	17. 3
	7.0	0. 5	67	65. 8 66. 8	4.7	27	125. 7 126. 7	8.9	87 88	185. 5 186. 5	13.0	1 77	246.4	17. 2
7	7.0	ο. <u>\$</u> σ. 6	67 68	67. 8 68. 8	4-7 4-7 4-8	27 28	127.7	8.6		187. 5 188. 5	13. 1	47	247. 4 248. 4	17.3
9	9.0	0.6	69	68, 8		29	128.7	9.0	89	188.5	13. 2	49	248.4	17.4
10	10.0	0.7	70	69.8	4.9	30	129. 7	9.1	90	189.5	13. 3	50	249.4	17.4
11	11.0	0.8	71	70.8	5.0 5.1 5.2 5.8	131	130. 7	9. 1	191	190.5	13. 3	251 52	250, 4	17. 5 17. 6
12	12.0	0,8	72	71.8	5.0	32	131. 7	9.2	98	191.5	13. 4 13. 5 13. 5 13. 6	52	251.4	17.6
13	13. 0 14. 0	0.9 1.0	73 74	72. 8 73. 8	>:	33 34	132. 7 133. 7	9.3	93 94	192.5	13-5	23	252. 4 253. 4	17.6
1 21	15.0	1.0	1 42	74.8 75.8 76.8	5.3	35	134.7	9.3 9.4 9.5	~	193. 5 194. 5	13.6	1 2	254-4	17. 7 17. 8
15	16. o	1.1	75 76	75. 8	5.3	35 36	135. 7	6.3	95 96	195.5	13. 7	36	255.4	17. 0
17	17.0 18.0	1. g	77	76.8	5.4 5.4	37 38	136.7		97 98	195. S 196. S	13.7	57	255.4 256.4	17.9 18.0
		1.3	76	77. 8 78. 8	5-4	38	137.7	9.6		197. 5	13. 7 13. 7 13. 8	53 54 55 57 58 59	257.4 258.4	18.0
19	19.0	1.3	72	78.8	5. 5 5. 6	39	138.7	9.7	99	198.5	13.9	\$9	258.4	18. 1
90	20.0	1.4		79.8	5.0	40	139.7		200	199. 5	14.0	961	259.4	18.1
21	20.9	1.5 1.5 1.6	81 82	80. 8 81. 8	5.7 5.8 5.9	141	140. 7		201	200, 5 201, 5	14.0	62	260, 4 261, 4	18. 2
23	\$1.9 \$2.9	1:31	83	82.8	2.7	42 43	142.7	9.9	03	202.5	14. I 14. 2	63	962.4	18. 3 18. 3 18. 4
24	23.9	1.7	84	8-8	1 6.0	44	142.7	10.0	04	203.5	14.2	64	262.4	18.4
25 26	24.9	1.7	85 86	84. 8 85. 8 86. 8	5. 9 6. 6	45 40	144.6	10. I	95	204. 5	14. 3	65 66		18.5 18.6
số l	25.9 26.9	1, 8	86	85.8	6.6	46	145.6 146.6	10, 2		205.5	14.1	66	265. 4 266. 3	18.6
27	s 6.9	19	87 88	86, 8	6.1	47	146.6	10.3	%	206, 5	14.4	67 68	266.3	18.6
	27. 9 28. 9	2.0	88 89	87. 8 88. 8	6. I 6. 2	48	147.6	10. 3 10. 4	05	207. 5	14.5	69	267. 3 268. 3	18. 7 18. 8
29 30	20.9	2,0 2,1	3	89.8	6.3	49 50	148. 6 149. 6	10. 4	10	208.5	14.6	70	268. 3 269. 3	18.8
	30.9	3, 3	91	90.8	6.3	151	150.6	10.5	211	210.5		271	270. 3	18.0
31 32	31.9	2. 3	92	91.8	6.3	52	151.6	10.5	12	811.5	14.7	72	270. 3 271. 3	19.0
33	32.9	2.3	93	028	6.4	53	152.6	10.7	13	312, 5	14 9	73	472.3	19.0
انتا	22.0	2.4	مند	93. 8 94. 8 95. 8 96. 8	6,6	54	153.6	10.7	14	213.5	14.9	73 74 75 76 77 78 80	273. 3	19.1
35 36	34.9 35.9 36.9	2.4	95 96	94.8	6,6	55 56	154.6	10.8	15 16	214.5	15.0	75	274-3	19. 2
36	35.9	2.5	96	95.8	6. 7 6. 8	56	155. 6 156. 6	10.9	10	215.5	15. 1	7º	275.3 270.3	19.3
37 38	30.9	2.0	97 98	90.8	6. 8 6. 8	57 58	157.6	11.0	17 18	210.5	15. 1	1 73	270.3	19. 3 19. 4
30	37. 9 38. 9	2.7	99	97. 8 98. 8	6.9	50	158.6	11.1	19	217.5	15. 2 15. 3	%	277.3 278.3	19.5
40	39.9	2. 7 2. 8	100	99.8	7.0	59 60	159.6	11.2	20	819.5	15.3	86	279.3	19.5
41	40.9	8.9	101	100.8	7.0	161	160.6	11.2	221	220. 5	15.4	281	280 2	10.6
43	41.9	2.9	02	101.8	7. 1	62	161.6	11.3	22	221.5	15. 5	82	281. 3	10.7
43	42.9	3.0	03	102. 7	7. I 7. 2 7. 3	63	162.6	11.4	23	222. 6	15. 5 15. 6	83	282. 1	19. 7 19. 8
44	43-0	3.1	04	102. 7	7.3	64	163.6	11.4	24	223. 5	15.6	84	283. 3	19.8
45	44.9	3.1	25	104.7	7.3 7.4	65	164.6	11.5	25 26	224. 5	15. 7 15. 8	85 86	254.2	19.9
40	45.9 46.9	3.8	, oo	104.7 105.7 100.7	7.4	67	165. 6 166. 6	11.6		225. 4 326. 4	15.8	87	285. 3 286. 3	20.0
47	47.0	3. 3 3. 3	37	106. 7 107. 6 108. 7	7.5 7.5 7.6	67 68	167.6	11.7	27 28	227. A	15.0	87 88	287.3	20.1
49	47.9 48.9	3.4	9	108. 7	7.6	69	167. 6 168. 6	11.7	29	227. 4 228. 4	15. 9 16. 0	89	288. 1	20, 2
5ó	49.9	3-5	ΙÓ	109. 7	7.7	70	169.6	11.9	30	229.4	16,0	90	289.3	20, 2
51	50.0	2.6	111	110.7	7. 7 7. 8	171	170.6	11.9	231	230.4	16. 1,	291	290, 3	20, 3
52	51.9 52.9	3.6	12	111.7	7.8	72	171.6	12.0	32	231.4	16. 4	92	291.3	20.4
53	52. 9	3-7	13	112.7	7.9	73	172.6	12. 1	33	232.4	16. 3 16. 3	93	292. 3	20.4
53 54 55 56	53. 9 54. 9	3. 8 3. 8	14	113.7	8.0	74	173.6 174.6	12. I 12. 2	34	233. 4 234. 4	16 4	94 95 96	293. 3 294. 3	20.5
갫	54.9	3.0	15 16	115.7	8. z	75 76	175.6	12.3	35 36	235.4	16.	23	295.3	20.6
57	56. 6	4.0	17	116. 7	8 .	77	176.6	12. 3	37	235.4 236.4	16.5 16.5 16.6	97 98	296.3	20. 7 20. 8
57 58	55. 9 56. 9 57. 9 58. 9	4.0	17 18	117. 7	8.1	78	177.6	12.4	37 38	237.4 238.4	16.6	98	297.3	20.8
52	58. ģ	4.1	49	118.7	8. 3	79 80	178.6	12, 5 12, 6	39	238.4	16. 7	99	298. 3	20.9
60	59.9	4.2	20	119.7	8.4	80	179.6	12.6	40	239.4	16. 7	300	299. 3	30.9
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	I,at.
┝╌┙			•			•						í F~	86 Degr	***
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	D	IFFE	CRE	NCE (OF L	ATIT	TUDE	AND	DE	PARTU	JRE	FOR	. 5°.		
Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Let.	Dep.	Dist.	Let.	Dep.	Dist.	Let.	Dep.	
1	1.0	0.1	61	60, 8 61, 8	5.3	191	120.5	10.5	181 82	180. 3 181. 3	15.8	241	240. I 241. I	21,0 21.1	
3	2. 0 3. 0	0.2	6a 63	62, 8	5. 4 5. 5 5. 6	22 23	121.5	10.7	83	182. 1	15.9 15.9 16.0	42 43	842, I	21.2	
4	4.0	0.3	64	63.8 64.8	1 6.6	24	123. 5 124. 5	10. 7 10. 8 10. 9	83 84 85 86	183. 3 184. 3	16, o 16, I	44	243. 1 243. 1	21.4	
8	6.0	35	65 66	65.7	5. 7 5. 8 5. 8	25 26	125.5	11.0	88	185. 3 186. 3	16. 2	45 46	245. I 246. I	21.4	
7	7.0	0.6	67 68	66.7	5.8	27 28	126. 5	11.1	87 88	186. 3 187. 3	16. 3 16. 4	47	246, 1	21.5 21.6	
9	9.0	0. 7 0. 8	69	67. 7 68. 7	6.0	29	128. 5	11. 2	89	188. 2	16.5	49	247. I 248. I	31.7	
10	10.0	0.9	70 71	69.7	6, 1	30 131	129. 5 130. 5	11.3	90 191	189. 3	16.6	50	249. 0 250, 0	21.8	
12	12.0	1.0	71 72	71.7	6.4	32	131.5	11.5	92	191.3	16. 7 16. 8	251 52	251.0	22.0	
13 14	13.0 13.9	I. I I. 2	73 74	72. 7	6.4	33 34	132. Š	11.6	93	192. 3 193. 3	16. 8 16. 9	53	252, 0 253, 0	22.J 22.1	
15 16	14.0	1.3	75	74.7	6.5	35 36	134-5	11.7	94 95 96	104. 1	17.0	53 54 55 56	254.0	22. 2	
	15.9 16.9	I.4	76	70. 7 71. 7 72. 7 73. 7 74. 7 75. 7	6.7	36 37	135. 5 136. 5	11.9	96	195. 3 196. 3	17.1	56	255. 0 250. 0	22. 3 22. 4	
	18 17.9 1.6 78 77.7 6.8 38 137.5 12.0 98 197.2 17.3 58 257.0 22.5 19 18.9 1.7 79 78.7 6.9 39 138.5 12.1 99 138.2 17.3 59 258.0 22.6 20 19.9 1.7 80 79.7 7.0 40 139.5 12.2 200 199.2 17.4 60 259.0 22.7														
19	19 18. 9 1. 7 79 78. 7 6. 9 39 138. 5 12. 1 99 198. 2 17. 3 59 258. 0 22. 6 20 19. 9 1. 7 80 79, 7 7. 0 40 139. 5 12. 2 200 199. 2 17. 4 60 259. 0 22. 7														
21	20 19.9 1.7 80 79.7 7.0 40 139.5 12.2 200 199.2 17.4 60 259.0 22.7 21 20.9 1.8 81 80.7 7.1 141 140.5 12.3 201 200.2 17.5 251 251 250.0 22.7 21 20.9 1.0 8 81 7.7 1 41 140.5 12.3 201 200.2 17.5 251 250.0 22.7														
	21 20, 9 1.8 81 80, 7 7.1 141 140, 5 12.3 201 200, 2 17.5 251 260, 0 22.7														
24	23 22.9 2.0 83 83.7 7.2 43 143.5 12.5 03 202.2 17.7 03 202.0 22.9 24 23.9 2.1 84 83.7 7.3 44 143.5 12.5 04 202.2 17.8 64 253.0 23.0 23.0 24 23.0 23.0 23.0 23.0 23.0 23.0 23.0 23.0														
25	23 22.9 2.0 83 83.7 7.2 43 142.5 12.5 03 202.2 17.7 03 202.0 23.9 24 23.9 2.1 84 83.7 7.3 44 143.5 12.6 04 202.2 17.8 64 263.0 23.0 23.0 24 20.0 2.2 86 84.7 7.4 44 143.5 12.6 05 202.2 17.8 64 263.0 23.0														
27 23	26.9	2.4	87 88	86.7	7. 5 7. 6 7. 7 7. 8	47 48	145. 4 146. 4	12. 7 12. 8	97 98	205. 2 206. 2	18.0	67 68	265. 0 266. 0	23.3	
23	27.9 28.9	2.4	80 80	87. 7 88. 7	7.7	45 49	147.4 148.4	12.9	05	207. 2	18, 1 18, 2	69	267. o 268. o	23.4	
30	29.9	2. § 2. 6	90	89.7	7.8	50	149. 4	13. 1	10	209. 2	18. 3	70	269. 0	23. 5	
31 32	30.9	2.7	91 92	90. 7 91. 6	7.9 8.0	151 52	150.4	13. 2 13. 2	211	210. 2 211. 3	18.4	271	270.0 271.0	23. 6 23. 7	
33	32. 9	2.9	93	Q2.6	l 8. r	53 54	152.4	13.3	13	212, 3	18. 5 18. 6	73	272.0	23.8	
34	33.9 34.9	3.0	94	93. 6 94. 6	8. a 8. 3	54	153.4	13.4	14	213. 2 214. 2	18.7	74	273. 0 274. 0	23.9 24.0	
35 36	35. 9 36. 9	3.1	95 96	95.6	8.4	55 56	154-4 155-4	13.6	15 16	216.2	18, 8	78 73 74 75 76 77 78 79 80	274.9 275.9 270.9	24.1	
37 38	36. 9 37. 9	3.2 3-3	97 98	90.0	8. 5 8. 5 8. 6	57 58	150.4	13. 7 13. 8	17 18	210. 2	18.9	72	275.9 270.0	24.1	
39	38.9	3.4	99	97. 6 98. 6	18.6	59	158.4	13.9	19	218.2	19.1	79	277. 9 278. 9	24.3	
41	40.8	3.5	100	99.6	8.7	161	159.4	13.9 14.0	20	219. 2	19. 2	281	270.0	24. 4 24. 5	
42	41.8	3.7	03	101.6	8.9	62	161.4	14. 1	22	221. 2	19. 3	82	279.9 280.9	24.6	
43 44	42. 8	3. 7 3. 8	03 04	103, 6 103, 6	9.0	63 64	162, 4 163, 4	14.2	23 24	223, 2 223, 1	19.4 19.5	83 84	281.9 282.9	24.8	
45	44.8	3.9	3	104.6	9.2	65	164.4	14.4	25	224. I	19. 5 19. 6	85	281.0	24.8	
40	43.8 44.8 45.8 47.8 47.8 49.8	40	3	105.6	9.2	67 68	165. 4 166. 4	14.8	27	225. I 226, I	19. 7 19. 8	87 88	#84.9 #85.9	24.9 25.0	
47 48	47.8	4.2		107.6	9.4	68	167.4	14.6	27 28	227. I 228. I	19.9	88 89	285. 9 286. 9	25. 1	
49 50	40.8	43	29	108.0	9.5	69 70	169. 4	14.7	39 30	228, I 229, I	90. 0 90. 0	90	287. 9 288. 9	25. 2 25. 3	
51		4.4	111	110,6	9.7	171	170. 3	14.9	231	230. 1	20. 1	29I	289.9	25.4	
52 53	51.8	4 8	12	111.6	9.7 9.8 9.8	72 73	171.3 172.3	15.0 15.1	32	231. I 232, I	90, 2 90, 3	98 93	290. 9 291. 9	25. 4 25. 5	
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55 56	54.8	4.8	15	114.6	10.0 10.1	75	174. 3 175. 3	15. 3 15. 3	35	234. I 235. I	20. 5 20. 6	23	293. 9 294. 9	25. 7 25. 8	
57 58	55. 3 57. 8	5.0	17	115.6	10, 2	77	176. 1	16.4	33 34 35 36 37 38	#35. I #36. I	20.7	97 98	295.9 296.9	25.9	
58 59	57. 8 58. 8	ğ. 1 5. 1	19	117.6	10.3	70	177.3 178.3	15. 5 15. 6	39	237. 1 238. I	80,8	99	297.9 298.9	26, 1	
66	59. 8	ğ. <u>a</u>	86	119.5	10. 5	86	179.3	15. 7	40	139. I	80. 9	300	a98, 9	26, I	
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DIFFERENCE OF LATITUDE AND DEPARTURE FOR 6°.

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Dist.	Lat	Dep.	Dist	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1 2	1.0	0.1	61 62	60. 7 61. 7	6.4	12 I 22	120. 3	12. 6 12. 8	181 82	180. 0 181. 0	18.9	241	239. 7	25. 2
3	3.0	0.2	63	62. 7	6.5	- 23	121, 3 122, 3	12.0	83	182.0	19.1	42 43	240. 7 241. 7	25. 3 25. 4
4	4.0	0.4	64	63.6	6. 7 6. 8	24	123. 3	13.0	انعا	183.0	19.3	44	242. 7	25. 5
ş	5. o	0.5	65	64.6	6.9	25 26	124. 3 125. 3	13. 1 13. 2	85 86	184. 0 185. 0	19. 3 19. 4	45 46	243. 7 244. 7	25.6 25.7
7	7. o 8. o	0.7	67	65. 6 66. 6	7. 0	27	126, 3	13.3	87 88	186.0	19. 5	47 48	244. 7 245. 6	25. 7 25. 8
8	8.0 9.0	0.8	68	67. 6 68. o	7. 1 7. 2	28 29	127. 3 128. 3	13.4	88	187. o 188. o	19.7	48	246, 6 247, 6	25. 9 26. 0
10	9.9	1.0	70	69.6	7.3	30	129. 3	13.5 13.6	90	189. o	19.9	50	248, 6	26, 1
11	10.9	1. I 1. 3	71 72	70.6 71.6	7.4	131 32	130. 3 131. 3	13. 7 13. 8	191	190, 0 190, 9	20, 0 20, I	251 52	249. 6 250. 6	26, 2 26, 3
13	12.9	1.4	73	72.6	7. 5 7. 6	33	132.3	13.9	93	191.9	20. 2	53	251.6	26. 4 26. 6
14	13.9	1.5	74	73.6	7. 7 7. 8	34	133. 3	14.0	94	192.9	20. 3	54	252.6	26, 6
15	14.9 15.9	1.7	75	74. 6 75. 6	7.0	35 36	134- 3 135. 3	14. I 14. 2	95 96	193. 9 194. 9	20. 4	55 56	253.6 254.6	26. 7 26. 8
17	16.9	1.7	77 78	75, 6 76, 6	7.9 8.0 8.2	37 38	136. 2	14.3	97 98	195. 9	20, 5	57 58	255.6	26, 9
10	17.9	1.9	70	77.6 78.6	8.3	38 39	137. 2 138. 2	14.4	98	196. 9 197. 9	20. 7 20. 8	50	256. 6 257. 6	27. 0 27. I
20	19.9	2. 1	79 80	79.6	8.4	40	139. 2	14.5 14.6	200	198.9	20.9	59 60	257. 6 258. 6	27. 2
21	20.9	2.3	81 82	80, 6, 81, 6	8. 5 8. 6	141 42	140, 2	14. 7 14. 8	201 02	199. 9 200. 9	21.0 21.1	261 62	259. 6 260. 6	27. 3 27. 4
23	22. 9	2,4	82	82, 5	8.7	43	142. 2	14.9	03	201.9	21.2	63	261.6	27. 5 27. 6
24 25	23. 9 24. 9	2.5	84 85 86	83. 5 84. 5	8.8	1 44	143. 2	15. I 15. 2	04 05	202. 9	21.3 21.4	64	262.6 263.5	27.6
26	25.9	2.7	88	85.5 86.5	9.0	45	145. 2	15.3	3	204.9	21.5	65 66	264. C	27. 7 27. 8
27 28	25. 9 26. 9 27. 8 28. 8	2.8 2.9	87 88	86.5	9.1	47 48	146, 2	15.4	27	205. 9 206. 9	21.6	67 68	265. 5 266. 5	27. 9 28. 0
29	28.8	3.0	89	87. 5 88. 5	9.3	49	148, 2	15. 5 15. 6	🐃	237. 9	21.7 21.8	69	267. 5 268. 5	28. I
30	29.8	3.1	90	89. 5	9.4	50	149. 2	15. 7	10	208, 8	22. 0	70	268. 5	28. 2
31 32	30. 8 31. 8	3. 2 3. 3	91 92	90. 5 91. 5	9.5 9.6	151	150, 2 151, 2	15. 8 15. 9	211 12	209. 8 210. 8	22. I 22. 2	271 72	269. 5 270. 5	28, 3 28, 4
33	12.8	3.4	93	92.5	9.7	53	152, 2	16,0	13	211.8	22. 3	73	271.5	28. 5 28. 6
33 34 35 36	33. 8 34. 8	3.0	왔	93. S 94. S	9.9	뚌	153. 2 154. 2	16. 1 16. 2	14	212, 8 213, 8	22. 4	74 75	872. 5 273. 5	28. 7
36	35. 8 36. 8	3. 7 3. 8	95 96	95. 5 96. 5	10.0	55 56	155. 1	16. 3	16	214.8	22. 5 22. 6	75 76	274.5	28, 7 28, 8
37 38	30. 8	3.9	97 98	90.5	10, 1	57 58	156, 1 157, 1	16, 4 16, 5	17	215, 8	22. 7 23. 8	77 78	275. 5 276. 5	29. 0 29. I
39	37. 8 38. 8	4.1	99	97. 5 98. 5	10, 3	59	158. 1	16.6	19	217.8	22.9	79	277.5	29. 2
40	39. 8 40. 8	4.8	100	99-5	10.5	161	159.1	16. 7	20	218.8	23. 0 23. I	281	278.5 279.5	29. 3 29. 4
42	41.8	4.4	02	101.4	10.7	62	161. 1	16.9	22	220, 8	23.2	82	280.5	29. 5
43	42. 8 43. 8	4.5	03 04	102, 4	10, 8	63 64	162, I 163, I	17. 0 17. 1	23 24	221, 8 222, 8	23. 3 23. 4	83 84	281.4 282.4	29.6
45 46	44.8	47	ος	104.4	11. Ó	55	164.1	17. 2	25	223, 8	23. 5 23. 6	85 86	283.4	29. 7 29. 8
46	45. 7 46. 7	4.9	06 07	105.4	11, 1	66	165. I 166. I	17.4	26 27	224. 8 225. 8	23.6	86	284. 4 285. 4	29. 9 30. 0
47	47. 7 48. 7	5.0	08	107. 4	11.3	67 68	167. 1	17. 5 17. 6	28	226, 8	23. 7 23. 8	87 88	286. A	30, I
49 50	48. 7 49. 7	5. 1 5. 2	09 IO	108.4	11.4	69 70	168, 1 169, 1	17. 7 17. 8	29 30	227. 7	23. 9 24. 0	89 90	287. 4 288. 4	30, 2 30, 3
51	50. 7	5.3	111	110.4	11,6	171	170. 1	17.9	231	229. 7	24.1	291	289. 4	30.4
52 53	51. 7 52. 7	5.4	12	111.4	11.7	72	171. 1 172. 1	18, 0	32	230. 7 231. 7	24-3	92	290. 4 291. 4	30. 5 30 6
54	53-7	5. 5 5. 6	13 14	112.4	11.0	73 74	173.0	18, 2	33 34	232. 7	24. 4 24. 5	93 94	291.4	30. 7 30. 8
54 55 56	54.7	5.7	15 16	114.4	12.0	75 76	174.0	18. 3	35 36	233. 7	24. 5 24. 6	95 96	293.4	
57	55. 7 56. 7	5.0	17	115.4	12, I 12, 3	77	175.0	18. 4 18. 5 18. 6	30 37	234. 7 235. 7	24. 7	97	294. 4 295. 4	30. 9 31. 0
57 58	57. 7 58. 7	6.1		117.4	12. 3	77 78	177.0	18, 6	37 38	276. 7	24.9	97 98	296.4	31. 1
82	50. 7 59. 7	6.3	19 20	118.3	12. 4 12, 5	20	178.0 179.0	18. 7 18. 8	39 40	237. 7 238. 7	25. 0 25. I	300	297. 4 298. 4	31. 3
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3 3.0 0.4 63 6.15 7.6 23 191.1 1 1.50 83 181.6 22.3 43 24.2 25.5 5.5 4.0 4.0 0.5 64 63.5 7.8 24 193.1 15.0 83 181.6 22.3 43 24.2 25.5 5.5 25.0 0.6 65.6 64.5 7.9 2.5 12.1 15.0 83 181.6 22.5 45 44 24.2 2.2 25.0 0.6 65.6 64.5 7.9 2.5 12.1 15.0 83 181.6 22.5 45 45 24.2 25.0 1.0 0.9 67 66.5 8.3 27 186.1 15.5 85 183.6 22.5 45 24.2 24.2 29.0 1.0 0.9 67 66.5 8.3 27 186.1 15.5 85 183.6 22.5 45 24.2 24.2 29.0 1.0 0.9 67 66.5 8.3 28 27 186.1 15.5 85 183.6 22.5 45 24.2 24.2 29.0 1.0 0.9 67 66.5 8.3 28 27 186.1 15.5 85 183.6 22.5 45 24.2 24.2 29.2 29.1 1.0 0.9 69.5 8.5 29 182.0 15.7 89 187.6 22.0 29.4 24.2 29.2 29.1 1.0 0.9 69.5 8.5 29 182.0 15.7 89 187.6 22.0 29.4 24.2 29.2 29.1 1.0 1.0 1.5 7.7 70.5 8.7 131 130.0 15.7 89 187.6 23.3 251 24.2 29.2 24.2 1.3 2.1 11.0 1.5 7.7 70.5 8.7 131 130.0 16.0 19.1 189.6 23.3 251 24.2 1.3 2.1 11.0 11.5 72 71.5 8.8 23 131.0 16.1 192 190.6 23.4 25.2 25.2 25.1 25.1 11.1 11.1 11.1 11.1	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Let.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	
3 3,0 0,4 63-63-5,7-7 a3 122.1 15.0 83 181.6 22.3 43 241.2 29.6 6.0 0.6 65 64.5 7.9 a5 124.1 15.2 85 183.6 22.5 45 243.2 29.7 6 0.0 0.7 66 65.5 8.2 27 124.1 15.2 85 183.6 22.5 45 243.2 29.0 7 6.9 0.9 67 66.5 8.2 27 124.1 15.2 85 183.6 22.5 45 243.2 29.0 9 0.9 67 66.5 8.2 27 124.1 15.2 85 183.6 22.5 45 243.2 29.0 9 1.0 68 67.5 8.3 28 127.0 15.6 88 183.6 22.9 48 24.2 29.0 9 82.0 1.0 69 66.5 8.4 29 128.0 15.7 89 183.6 22.9 48 24.2 29.0 19.0 19.0 10.0 86 67.5 8.3 28 127.0 15.6 88 183.6 22.9 48 24.2 29.0 19.0 19.0 19.0 19.0 19.2 19.0 19.2 19.0 19.2 19.0 19.2 19.0 19.2 19.0 19.2 19.0 19.2 19.0 19.2 19.2 19.0 19.2 19.0 19.2 19.2 19.0 19.2 19.2 19.0 19.2 19.2 19.0 19.2 19.2 19.0 19.2 19.2 19.0 19.2 19.2 19.2 19.2 19.2 19.2 19.2 19.2					6a. 5	7.4					179-7				29.4	
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10	-	7.9	1.0		67.5	8, 1		127. 0	15.6		186.6	22.9	#	846. 3	30, 2	
11					69.5	8.4			15.7		187.6	23.0		247. 1	30.3	
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15	13	12.9	1.8	73	72.5	8.9	33	132.0	16. 2	93	191.6	23. 5	53	251. 1		
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49 Å.6 Ö.0 Op 108.2 13.3 69 167.7 20.0 20 287.3 27.9 89 285.8 35.2 51 50.6 6.1 10 109.2 13.4 70 168.7 20.7 30 283.3 38.0 30 20 287.8 35.5 35.3 31 289.3 38.1 281 38.8 35.5 35.6 6.3 11 110.2 13.5 171 169.7 20.8 33.1 289.3 38.8 35.5 35.6 55.0 6.3 111.2 13.5 171 170.7 10.0 33.3 33.3 33.3 33.3 33.3 33.3 34.3 34.0 36.8 35.5 35.6 35.7 73.7 71.7 21.0 33 33.3 33.3 33.3 33.3 33.3 34.3 34.0 36.8 35.7 35.7 73.7 71.7 21.0 33.3 33.3 34.3 34.4 32.5 72	47	45.6	5.7	37	107. 2		68	166. 7	20.4		225. 3 226, 3	27.7		285.9 285.9	35. 1	
51 50.6 6.8 111 110.2 13.5 171 169.7 20.8 231 289.3 28.8 291 285.8 35.5 52 51.6 6.3 12 111.2 13.6 72 170.7 21.1 33 23.3 28.3 32 289.8 25.5 25 25.6 6.5 13 111.2 13.8 73 171.7 21.1 33 23.3 38.4 291 290.8 25.7	49	48.6	6.0	09	108.2	13.3	69	167. 7		29	227. 3	27.9		285, 8	35.2	
52 51.6 6.3 18 111.2 13.6 78 170.7 21.0 32 230.3 23.3 92 239.5 35.6 53 52.6 6.5 13 112.2 13.8 73 171.7 21.1 33 231.3 28.4 93 290.8 35.7	ŞI	50.6	6. a	111	110, 2		171	169. 7	20, 8	231	289. 3	28.2	29I	288.8	2.28	
54 53.6 6.6 14 113.2 13.9 74 170.7 21.2 34 234.3 28.5 44 291.8 25.6 55 54.6 6.7 15 114.1 14.0 75 173.7 21.2 35 233.2 28.6 95 29.8 35.2 55 55.6 6.8 16 115.1 14.1 76 174.7 21.4 36 234.2 28.8 95 29.8 36.1 57 55.6 6.9 17 116.1 14.3 77 124.7 21.4 36 234.2 28.8 99 29.8 36.1 27 28.6 1	52	51.6 52.6	6.3			13.6		170.7		32 11		28.3		200,8	35.6	
33 32 33 33 33 33 33 33 33 33 33 33 33 3	44	53.6	6.6	14	113. 2	13.9	74	172.7	81. 8	34	232, 3	28.5	💥	201.8	35.	
57 50.6 0.9 17 116.1 14.3 77 175.7 21.6 37 235.2 25.9 97 254.8 36.2	55	55.6	6.8	16	115.1	14. 1	73	174.7	21.4	35	834. 2	-R R	33	293.8	36.1	
	57	56.6 57.6	7.1	17	116. 1	14.4	77	175.7	21.6 81.7	37 38	23C. 2	38.9 39.0	97 98	294.8	36.3	
58 57.6 7.1 18 117.1 14.4 76 176.7 21.7 38 236.2 29.6 58 29.8 36.3 59 58.6 7.2 19 118.1 14.5 79 177.7 21.8 39 237.2 29.1 29 236.2 36.3 6.5 59.6 7.3 20 119.1 14.6 80 178.7 21.9 40 238.2 29.2 30.2 36.2 36.2	59	58.6	7.2	19		14.5	12	177.7	21.8	39	217. 2	29. I	99	8,008	36.4	
	Dist.		_	_			_		_	_		_	_			
[For 83 Degrees.																

	D	IFFE	CRE	NCE ()F L	ATI	TUDE	AND	DE	PART	JRE	FOR	. 8°.		
Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat	Dep.	
1 2	1.0	0.1	61 62	60. 4 61. 4	8.5 8.6	121	119.8	16.8	181 82	179. 2 180. 2	25. 2	241	238. 7 239. 6 240. 6	33- 5	
3	2.0 3.0	0.3 0.4 0.6	63	62.4	8, 8	23	121.8	17.0 17.1	83 84	181.2	25. 3 25. 5 25. 6	43 43	240.6	33. 7 33. 8	
4 5	4.0 5.0	0.0 0.7 0.8	64 65 66	63.4	8.9 9.0	24 25 28	122, 8 123, 8	17.3 17.4	85 85 86	182, 2 183, 2	25.7	44 45 46	241. 6 242. 6	34. 0 34. I	
7	5. 9 6. 9	1.0	66 67 68	65.4	9.2 9.3	26 27 28	124. 8 125. 8 126. 8	17.5 17.7 17.8	86 87 88	184, 2 185, 2 186, 2	25. 9 20. 0	46 47 48	243. 6 244. 6	34. 2 34. 4	
8	7.9	1. I 1. 3	68 60	67.3 68.3	9.5	28 20	126. 8 127. 7	17.8 18.0	88 89	187. 2	26, 2	48 49	245.6	34-5	
10 11	9.9	1.4	70	69.3	9.7	30	127. 7	18. 1	90	188, 2	26, 4	50	247. 6 248. 6	34.8	
12	10.9	1.5 1.7 1.8	71 73	70.3 71.3	9. 9 10. 0	131 32	129. 7 130. 7	.8. ▲	191 92	190. 1	26. 7	251 52	249.5	34-9 35. I	
13 14	12. Q 13. 9	1.9	73 74	72.3 73.3	10. 2 10. 3	33 34	131. 7 132. 7	18.5	93 94	191. I 192. I	26. 9 27. 0	53 54	250. 5 251. 5	35. 2 35. 3	
15	14. 9 15. 8	2, I 2, 2	75 76	74.3	10. 4 10. 6	35 36	133. 7 134. 7	18.8 18.9	95 96	193. 1 194. 1	27. I 27. 3	55	252. 5 253. 5	35. 5 35. 6	
	17 16.8 2.4 77 76.3 10.7 37 135.7 19.1 97 195.1 27.4 57 254.5 35.8 18 17.8 2.5 78 77.2 10.0 38 136.7 10.2 08 106.1 27.6 58 255.5 35.0														
19 20	19 18.8 2.6 79 78.2 11 0 39 137.7 19.3 99 197.1 27.7 59 256.5 36.0 so 19.8 2.8 80 79.2 11 1 40 138.6 19.5 200 198.1 27.8 60 257.5 36.2														
81	19 18, 8 2, 6 79 78, 2 11 0 39 137. 7 19, 3 99 197. 1 27. 7 59 256. 5 36. 0 20 19, 8 2, 8 80 79, 2 11 1 40 136. 6 19, 5 200 198. 1 27, 8 00 257. 5 36. 2 21 30. 8 2, 9 81 80. 2 11, 3 141 130. 6 10, 6 201 190. 0 28, 0 261 248, 5 36. 3														
23	81 80. 8 2.9 81 80. 2 11.3 141 139. 6 19. 6 201 199. 0 28. 0 261 258. 5 36. 3 22 21 22. 8 1.8 3.1 82 81. 2 11. 4 42 140. 6 19. 8 02 200. 0 28. 1 62 259. 5 36. 5 21 22. 8 3. 2 8 3. 2 11. 6 42 141. 6 19. 0 01 201. 0 28. 7 01 200. 4 76 6														
24 25	23 22.8 3.8 83 82.2 11.6 43 141.6 19.9 03 201.0 28.3 03 260.4 36 6 84 23.8 3.3 84 83.8 11.7 44 142.6 20.0 04 20.0 28.4 64 261.4 36.7 85 28.2 81.8 45 11.8 45 14.6 20.0 04 20.0 28.5 65 262.4 36.9														
27 28	35.7 35.7	3.8	86 87 88	85, 2 86, 2	12.0 12.1	46 47 48	144. 6 145. 6 146. 6	20. 5 20. 6	06 07 08	204. 0 205. 0 206. 0	28. 7 28. 8	67	263. 4 264. 4	37.0 37.2	
28 29	27. 7 28. 7	3.9	88 89	87. I 88. I	12, 2 12, 4	48	147. 5	20.6	08 09	207.0	28. 9 29. I	68 69	265.4 266.4	37·3 37·4	
30	29. 7 30. 7	4.2	90 19	89. I 90. I	12. 5	50 151	148.5	20.9	211	208.0	29. 2 29. 4	70 271	267. 4	37. 4 37. 6 37. 7	
31 32	31.7	43 45 46	92	91.1	12. 7 12 8 12. 9	53	150.5	21, 2	12	209.9	29.5	72	269. 4 270. 3	37.9 35.0	
33 34	32. 7 33- 7	47	93 94	92. I 93. I	13.1	53 54	152.5	21.3 21.4 21.6	13 14	211.9	29.8	73 74	871.3	38. I	
35 36	34- 7 35- 6 36- 6	4.9 5.0	95 96	94. I 95. I 96. I	13. 2 13. 4	55 56	153-5 154-5	21.7	15	212.9 213.9	29. 9 30. I	75	272. 3 273. 3	38. 3 38. 4 38. 6	
37 38	36, 6 37, 6 38, 6	5, 1 5, 3	97 98	96. I 97. 0 98. 0	13. S 13. 6	57 58	155. 5 156. 5	21.9 22.0	17	214.9	30. s 30. 3	77	274. 3 275. 3 276. 3	38.7	
39 40	38.6 39.6	5.4 5.6	99	98.0 99.0	13.8 13.9	59	157. 5 158. 4	22. I 22. 3	19	215.9 216.9 217.9	30. 5 30. 6	72	276.3 277.3	38. 8 39. 0	
41 43	40.6 41.6	5. 7 5. 8 6. 0	101 02	100, 0	14. I 14. 3	161 62	159. 4 160. 4	22, 4 22, 5	221 22	218, 8 219, 8	30, 8 30, 9	281 82	278, 3	39. I 39. 2	
43	42.6	6.0 6.1	03	102, 0	14. 3	63	161.4 162.4	22. 7 22. 8	23	220. 8 221. 8	31.0	81	279. 3 280. 2 281. 2	39.4	
44 45 46	43.6 44.6	6.3	45.8	103. 0 104. 0	14.5	64 65 66	163.4	23.0	24 25 26	222, 8	31. 3	84 85 86	282, 2	39. 5 39. 7 39. 8	
47 43	45.6 46.5	6.4	96 97 98	105.0	14.8 14.9	67 68	164.4 165.4 166.4	23. I 23. 2	25 27 28	223. 8 224. 8	31.3 31.5 31.6	86 87 88	283, 2 284, 2	39.9	
49	47: 5 48: 5	6.7	09	106.9 107.9 108.9	15, ó 15, s	69	166. 4 167. 4 168. 3	23. 4 23. 5	29	225, 8 226, 8	31.7 31.9	89	285, 2 286, 2	40, I 40, 2	
50 51	49. 5 50. 5	7.0	10	108.9	15.3	70 171	168, 3	23. 7 23. 8	30 231	227. 8 228. 8	32. 0 32. 1	90 291	287. 2	40.4	
52	51. 5 52. 5	7.2	12	110.9	15.4 15.6 15.7	72	170.3	23.9 24.1	32	239. 7 230. 7	32. 3	92	289, 2 290, 1	40. 5 40. 6 40. 8	
33 54	62.6	7.5	14	112.9	15.7 15.9 16.0	73 74	172.3	24.2	33 34	231.7	32. 4 32. 6	93 94	291, 1	40.9	
55	54.5 55.4 50.4	7.7	15 16	113.9 114.9	16. 1	75 78	173.3 174.3	24 5	34 35 36	232. 7 233. 7	32, 7 32, 8	95 96	292. I 293. I	41. I 41. 8	
53 455 55 55 888	50.4 57.4 58.4	7.9	17 18	115.9 116.9 117.8	16. 3 16. 4 16. 6	77	175.3 170.3	24.8	37	#34-7 #35-7	33. 0 33. 1	97 98	994. 1 995. 1 996. 1	41.3 41.5 41.6	
2	58.4 59.4	8.4	19 20	117.8	16.6 16.7	2	177.3 176.8	24.9 25.1	39 40	236. 7 237. 7	33- 3 33- 4	99 300	996. I 997. I	41. 6 41. 8	
Dist.	Dop.	Lat.	Dist.	Dep.	Lat	Dist.	Dep.	Las.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	
Г												[Fo	å Degr	.	

DIFFERENCE OF LATITUDE AND DEPARTURE FOR 9°.

<u> </u>			T	<u> </u>	-			T .	1		-			
Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
,	1.0	0.2	61	60.2	9.5	121	119.5	18.9	181	178.8	28, 3	241	236.0	37.7
2	2, 0	9,3	62	61.2	9.7	22	120.5	19. 1	82	179.8 180.7	28. 5 28. 6	42	239.0	37.9 38.0
3	3.0	0.5	63 64	62.2	9.9	23	121.5	19.8	83	181.7	28. 6 28. 8	43	240.0	38.0 38.2
4	4.0	0.8	1 %	63.2	10, 0	24 85	122, 5 123, 5	19.4	84	182. 7	28, 9	44	241.0 242.0	28.2
ş	5.6	0.9	65 66	65. 2	10. 3	26	124.4	19.7	85 86	183.7	29. I	45 46	243.0	38. 5 38. 6
Z	5.9 6.9	1, 1	67	66.2	10.5	27	125.4	19.9	87 88	184.7	29. 3	47 48	244.0	38.6
	7.9	1.3		67.2	10.6	28	126.4	20.0	88	185. 7 186. 7	29. 4 29. 6		244.9	38.8
10	9.9	1.4	69 70	69.1	10.8	29 30	127.4 128.4	20. 2	89 90	187.7	29. 7	49 50	245.9 246.9	39. 0 39. I
111	10.9	1.7	71	70.1	11.1	131	129.4		191	188.6	29.9	251	247. 9	39-3
12	11. 9 12. 8	1.9	72	71.1	11.3	32	130.4	20, 5	92	189.6	30.0	52	247.9 248.9	39 4
13	12.8	2.0	73	72. 1	11.4 11.6	33	131.4	20, 8	93	190.6	30. 2	53	249.9	
14	13.8 14.8	2, 2 2, 3	74	73.1	11.0	34	132.4 133.3	21.0 21.1	94	191.6 192.6	30. 3	54	250.9	39-7 39-9
15	14.8	2.5	75 76	75. 1	11.9	35 36	134.3	21.3	95 96	193.6	30. 5	55 56	251.9 252.8	40.0
17	15. 8 16. 8	2. 7 2. 8	77 78	75. 1 76. 1	12.0	37 38	135.3	21.4	37	1 104.6	30. 7 30. 8	57 58	253. 8	40.2
	17.8	2.8	78	77.0	12, 2		135. 3 136. 3			195.6 196.5	31.0	58	254.8	40.4
19	18.8 19.8	3.0 3.1	72	78.0	12.4	39 40	137. 3 138. 3	21.7	99	190.5	31. I 31. 3	59	250.8 250.8	40.5
21	20. 7	3.3	1	80.0		141	139.3	21.9	201	198.5		261	257.8	40.8
22	21.7	3.4	82	81.0	12. 7 12. 8	42	140.3	22. 2	2	199.5	31.4 31.6	62	258.8	41.0
23	22. 7	3.4 3.6	83	82.0	13.0	43	141.2	22.4	03	200.6	31.8	62	259.8	41.1
24	23.7	3.8	84	83. 0 84. 0	13. 1	44	142. 2	22.5	94	201.5 202.5	31.9	64	260. 7 261. 7	41.3
25 26	24.7	3.9 4.1	85 86	84.9	13.3	45 46	143.2	22. 7	0 <u>5</u>	202.5	32. 1	65 66	262.7	41.5 41.6
27 28	25. 7 26. 7	4.2	87 88	85. 9 86. 9	13. 5 13. 6	47 48	145. 2	23.0	ű	204.5	32.4	67 68	263.7	41.8
	27. 7 28. 6	4.4		86.9	13.8		146. 2	23. 2		205.4	32.5		264. 7	41.9
29		4.5	89	87. 9 88. 9	13.9	49	147.2	23.3	09	206.4	32. 7 32. 9	70	265. 7 266. 7	42. I 42. 2
30 31	29.6 30.6	4.7	90	89.9	14. 1	151	148, 2	23.5	211	207.4	33.0	271	267.7	
32	31.6	5.0	92	90.9	14.4	52	150. 1	23.8	121	200.4	33. 2	72	268. 7	42.4 42.6
33 34	32, 6	5.2	93	91.9 92.8	14.5	53	151.1	23.9	13	210.4	33.3	73	269.6	48.7
34	33.6	5.3	94	92.8	14.7	54	152. 1	24. 1	14	211.4	33. 5 33. 6	74	270.6	42.9 43.0
35 36	34.6	5. 5 5. 6	95 96	93.8 94.8	14.9	55 56	153. I 154. I	24. 2 24. 4	18	213.3	33.8	75 76	272.6	43.2
37	35. 6 36. 5	5,8	97 98	95.8 96.8	15. 2	57	155.4	24.6	17	814.3	33.9	77 78	273.6	42.2
37 38	37. 5 38. 5	5.9 6.1		96.8	15.3	57 58	156. 1	24.7		215.3	34. 1	78	274.6	43-5 43-6
39	38. 5	6.3	99	97. 8 98. 8	15. 5 15. 6	59 60	157. 0 158. 0	24.9 25.0	19	216. 3 217. 3	34- 3 34- 4	72	275.6 276.6	43.8
40	39-5 40-5		101	99.8	15.8	161	159.0	25.2	221	218.3	34.6	281	277. 5	44.0
42	41.5	6. 4 6. 6	02	100.7	16.0	62	160.0	25.3	22	219.3	34.7	82	277.5 278.5	441
43	42.5	6.7	03	101.7	16. 1	63	161.0	25. 5	23	220.3	34.9	83	279. 5 280. 5	44-3
44	43.5	6.9	94	102. 7	16.3	64	162, 6	25. 7 25. 8	24	221.2	35.0	84	280. 5 281. 5	44: 6
45	44.4 45.4	7.0	25	103.7	16.4	65 66	163.0	26.0	25	223. 2	35. 2 35. 4	85 86	282. 5	44.7
47	46.4	7.4	97 88	105. 7	16. 7	67 68	164.9	26. 1	27	224. 2	28.6	87 88	282.5	44-9
47 48	47-4	7.5		106.7	16.9		165.9	26.3		225. 2 226. 2	35.7	88 80	284. 5	45. I
49 50	48. 4 49. 4	7.7 7.8	10	107. 7	17.1	70	166. 9 167. 9	26.4	29 30	220.2	35. 7 35. 8 36. 0	99	285.4 286.4	45. 8 45. 4
51	50.4	8.0	1111	109, 6	17.4	171	168.9	26.8	231	228. 2	36. 1	291	287.4	45.5
52	51.4	8, r	12	110,6	17.5	72	169.9	26.9	32	229. I	36. 3	92	287.4 288.4	45-5 45-7 45-8
53	52. 3	8. 3	13	111.6	17.7	73	170.9	27. I	33	230.1	36. 4 36. 6	93	289. 4	45.8
54	53.3	8. 4 8. 6	!4	112.6	17.8	74	171.9	27.2	34	231. I 232. I	36.8	94	290. 4 201. 4	I 46. ₹ I
55 56	54- 3 55. 2	8.8	15	114.6	18. 1	75 76	172.8 173.8	27.4 27.5	35 36	232.1	36.0	95 96	292.4	ا 5.4 أما
57	55. 3 56. 3	8.9	17	115.6	18. 2	77 78	174.8	27.7	37 38	234.1	37. 1	97 68	293. 3	46. 5 46. 6
57 58	57· 3 58. 3	9. ī	18	116.5	18. 5	78	175.8 176.8	27. 7		235. t 236. ī	37.2		294-3	46.6 46.8
59	58. 3	9. 2	19	117.5	18. 6 18. 8	79	17,7.8	28. 0 28. 2	39 40	230.1	37·4 37·5	99 300	295. 3 296. 3	46.9
	59- 3	9.4	20	110.5	10. 8	_~	14.9	20. 3	<u> </u>	237.0	34.3	,,,,,	-73	
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.
		·						<u> </u>				[Fo	81 Degr	ees.
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DIFFERENCE OF LATITUDE AND DEPARTURE FOR 10°.

L_					,									
Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Diet.	Lat.	Dep.
1	1.0	0, 2	61	60. I	10.6	121	119. 2	21, 0	181	178. 3	31.4	241	237. 3 238. 3	41.8
2	2. 0	0.3	62	61. 1	10.8	22	120, I	21, 2	82	179. 2	31.6	42	238.3	42.0
3	3.0	0.5	63	62.0	10.9	23 24	121. 1 122. 1	21.4	83 84	180, 2 181, 2	31.8	43	239. 3 240. 3	42, 2 42, 4
4	3.9 4.9	0.7	64	63.0	11.1	1 7	123.1	21.7	86	182, 2	32, 1	44	241.3	42.5
ş		1.0	65	65.0	11.3	25 26	124.1	21.0	85 86	183. 2	32. 3	45 46	242. 3	42.7
7	5. 9 6. 9	1.2	67 68	66.0	11.5	27	125. I 126. I	22. I	87 88	184, 2	32. 5 32. 6	47	243, 2	42.9
	7.9	I. 4 I. 6		67. 0 68. 0	11.8	28	126, 1	22, 2		185. 1	32.6	48	244. 2	43. 1
.9	7. 9 8. 9 9. 8		69	68.9	12.0	29	127. 0 128. 0	22. 4 22. 6	89 90	186. 1 187. 1	32. 8 33. 0	49	245. 2 246, 2	43.2
10	9.8	1.7	70	69.9	12. 2	30	129, 0		191	188. 1	33. 2	50 251		43. 4
12	11.8	1.9	71 72	70.9	12.5	131 32	130.0	22. 7 22. 9	92	189. 1	33.3	52	247. 3 248. 2	43.8
13	12. 8	2.3	73	71.9	12.7	33	131.0	23. 1	93	190, 1	33.5	53	249, 2	43.9
14	13, 8	2. 4 2, 6	74	72.0	12. 7	34	132.0	23. 3	94	191.1	33.7	54	250, 1	44.1
15 16	14.8	2, 6	75 76	73. 9 74. 8	13.0	35 36	132.9	23.4 23.6	95 96	192.0	33.9	55 56	251. I	44-3
10	15. 8 16. 7	2, 8	70	74.8	13.2	30	133.9	23. 0 23. 8	90	193.0	34.0	50	252. 1	44. 8
17	10. 7	3.0 3.1	77	75.8 76.8	13. 4 13. 5	37 38	134.9	24.0	97 98	194.0	34. 2	57 58	253. I 254. I	44.6 44.8
10	17. 7 18. 7	3.3		77.8	13.7	39	135.9 136.9	24. 1	99	195.0	34. 4 34. 6	6		45.0
20	19. 7	3.5	79	77. 8 78. 8	13.9	46	137.9	24.3	200	197.0	34-7	59	255. I 256. I	45. 1
21	20. 7	2.6	81	79.8 80.8	14.1	141	138.9	24. 5	201	197.9	34-9	261	257.0	45.3
22	21. 7	3,8	82	80.8	14. 2	42	139. 8	24. 7 24. 8	02	198.9	35. 1	62	258.0	45. 5 45. 7 45. 8
23	22. 7 23. 6	4.0	83 84	81.7	14.4	43	140.8	24. 8	03 04	199. 9 200. 9	35.3	63 64	259. 0 260. 0	45.7
24	24.6	4.2	85	82. 7 83. 7	14.6	44	141.8	25. 0 25. 2	04	201.9	35. 4 35. 6	65	261.0	45. 8 46. 0
25 26	25. 6	4-3 4-5	85 86	84.7	14.9	45 46	143.8	25.4	05 06	202.0	1 35.8	65 66	262.0	46, 2
27 28	25. 6 26. 6	4.7	87 88	85.7	15.1	47 48	144.8	25.4	្ល	203. 9	35. 9 36. I	67 68	262.9	46.4
	27. 6 28. 6	4.9		86. 7	15. 3		145. 8 146. 7	25. 7		204, 8	36. I		263.9	46.5
29		5.0 5.2	89 90	85. 7 86. 7 87. 6 88. 6	15. 5 15. 6	49 50	140. 7	25. 9 26. 0	09 IO	205.8	36. 3 36. 5	69 70	264. 9 265. 9.	46. 7 46. 9
30 31	29. 5 30. 5		91	80,6	15.8	151	148.7	26, 2	211	207. 8	36.6	271	266. 0	47.1
32	31.5	5. 4 5. 6	92	90.6	16.0	.3.	149.7	26.4	12	208.8	36.8	72	267. 0	47.2
33	32. 5	E. 7	93	91.6	16. 1	53	150. 7	26, 4 26, 6	13	209.8	37.0	73	268. 9 269. 8	47.4 47.6
34	33- 5	5.9 6.1	94	92.6	16. 3	54	151. 7	26. 7	14	210. 7	37. 2	74	269. 8	47.6
35 36	34-5	6.3	95 96	93.6	16. 5 16. 7 16. 8	55 56	152.6	26. 9 27. I	15	211.7	37· 3 37· 5	75 76	270. 8 271. 8	47.8
30	35. 5 36. 4	6.3	97	94-5	16.8	27	153. 6 154. 6	27. 3	17	213.7	37.7	77	272. 8	47.9 48.1
37 38	37. 4	6.4	97 98	94. S 95. S 96. S	17.0	57 58	155.6	27.4	17	214.7	37.9	77 78	273.8	I⊿8.3 I
39	37· 4 38. 4	6, 8	99	97. 5 98. 5	17. 2	59 60	155. 6 156. 6	27. 4 27. 0	19	215.7	37. 9 38. 0	79	274.8	48. 4 48. 6
40	39-4	6.9	100		17.4		157.6	27.8	20	216. 7	38. 2		275.7	48.0
41	40.4	7.1	101	99. 5	17.5	161 62	158.6	28. 0 28. I	221	217. 6 218. 6	38.4	251 82	276. 7	48. 8 49. 0
42 43	41. 4 42. 3	7.3	02	100. 5	17. 7	63	159. 5 160. 5	28.1	23	219.6	38. 5 38. 7	83	277. 7 278. 7	49. I
44	43.3	7. § 7. 6	٠ 4	102.4	17.9	64	161.5	28. 3 28. 5	24	220.6	38. 9	84	279. 7 280. 7	49.3
45 46	44.3	7.8 8.0	95	103.4	18. 2	65 66	162, 5	28. 7 28. 8	25 26	221.6	39. 1	85 86	280.7	49.5
46	45. 3 46. 3	8.0	- 06	104.4	18. 4 18. 6	66	163. 5		26	222.6	39. 2	86	281. 7 282. 6	49.7
47	46. 3	8. 3	97 08	105.4	18. 8	67 68	164. 5 165. 4	29. 0 29. 2	27 28	223. 6 224. 5	39. 4 39. 6	87 88	283. 6	49, 8 50, 0
49	47.3 48.3	8. 3 8. 5	8	100.4	18. 0	60	166.4	29. 3	29	225.5	39.8	89	284.6	50.2
50	49. 2	8.7	10	107. 3	19. 1	70	167.4	29. 5	30	226, 5	39.9	96	285. 6	50.4
31	50. 2	8.9	111	109. 3	19.3	171	168.4	29. 7	231	227.5	40, I	29I	286.6	50.5
52	51.2	9.0	12	110.3	19.4	72	169.4	29.9	32	228.5	40.3	92	287.6	50. 7
53	52.2	9.8	13	111.3	19.	73	170.4	30, 0 30, 2	33	229. 5 230. 4	40.5 40.6	93 94	288. 5 289. 5	50. 9 51. 1
[#	53. 2 54. 2	9.4 9.6	14	112.3	19.8	74 75	171.4 172.3	30. 2	34	231.4	40.8	35	290.5	51.2
3. XX	55, 1	9.7	15 16	114.3	20, I	75 76	173.3	30. 4 30. 6	35 36	232.4	41.0	95 96	291.5	51.4
57 58	55. 1 56. 1	9.9	17 18	115, #	20.3	77	174.3	30. 7	37 38	233.4	41. 2	97 98	292. 5	51.6
98	57. 1 58. 1	10. 1	18	116. 2	80, 5	78	175.3 176.3	30. 9	38	234-4	41.3		293.5	51.7
8	58, r 59, 1	10. 2	19	117.2	20. 7 20. 8	79	170.3	31. 1	39 40	235.4 236.4	41.5 41.7	99 300	294. 5 295. 4	51.9 52. I
	37- 1	14.4	_~	410,3	500,0	L~	-//-3	33	<u>,,,</u>	-37	ļ,	٣,	-73.4	J
Dist.	Dep.	Lat	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.
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DIFFERENCE OF LATITUDE AND DEPARTURE FOR 11°.

Dist.			T	· · ·	-			-					· · ·	r
Dist.	Lat	Dep.	Dist.	Lat.	Dep.	Dist.	Lat	Dep.	Dist.	Lat.	Dep.	Dist.	Lat	Dep.
1	1.0	0.2	61	59-9	31.6	121	118,8	23. 1	181	177. 7 178. 7 179. 6 180. 6	34.5	241	236.6	46.0
2	2, 0	0.4	62	60, 9 61, 8	11 8	23	119.8	23.3	82	178.7	34-7	42	237. 6 238. 5	46. 2
3	2.9	0.6	63	61.8	12, 0	23	120, 7	23.5	83 84	179.6	34-9	43	238, 5	46. 4 46. 6
4	3.9	0.8	64	62. 8 63. 8	12. 2 12. 4	24	121. 7 122. 7	23.7	[않	181, 6	35. 1	44	239. 5 240. 5	40.0
5	4.9	1.1	65	64.8	12.6	25	123. 7	23. 9 24. 0	85 86	182, 6	35. 3 35. 5	45 46	241.5	46.9
	5. 9 6. 9	1.3		64.8	12.8	27	124. 7	24. 2		183.6	35. 7	47	242.5	47.1
8	7.8	1.5	67 68	65. 8 66. 8	13.0	27 28	124. 7 125. 6		87 88	18ã. C	35. 9 36. 1	47	243.4	47-3
9	8, 8	1.7	99	67. 7 68. 7	13. 2	29	126, 6	24. 4 24. 6	89	185. 5 186. 5	36.1	49	244. 4	47.5
10	9.8	1.9	70		13.4	30	127.6	24.8	90	186.5	36. 3	50	245.4	47-7
11	10, 8	2.1	71	69. 7	13.5	131	128.6	25.0	191	187, 5	36. 4. 36. 6	251	246. 4	47.9
12	11.8	2.3	72	70.7	13.7	32	129.6	25. 2	92	188, 5	30. 0	52	247.4 248.4	48.1
13 14	13.7	2.5	73 74	71. 7 72. 6	13.9 14.1	33 34	130, 6 131, 5	25. 4 25. 6	93 94	199.5	37.0	53 54	249.3	48. 3 48. 5
;;	14.7	2.9	1 42	73.6	14.3	**	132.5	25.8	I 27 I	191.4	37. 2	1 22	250. 3	48.7
15	15. 7	3.1	75 76	74.6	14.5	35 36	133. 5	25.8 20.0	95 96	192.4	37.4	55 56	251.3	48.7 48.8
17 18	15. 7 16. 7	3.2	77	75.6 76.6	14 7	37 38	134. 5	26, 1	97	193.4	37. 4 37. 6	57 58	252. 3	49.0
	17. 7	3.4 3.6	78	76.6	14.9	38	135. 5 136. 4	26. 3		194.4	37. 8 38. 0	58	253. 3	49. 2
19	18. 7	3.6	72	77.5 78.5	15. 1	39	136.4	26, 5	99	195. 3 196. 3	38.0	8	-254. 2	49.4
	19.6	3.8	81	70.5	15.3	40	137. 4	26. 7		190.3	38. 2	261	255. 2	49.6
21 22	20, 6 21, 6	40	82	79. 5 80. 5	15. 5 15. 6	141	138.4	26. 9 27. 1	201	197. 3 198. 3	38.5	62	256. 2	49. 8 50. 0
23	21. 0	1 2 2	83	81.5	15.8	43	139. 4 140. 4	27.1	03	199.3	38.7	63	257. 2 258. 2	50.2
24	22.6	4.4	84	82.5	15. 8 16. 0	1 24	141.4	27.5	o4	200.3	38.9	64	259. I	50.4
25 26	24. 5 25. 5 26. 5	4.8	85 86	81.4	16. 2	45	142. 3	27. 7	9	201.2	39.1	65 66	260, I	50. 4 50. 6
	25.5	5.0	86	84.4	16. 4 16. 6	46	143. 3	27. 9 28. 0	જ	202. 2	39. 3	66	261. I	50.8
27 28	26. 5	5. 2	87 88	85. 4 86. 4	16.6	47	144-3	28.0	27	203. 2	39- 5	67 68	262. I	50.9
28	27. 5 28. 5	5.3	88	80. 4 87. 4	16.8	48	145. 3 146. 3	28. 2	8	204. 2	39. 7 39. 9	69	263, 1 264, 1	51. 1 51. 3
30	20.5	5. 5 5. 7	99	88. 3	17. 0 17. 2	49 50	140. 3	28. 4 28. 6	109	205.2	39. 9 40. I	70	265.0	51.5
31	30. 4		91	89.3		151	148, 2	28.8	211		40.3	271	266.0	51.7
32	31.4	5. 9 6. I	92	90.3	17. 4 17. 6	52	149. 2	29.0	12	207. 1	40.5	72	267. 0 268. 0	51.9
33	32. 4	6. 3	93	91.3	17. 7	62	150.2	29. 2	13	209. 1	40. 5 40. 6	73	268.0	52. 1
34	33- 4	6.5	94	92. 3	17.9 18.1	54 55 56	151. 2	29.4	14	\$10.1	40.8	74	269.0	52. 3
35 36	34- 4	6.7	95 96	93. 3	18.1	55	152, 2	29.6	15	211.0	41.0	75	269.9	52. 5
30	35. 3 36. 3	6.9	90	94. 2	18. 3	50	153. 1	29. 8 30. 0		212.0 213.0	41.2		270. 9 271. 9	52. 7 52. 9
37 38	30. 3	7. I 7. 3	97 98	95. 2 96, 2	18. 5 18. 7	57 58	154. 1	30.1	17 18	214.0	41.4 41.6	77	272.9	53.0
39	37· 3 38. 3	7.4	99	97. 2	18. 9	6	155. 1 156. 1	30. 3	19	215.0	41.8	79	273.9	53.2
40	39. 3	7.0	100	97. 2 98. 2	19. I	59 60	157. 1	30.5	20	216.0	42.0		274-9	53.4
41	40, 2	7.8	101	99. 1	19. 3	161	158.0	30.7	221	216.9	42.2	281	275.8	53.6
42	41. 3	8.0	02	100, 1	19.5	62	159.0	30.9	22	217.9	42. 4 42. 6	82	270.8	53.8
43	42. 2	8. 2	03	101, 1	19. 7 19. 8	63	160.0	31. 1	23	218.9	42. 0	83	277. 8 278. 8	54.0
44	43. 2	8. 4 8. 6	94	102, 1	19.8	64	161.0 162.0	31.3	24	219. 9 220. 9	42.7 42.9	84 8c	270.8	54.2 54.4
45 46	44. 2	8.8	25	103. I 104. I	20.0	65 66	163.0	31.5	25 26	1 221 8	43. I	85 86	279. 8 280. 7	54-4 54-6
47	45. 2 46. I	9.0		105.0	20.4	67	163. 9	31.9	27	222. 8	43-3	87 88	281.7	54.8
47 48	47. 1	9.2	97 88	105.0	20. 4 20. 6	67 68	164.9	32. I	28	223.8	43-5		282. 7.	55. 0 55. I
49	47. I 48. I	9.3	99	107. 0 108. 0	20.8	69	165. 9	32. 2	29	224. 8	43-7	89	283.7	55. E
50	49. I	9.5	10		21.0	70	166. 9	32.4	30	225.8	43 9	90	284, 7	55-3
51	50, 1	9.7	1111	109. 0	21, 2	171	167. 9 168. 8	32.6	231	226, 8	44.1	291	285. 7 286. 6	55- 5
52	51. 0 52. 0	9.9 IO. I	12	109. 9	21.4 21.6	72	169.8	32.8	32	227. 7 228. 7	44- 3	92 93	287.6	55. 7 55. 9 56. 1
53 54	53.0	10. 3	13	111.9	27 8	73 74	170, 8	33. 0 33. 2	33 34	220. 7	44.5	94	288.6	16.1
33	54.0	10.5	1 17	112 9	21.0	75	171.8	33.4	35	230.7	44.8	95	289.6	1 56 2
55 56	55.0	10.7	15 16	113.9	22. 1	75 76	172.8	33. 4 33. 6	35 36	231.7	45.0	95 96	290, 6	56. 5 56. 7
57 58	55. o 56. o	10.9	17	114.9	22. 3	77	173. 7	33.8	37 38	232.6	45. 2	97 98	291.5	56. 7
58	€6. q	11.1		115.8	22. 5	78	174. 7	34.0		233.6	45. 4 45. 6		292. 5	56. 9
59	57. 9 58. 9	11.3	19	116.8	22. 7	79	175. 7	34. 2	39	234.6	45. 6	.99	293. 5	57. I
_ ∞	50.9	11.4	20	117.8	22. 9		176. 7	34-3	40	235. 6	45.8	300	294 . 5	57. 2
Dist.	Dep.	Lat	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.
لتنا														
												Fro	79 Degr	ees.

	DIFFERENCE OF LATITUDE AND DEPARTURE FOR 12°.													
Dlat.	Let	Dep	Dist.	Lat.	Dep	Dist	Let.	Dep.	Dist.	Lat.	Dep.	Dist.	Lie.	Dep.
,	1, 0	0.2	61	59. 7	12. 7	121	118.4	25. 2	181	177. 0	37.6	241	#1C. 7	50, I
	2,0	0.6	62	59. 7 60. 6	12.9	23	119.3	25. 4 25. 6	82	178.0	37. 8 38. 0	42	235-7 236-7	50.3
3	2,9	0.6 0.8	63	61. 6 62. 6	13.1	*3	120, 3	25. 6 25. 8	83	179.0 180.0	38. o 38. g	43	237.7 238.7	50. 5
1 1	3.9 4.9	1.0	64	63.6	13.3	24 25	122, 3	26.0	83 84 85	181.0	38. 5	44	239.6	50.7 50.9
8	5. 9 6. 8	1. 2	65 66	64.6	13.7	26	123. 2	26, 2	86	181.9	28.7	45 46	240, 6	51 1
7	6.8	1.5	67 68	65. 5 66. 5	13.9	27	124. 2	26, 4 26, 6	87 88	182.9	38. 9	47 48	241.6	51.4 51.6
Š	7. 8 8. 8	1.7	69	67.5	14.1	20	125. 2 126. 2	20.0	80 80	183. 9 184. 9	39. I 39. 3	49	242.6 243.6	51.8
10	9.8	2, 1	70	67. 5 68. 5	14.3	30	127. 2	27.0	90	184. 9 185. 8	39. 5	50	244.5	52.0
11	10, 8	2. 3	71	69.4	14.8	131	128, 1	27.2	191	186. 8	39- 7	251	245. 5 240. 5	52, 2
12	11.7	2.5	72	70.4	15.0	32	129. 1	27.4	93	187. 8 188. 8	39. 9	52	246, 5	52.4 52.6
13 14	12. 7 13. 7	2.7	73 74	71.4	15.2	33 34	130, 1 131, 1	27. 7	93 94	180. 8	40, I 40, 3	53 54	247. 5 248. 4	52.8
15	14.7	3.1	75	73-4	15.6	35 36	132.0	27. 9 28. 1	95 96	190. 7	40.5	55 56	249.4	53.0
16	15.7	3-3	76	74-3	15.4 15.6 15.8 16.0	36	133.0	28, 3	96	191. 7	40.8	56	250, 4	52.2
13	10.0	3.5 3.7	77	75.3 76.3	16, 2	37 38	134.0	28. 5 28. 7	97 98	192. 7 193. 7	41.0 41.2	57 58	251.4 252.4	53. 4 53. 6
19	17.6 18.6	4.0	79	77.3	16.4	39	135. 0 136. 0	28.9	99	194. 7	41.4	59 60	253-3	53.8
20	19.6	4.2		77.3 78.3		40	136.9	29. 1	200	194. 7 195. 6	41.6		254-3	54. 1
21	20, 5	4.4	81	79. 2 80. 2	16, 8	141	137.9	29. 3	201	196.6	41, 8	261 62	255- 3 256. 3	54-3
22 23	21, 5	4.8	82 83	80, 2 81, 2	17.0	42	138, 9 139, 9	29. 5 29. 7	02 03	197. 6 198. 6	42. 0 42. 2	63	250. 3	54-5 54-7
24	23.5	5.0	84	82, 2	17. 3 17. 5	#	140.9	29.9	04	199. 5	42. 4 42. 6	64	257. 3 258. 2	54.9
25 26	24.5	5.2	85 86	83.1	17.7	45 46	140, 9 141, 8	30. I	95	200, 5	42.6	65 66	259. 2 260. 2	55. I
	25.4 26.4	5. 4 5. 6	86 87	84. I	17.9	46	142. 8 143. 8	30. 4 30. 6	06	201. 5	42. 8 43. 0	67	260, 2 261, 2	55.3
27 28	27.4	5.0	88	85. 1 86. 1	18. 3	47	144.8	30.8	97	203.5	43.2	67 68	262. I	55. 5 55. 7
29	27. 4 28. 4	5.8	89	87. I 88. o	18,5	49	145. 7	31.0	09	204. 4	43-5	.69	267.1	55.9 56.1
30	29. 3	6, 2	90		18. 7	50	P46. 7	31.2	10	205. 4	43.7	70	264. I	
31 32	30. 3 31. 3	6.4	91 92	89. o 90. o	18.9 19.1	151 52	147. 7 148. 7	31.4 31.6	211 12	206. 4	43. 9 44. I	271 73	265. 1 266. 1	56. 3 56. 6
33	32. 3	6.9	93	91.0	19. 3	53	149. 7	31.8	13	207.4	44.3	73	267.0	56.8
34	33- 3	7. 1	94	91.9	19. 5	54	149. 7 150. 6	32, 0	14	209.3	44.5	74	268,0	57.0
35 36	34. 2	7.3	95 96	92.9	19.8	55 56	151.6 152.6	32, 2	15	210. 3 211. 3	44-7 44-9	75 76	269.0 270.0	57. 8
37	35. 2 36. 2	7.5 7.7	97	93.9 94.9	20, 2	57	153.6	32. 4 32. 6		212.3	45. 1	77	270.9	57. 4 57. 6
37 38	37. 2 38. 1	7.9	97 98	95. 9 96. 8	20.4	57 58	154.5	32.9	17 18	213.2	45-3	77 78	271.9	57.8
39	38. 1	8, 1 8, 3	100	96,8	20, 6	.59	155. 5 156. 5	33. 1	19	214.2	45. 5 45. 7	79	272.9 273.9	58. o 58. d
40 41	39, 1 40, 1	8.5	101	97. 8 98. 8	21,0	161	157.5	33·3 33·5	221	216. 2	45.0	281		
42	41. 1	8.7	02	99.8	21, 2	62	157. 5 158. 5	33.7	22	217.1	45. 9 46. 2	82	274. 9 275. 8 276. 8	l (8.6 l
43	42. I	8.9	03	100. 7	21.4	63	159.4 160.4	33.9	23		46.6	83	276. 8	58. B
44	43. 0 44. 0	9.1	04 05	101.7	21.6	65	161.4	34. I 34. 3	24	219. I 220. I	46.8	84 85	277. 8 278. 8	59.0 59.3
45 46	45.0 45.0	9.4 9.6	25	103. 7	22.0	65 66	162.4	34.5	25 26	221, 1	47.0	85 86	279. 8 280. 7	59.5
47	46.0	9.8	07	104. 7	22. 2	°7	163.4	34-7	27 28	222, 0	47. 2	87 88	280, 7	59.7
48 49	47.0	10.0	08 00	105. 7	22. 5 22. 7	60	164. 3 165. 3	34. 9 35. I	20	223. 0 224. 0	47. 4 47. 6	88 89	281. 7 282. 7	59.9
50	47.9 48.9	10. 4	10	107.6	22. 9	70	166. 3	35.3	30	225.0	47.8	90	283.7	60.3
51	49.9	10, 6	111	108, 6	23. I	171	167. 3 168. 2	35.6	231	226, 0	48 0	291	284, 6	60.5
52	50. 9 51. 8	10, 8	12	109, 6	23.3	72	168. 2 169. 2	35. 8 36. 0	32	226.9	48, 2 48, 4	92	285.6 286.6	60.7
53 54 55 56	51. 8 52. 8	11.0 11.2	13	110.5	23. 5 23. 7	73 74	170.2	36. 2	33 34	227. 9 228. 9	18. 7	93 94	287. 6	61, 1
55	53.8		15	112.5	23.9	75	171. 2	36. 4 36. 6	35 36	229. 9 230. 8	48.9	95 96	288.6	61.3
56	54.8	11.4 11.6		113.5	24. 1	76	172. 2	36.6	36	230, 8	49. I	96	289. 5	61.5
57 58	55. 8 50. 7	11.9	17	114.4	24.3 24.5	77	173. I 174. I	36. 8 37. 0	37 38	231, 8 232, 8	49.3 49.5	97 98	290. 5 291. 5	61.7
59 60	57. 7	12. 3	19	115.4	24.7	72	175. 1	37.2	39	233.8	49.7	99	292.5	62, 2
60	57. 7 58. 7	12. 5	20	117. 4	24.9	80	175. I 176. I	37-4	40	234.8	49.9	300	293. 4	62.4
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep	Lat.	Dist.	Dep.	Lat.	Dist.	Dep	Lat.
•												[Fo	r 78 Degr	ocs.

DIFFERENCE OF LATITUDE AND DEPARTURE FOR 13°.

_			_		,				_			_		
Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Let.	Dep.	Dut.	Lat.	Dep.
1	1.0	0, 2	61	E0.4	13.7	121	117.0	27. 2	181	176.4	40.7	241	234. 8	54.8
2	1.9	0.4	62	59.4 60.4	13.9	22	117. 9 118. 9	27.4	ا 🔐	177. 2	40.9	4	235.8	54.4
3	2.9	0.7	63	61.4	14.2	23	118.9	27. 7	81	177.3 178.3	41. 2	43	235. 8 236. 8	54.7
4	20	وه ا	64	62.4		24	120.8	27. 9	83 84	179.3	41.4	44	237-7	54.9
5	4.9 5.8 6.8	1.1	65	63.3	14.4	25 26	121.8	27. 9 28. 1	85 86	180.3	41.4 41.6	45	237. 7 238. 7	55.1
	5.8	1.3	66	64.2	14.8		122. 8	28. 3 28. 6	88	181.2	41. 8	46	839.7	55. 3 55. 6 55. 8 56. 0
7	6.8	1.6	67 68	65.3	15. 1	27 28	123. 7	28, 6	87 88	182, 2	42. 1	47	240. 7 241. 6	55.6
	7. 8 8. 8	1.8		66.3	15. 3		124. 7	28, 8	88	183. 2	42. 3		841.6	55.8
9		2.0	69	67. 2	15.5	29	125. 7 126. 7	29.0	89	184. 2 185. I	42.5	49	242.6	56. s
	9.7		70		15.7	30	120, 7	20, 2	90	185, 1	42. 7	50		50. 3
11	10. 7 11. 7	2.5	71	69. 2	16,0	131	127. 6 128. 6	29. 5	192	186. 1	43. 0	251	244.6	56. 5
12	11.7	2.7	72	70. 2 71. I	16, 2 16, 4 16, 6	32	128.0	29. 7	92	187. I 188. I	43. 2	52	245.5 240.5	56. 7 56. 9
14	12. 7 13. 6	3.1	73	71. 1	10.4	33	130, 6	29.9 30.1	93 94	189.0	43. 4 43. 6	53	240.5	50. 9 57. 1
12	14 6	3.4	#	73. 1	16.9	37	131.5	30. 4	I 💝	190.0	43.9	?:	247. 5 248. 5	2/. 1
16	15. 6 16. 6	3.4 3.6 3.8	75	74 1	17. 1	34 35 36	132.5	30. 4 30. 6	95	191.0	44.1	54 55 56	249.4	57.4 57.6
	16, 6	3.8	77	75.0	17.3	37	133.5	30.8	67	192,0	II 1	37	250.4	57.8
17	17.5 18.5	4.0	77	75.0	17.5	37 38	134.5	31.0	37	192.9	44-3 44-5 44-8	57 58	251.4	57.8 58.0
19	18, 5	4.3	122	77.0	17.8	39	135. 4 136. 4	31.0 31.3	99	193.9	44.8	1 22	852.4	58.3 58.5
30	19. 5	4.5		77.9	18,0	40	136.4	31.5	200	194.9	45. 0		253.3	58.5
21	20. 5	4.7	81	78.9	18. 2	141	137·4 138·4	31.7	20I	194. 9 195. 8 196. 8	45. 2	261	254.3	58.7
22	21.4	4.0	82	79. 9 80. 9 81. 8	18. 4 18. 7	42		31.9	02	106.8	45.4	63	255. 3 256. 3	58.9
23	22. 4	5.4 5.6 5.8 5.6	83	80.9	18. 7	43	139. 3	32, 2	03	197. 8 198. 8 199. 7 200. 7	45. 7 45. 9 46. I	63	256. 3	59.2
24	23.4	5.4	84 85 86	81.8	18.9	- 44	140, 3	32. 4 32. 6	94	198.8	45.9	64 65 66	257. 2 258. 2	59.4 59.6
25 26	24. 4	5.0	1 35	82.8	19. 1	45	141.3	32, 0	25	199.7	40.1	25	258. 2	59.0
20	25. 3 26. 3	1 2.0	≈	83. 8 84. 8	19. 3 19. 6	40	142, 3 143, 2	32, 8	,	201.7	40. 3	, oo	259, 2 260, 2	59.8 60.1
27	20. 3	1 6.	87 88	84.0	19.8	47	144. 2	33. I 33. 3	37	201.7	46. 3 46. 8 46. 8	67 68	261.1	60.3
20	27.3 28.3	6.3 6.5	89	85. 7 86. 7	20.0	49	145.2	33.5	9	202. 7 203. 6	47.0	69	262, 1	60.5
30	29. 2	6.7	90	87. 7	20, 2	50	145. 2 146. 2	33.7	1 76	204.6	47. 2	70	263. I	60.7
31	30. 2	7.0	91	88. 7	20. 5	151	147. 1	34.0	211	205.6	47.5	271	264. I	61,0
32	31. 2	7. 2	92	89.6	20. 7	52	147. I 148. I	34.2	12	206.6	47.7	72	265. 0 266. 0	61.2
33	32. 2	7. 4 7. 6	93	90.6	20.9	53	149. 1	34.4	13	207. 5 208. 5	47. 9 48. 1	73	266.0	61.4 61.6
34	33. 1	7.6	-94	91.6	21, 1	54	150. 1	34. 4 34. 6	14	208.5-	48. I	74	267. 0 268. 0	61.6
35 36	34. I	7.9	95 96	92.6	21.4 21.6	55 56	151.0	34.9	15	209. 5	48. 4 48. 6	75 76	268.0	61.9
30	35. 1 36. 1	2.1	90	93- 5	21.8	50	152.0	35. I	10	210.5	48.8	<u> 20</u>	268, 9 269, 9	6a. i
37 38	30.1	8. 3 8. 5 8. 8	97 98	94-5	21. 0	57 58	153. 0 154. 0	35- 3	17	211.4	49.0	77 78 79	309.9	62. 3
39	37. o 38. o	8.5	99	95. 5 96. 5	22. 3	30	154.9	35. \$	10	213.4	49.3	I %	270.9 271.8	62.5
40	39. 0	9.0	100	97.4	22. 5	59 60	155.9	35. § 35. 8 36. 0	20	214.4	49.5	& i	272.8	63.0
41	39.9	9.2	101	98:4	22. 7	161	156.0	36.2	221	215 2	49.7	281	273.8	63. 2
42	40.9	9.4	02	99.4	22.9	62	156. 9 157. 8	36. ₄	22	215.3 216.3	49.9	82	274.8	63.4
43	41.9	0.7	03	100.4	23.2	63	158.8	36. 7	23	217. 3	50, 2		275. 7	63.7
44	42. 9 43. 8	9.9 10.1	04	101.3	23.4 23.6	64	159. 8 160. 8	36.9	24	217. 3 218. 3	50. 4 50. 6	83 84 85 86	275.7 276.7	63.9
45	43.8	10. 1	05 06	102. 3	23.6	65 66	100.8	37. I	25 26	219.2	50.6	85	377.7	افستا
46	44.8	10. 3 10. 6	06	103. 3	23.8	66	161. 7 162. 7	37. 3 37. 6	26	220, 2	50.8	86	278. 7 -279. 6 280. 6	64.3 64.6
47 48	45. 8 46. 8	10. 8	°7 08	104.3	24. I	67 68	102. 7	37. 6	27 28	221. 2	51. 1	87 88	-279.6	04.0
40	40. 8	10.8	05	105, 2	24. 3	60	163. 7 164. 7	37. 8 38. 0		222. 2	51.3	80	280. 6 281. 6	64.8
49 50	47.7	11.0	10	100. 2	24. 5 24. 7	70	164. 7 165. 6	38. 2	29 30	223. I 224. I	51. 5 51. 7	99	282.6	65. o 65. 2
	49.7	11.5	111	108.2	24. 7 25. 0	171	166.6	38. 5		225. I	52. 0	291	283. 5	65.5
51 52	50.7	11.7	111	100. 2	25. 2	72	167 6	38. 7	231 32	225.1	52.0	92	284.5	65.7
53	50. 7 51. 6	11.9	13	110.1	25.4	73	167. 6 168. 6	38.9	33	227. 0	52.4	93	285.5	65.0
53 54 55 56 57 58	52, 6	12. 1	14	111.1	25.4 25.6	74	169.5	39. 1	34	227. 0 228. 0	52. 4 52. 6	94	285. 5 286. 5	65. 9 66. I
55 1	53.6	12.4 12.6	15	112. I	25. 9 26. I	75	170.5	39.4	35	229. 0	52.9	95	287. 4 288. 4	66. 4 66. 6
56	54.6	12.6	16	113.0	26. 1	75 76	171.5	39. 4 39. 6	35 36	230.0	53. 1	95 96	288. 4	66.6
57	55. 5 56. 5	12.8	17	114.0	26. 3	77 78	172.5	39.8	37 38	230.9	62.2	97 98	289.4	66,8
58	56. 5	13.0		115.0	26. 5 26. 8	78	173-4	40,0		231.9	53. §	98	290.4	67.0
59	57. 5 58. 5	13.3	19	116.0	20. 8	79	174.4	40. 3	39	232. 9		99	291.3	67. 3
∞	50. 5	13. 5	20	116.9	27. 0	80	175-4	40. 5	40	233. 8	54.0	300	292. 3	67. 5
Dist.	Dep.	Lat	Dist.	Dep.	Lat.	Dist.	Dep.	Lat	Dist.	Dep.	Lat	Dist.	Dep.	Lat
	~-p									2-4				
												Γ Frα	77 Degr	

[For 77 Degrees.

DIFFERENCE OF LATITUDE AND DEPARTURE FOR 14°.

Data Lat. Dop. Data				_	_		_			_					
\$ 1.9	Dist.	Let.	Dep.	Dist.	Lat.	Dep.	Dist.	Let.	Dep.	Dist.	Let	Deb	Dist.	Let	Dep.
\$ 1.9		1.0	0.2	61	50.2	14.8	121	117.4	20. 1	181	175. 6	42.8	241	212.5	48. 2
\$ 1.9			0.5		60.2			118.4	89.5		176.6	44.0		234, 8	58.5
5 4.9 1.2 65 63.1 15.7 25 121.3 30.2 85 170.5 44.8 45 237.7 30.5 5 6.6 4.0 16.2 27 123.2 30.5 86 180.5 45.0 48 237.7 30.5 5 7 6.8 1.7 67 65.0 16.2 27 123.2 30.7 87 181.4 45.2 47 239.7 30.5 5 7 8.8 1.9 68 6.0 16.5 27 123.2 30.7 87 181.4 45.2 47 239.7 30.5 60.0 10.9.7 2.2 21.2 21.0 10.9.7 2.2 21.0 10.9	3		0.7			15. 8		119.3		83	177.6	44-3		235. 8	
8 1.5 65 64.0 18.0 a6 12.3 3 0.5 85 18.5 45.0 a6 21.5 7 50.5 85 8 17.6 17.6 65.0 16.5 a8 124.2 31.2 85 181.4 45.5 48 48.0 5 60.0 9 8.7 a.2 69 67.0 16.5 a8 124.2 31.2 85 183.4 45.5 48 840.6 60.0 10. 9.7 a.2 69 67.0 16.9 30 120.1 31.4 90 184.4 45.5 18.0 a8.4 6.6 0.2 a8.6 10. 9.7 a.2 69 17.4 32 131.2 131.2 131.1 131.7 191 185.3 46.4 51.2 34.6 60.2 11.1 10.7 a.9 7 a.9 125.1 31.7 191 185.3 46.4 51.2 244.5 60.2 11.1 10.7 a.9 7 a.9 125.1 31.7 191 185.3 46.4 51.2 244.5 60.2 11.1 10.7 a.9 7 a.9		3.9		94		15. 5	24			54	178. 5	44. §	44	230, 8	
7 6.8 1.7 67 65.0 16.2 37 123.2 30.7 87 181.4 45.2 47 239.7 60.0 9 8.7 a.2 69 67.0 16.7 39 125.2 31.2 89 183.4 45.5 48 44.6 60.2 10.9.7 a.4 70 67.9 16.9 30 126.1 31.4 99 184.4 46.0 50 44.6 60.4 16.0 10.9.7 1.2 11.0 0.7 2.7 71 68.9 17.2 131 127.1 31.7 191 185.3 46.2 51 44.6 60.4 131 131.4	1 2	2.3		12	63.1	13.7	12			1 23	179. 5		1 22 1	237. 7	20- 3
8 7.8 1.9 68 66.0 16.5 28 124.2 31.2 83 183.4 45.5 48 44.6 60.2 10 9.7 2.2 12 12 12 12 12 12 12 12 12 12 12 12 12		6.8	1.7	67	65.0	16 .	37	123. 2	30. 7	87	181.4		47	210.7	10.8
11 10. 7 2. 7 71 68. 9 17. 2 131 127. 1 31. 7 192 185. 3 46. 2 351 43. 5 60. 7 132 113. 1 130. 9 180. 3 46. 4 53 4 74. 61. 0 131 130. 9 180. 3 46. 4 53 4 74. 61. 0 131 130. 9 180. 3 46. 7 53. 4 45. 61. 0 131 14. 63. 6 75 72. 8 18. 1 35 130. 0 32. 4 93. 185. 3 46. 7 53. 445. 5 61. 4 13. 6 3. 6 75 72. 8 18. 1 35 131. 0 32. 4 93. 185. 3 46. 7 53. 445. 5 61. 4 13. 6 3. 6 75 72. 8 18. 1 35 131. 0 32. 4 93. 185. 3 46. 7 53. 445. 5 61. 4 13. 6 13. 6 75 72. 8 18. 1 35 131. 0 32. 4 99. 190. 4 47. 4 55 48. 4 61. 9 17 17 74. 7 18. 6 37 132. 0 32. 9 99. 190. 4 47. 4 55 48. 4 61. 9 17 17 74. 7 18. 6 37 132. 0 32. 9 99. 190. 4 47. 4 55 48. 4 61. 9 17 17 18. 6 37 132. 0 32. 9 99. 190. 4 47. 4 55 48. 4 61. 9 17 17 18. 6 37 132. 0 32. 9 33. 1 97 190. 1 47. 7 57 40. 4 62. 2 190. 190. 1 47. 9 53 48. 4 61. 9 19 18. 17. 7 19. 1 39 38 133. 9 33. 4 99 190. 1 47. 9 53 48. 4 60. 9 190. 1 47. 9 53 48. 4 61. 9 190. 1 47. 9 18. 6 77. 9 19. 1 39 313. 9 33. 4 99 190. 1 44. 1 90. 1 92. 0 48. 6 23. 3 62. 4 190. 1 90. 1		7.8	1.9		66.0	16.5	28	124. 8	31.0		182.4	45. 5		840.6	60.0
11 10. 7 2. 7 71 68. 9 17. 2 131 127. 1 31. 7 192 185. 3 46. 2 351 43. 5 60. 7 132 113. 1 130. 9 180. 3 46. 4 53 4 74. 61. 0 131 130. 9 180. 3 46. 4 53 4 74. 61. 0 131 130. 9 180. 3 46. 7 53. 4 45. 61. 0 131 14. 63. 6 75 72. 8 18. 1 35 130. 0 32. 4 93. 185. 3 46. 7 53. 445. 5 61. 4 13. 6 3. 6 75 72. 8 18. 1 35 131. 0 32. 4 93. 185. 3 46. 7 53. 445. 5 61. 4 13. 6 3. 6 75 72. 8 18. 1 35 131. 0 32. 4 93. 185. 3 46. 7 53. 445. 5 61. 4 13. 6 13. 6 75 72. 8 18. 1 35 131. 0 32. 4 99. 190. 4 47. 4 55 48. 4 61. 9 17 17 74. 7 18. 6 37 132. 0 32. 9 99. 190. 4 47. 4 55 48. 4 61. 9 17 17 74. 7 18. 6 37 132. 0 32. 9 99. 190. 4 47. 4 55 48. 4 61. 9 17 17 18. 6 37 132. 0 32. 9 99. 190. 4 47. 4 55 48. 4 61. 9 17 17 18. 6 37 132. 0 32. 9 33. 1 97 190. 1 47. 7 57 40. 4 62. 2 190. 190. 1 47. 9 53 48. 4 61. 9 19 18. 17. 7 19. 1 39 38 133. 9 33. 4 99 190. 1 47. 9 53 48. 4 60. 9 190. 1 47. 9 53 48. 4 61. 9 190. 1 47. 9 18. 6 77. 9 19. 1 39 313. 9 33. 4 99 190. 1 44. 1 90. 1 92. 0 48. 6 23. 3 62. 4 190. 1 90. 1					67.0	16. 7		125. 2	31. 2		183.4	45-7		241.6	60.8
12 11.6 2.9 73 69.0 17.4 32 128.1 31.9 99 185.3 40.4 52 244.5 61.2 13 12.6 3.4 74 71.8 17.9 34 130.0 32.4 94 188.2 46.9 54 44.5 61.2 15 14.6 3.6 75 77.8 78.1 13.5 131.0 32.7 95 189.2 47.2 55 44.6 51.1 16 15.5 3.9 70 77.7 71.8 4 35 131.0 32.7 95 189.2 47.4 55 248.4 61.7 17 10.5 4.1 77.4 71.8 35 131.0 32.9 95 190.2 47.4 55 248.4 61.7 18 17.5 4.4 76 77.7 71.8 9 37 133.9 33.1 9 191.1 47.7 57 40.4 62.2 18 17.5 4.4 76 77.7 71.8 9 37 133.9 33.4 96 190.2 47.4 55 248.4 40.2 18 17.5 4.4 76 77.7 71.8 9 37 133.9 33.4 96 190.2 47.6 50 248.4 50 251.3 62.7 18 18 18 18 18 18 18 18		9.7			97.9	10.9					184.4	40.0			Ou 5
13		10.7	2.7		60.9	17.2		127. 1			186.2	46.4	75.		61.0
14 13.6 3.4 74 71.8 71.9 34 130.0 32.4 94 188.2 46.9 54 44.6 61.1 11.1 14.6 3.6 75 72.8 18.1 35 131.0 32.7 95 189.2 47.2 55 44.7 61.7 110 15.5 3.9 76 73.7 18.4 36 132.0 32.9 96 190.2 47.4 55 42.8 46.5 61.1 118 17.5 4.4 75 75.7 74.7 18.9 38 133.9 33.1 97 191.1 47.7 57 42.8 46.5 21.1 119 18.4 4.6 79 70.7 70.7 71.1 39 134.9 33.4 98 199.1 47.9 53 455.3 56.7 120 19.4 4.8 80 77.6 19.4 61.1 135.8 33.9 800 194.1 48.4 60 25.3 35.2 67.1 121 20.4 4.8 80 77.6 19.4 61.1 135.8 34.1 90 195.0 48.5 61.2 48.4 60 25.3 36.7 122 23 23.3 5.0 83 80.5 80.1 43 133.8 34.4 60 195.0 48.5 61.2 48.4 50 25.3 25.2 65.6 144 23.3 5.0 83 80.5 80.1 43 133.8 34.4 60 195.0 48.5 61.2 43.2		12.6	1 77		70.8	17. 7		120.0			187. 3	46. 7		845.5	
10 15.5 3.9 70 73.7 18.4 30 133.0 33.9 90 190.1 47.4 150 248.4 6.2 2 18 17.5 4.4 77 77.7 74 7 18.9 37 133.9 33.1 9 190.1 47.7 55 248.4 6.5 2 18 17.5 4.4 77 77.7 74 7 18.9 37 133.9 33.4 95 190.1 47.7 55 248.4 6.5 2 10 10.4 4.8 80 77.6 19.4 40 33.6 93 193.1 47.9 35 25.3 36.2 7 10 19.4 4.8 80 77.6 19.5 41 135.8 33.4 95 190.1 47.9 35 25.3 36.2 7 10 19.4 4.8 80 77.6 19.5 41 135.8 33.4 95 190.1 48.4 59 25.3 36.2 7 10 19.4 4.8 80 77.6 19.5 41 135.8 33.4 95 190.1 48.4 59 25.3 36.2 7 12 22 23 23 23 35 53 83 79.6 19.8 42 137.8 34.4 00 190.0 48.9 62 25.2 25.2 55.1 22 23 23 23 35 16 85 85 25 20.3 44 139.7 34.1 00 197.0 48.5 66 25.2 25.2 05.6 24.4 23.3 5.6 85 85.5 20.3 44 139.7 34.1 00 197.0 48.6 64 25.2 25.6 05.6 24.4 23.3 5.6 85 85.5 20.3 44 139.7 34.1 00 197.0 48.6 64 25.2 25.2 05.6 24.4 23.3 5.6 85 85.5 20.3 44 139.7 34.1 00 197.0 48.6 64 25.2 25.2 05.6 25.2 25.2 25.2 25.2 25.2 25.2 25.2 2	14	13.6	3.4	74	71.8	17.9	34	130.0	32. 4	94.	188. 2	46.9	54	846.5	61.4
10 15.5 3.9 70 73.7 18.4 30 133.0 33.9 90 190.1 47.4 150 248.4 6.2 2 18 17.5 4.4 77 77.7 74 7 18.9 37 133.9 33.1 9 190.1 47.7 55 248.4 6.5 2 18 17.5 4.4 77 77.7 74 7 18.9 37 133.9 33.4 95 190.1 47.7 55 248.4 6.5 2 10 10.4 4.8 80 77.6 19.4 40 33.6 93 193.1 47.9 35 25.3 36.2 7 10 19.4 4.8 80 77.6 19.5 41 135.8 33.4 95 190.1 47.9 35 25.3 36.2 7 10 19.4 4.8 80 77.6 19.5 41 135.8 33.4 95 190.1 48.4 59 25.3 36.2 7 10 19.4 4.8 80 77.6 19.5 41 135.8 33.4 95 190.1 48.4 59 25.3 36.2 7 12 22 23 23 23 35 53 83 79.6 19.8 42 137.8 34.4 00 190.0 48.9 62 25.2 25.2 55.1 22 23 23 23 35 16 85 85 25 20.3 44 139.7 34.1 00 197.0 48.5 66 25.2 25.2 05.6 24.4 23.3 5.6 85 85.5 20.3 44 139.7 34.1 00 197.0 48.6 64 25.2 25.6 05.6 24.4 23.3 5.6 85 85.5 20.3 44 139.7 34.1 00 197.0 48.6 64 25.2 25.2 05.6 24.4 23.3 5.6 85 85.5 20.3 44 139.7 34.1 00 197.0 48.6 64 25.2 25.2 05.6 25.2 25.2 25.2 25.2 25.2 25.2 25.2 2	15	14.6] š. 6	75	72.8	18.1	35	131.0		95	189. 2	47. 2	55	247.4	61.7
18	10	15.5	J 3-9	<u></u>	73.7	18.4	30	132.0	32.9	90	190.8	47-4	50	248. 4	61.9
12 19.4 4.8 80 77.6 19.4 40 135.8 33.9 800 194.1 48.4 60 253.2 63.1 22 21.3 5.3 82 79.6 19.8 42 137.8 34.4 60 195.0 48.5 65 253.2 63.1 23 23.3 5.0 83 80.5 80.1 43 137.8 34.4 60 195.0 48.9 66 255.2 63.6 44 23.3 5.8 84 81.5 80.3 44 139.7 34.8 64 107.9 49.4 64 255.2 63.6 45 23.3 5.8 84 81.5 80.3 44 139.7 34.8 64 107.9 49.4 64 257.1 64.1 45 25 25 25 25 25 25 25	1 14 1	17.5	1 2 4	146	75.7	18.0	36	132.9	33. 4	1 24		47. 0	1 24	250.2	
12 19.4 4.8 80 77.6 19.4 40 135.8 33.9 800 194.1 48.4 60 253.2 63.1 22 21.3 5.3 82 79.6 19.8 42 137.8 34.4 60 195.0 48.5 65 253.2 63.1 23 23.3 5.0 83 80.5 80.1 43 137.8 34.4 60 195.0 48.9 66 255.2 63.6 44 23.3 5.8 84 81.5 80.3 44 139.7 34.8 64 107.9 49.4 64 255.2 63.6 45 23.3 5.8 84 81.5 80.3 44 139.7 34.8 64 107.9 49.4 64 257.1 64.1 45 25 25 25 25 25 25 25	19	18.4	4.6	79	76.7	19. i	39	134.9	33. 6	99	193. 1	48 í	59	251. 3	62. 7
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\$\frac{5}{5}\$ \ \frac{5}{4}\$ \ \frac{1}{3}\$ \ \ \ \frac{1}{3}\$ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \		47.5	12.1		100.7	20.8		161.0	45.9			35. 4		280. 4	70.8
\$\frac{5}{5}\$ \ \frac{5}{4}\$ \ \frac{1}{3}\$ \ \ \ \frac{1}{3}\$ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \		40. 6				26.0		166.0							
\$\frac{5}{5}\$ \ \frac{5}{4}\$ \ \frac{1}{3}\$ \ \ \ \frac{1}{3}\$ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	l to l	50.5	12.6	12	108. 7	27. 1	72	166.9	41.6	32	225. 1	56. i	93	281. 1	70.6
\$\frac{5}{5}\$ \ \frac{5}{4}\$ \ \frac{1}{3}\$ \ \ \ \frac{1}{3}\$ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	\$3	51.4	12.8	13	109.6	27.3	73	167. 9	41.9	33	226, 1	56.4		284. 2	70.9
\$6 \$4.\$ 1 \$1.\$ 15 \$110.\$ 6 \$8.\$ 1 \$76 \$170.\$ 8 \$4.\$ 5 \$36 \$10.\$ 6 \$75.\$ \$1.\$ 6 \$75.\$ \$1.\$ 6 \$75.\$ \$1.\$ 6 \$75.\$ \$1.\$ 6 \$10.\$ 6 \$8.\$ 1 \$76 \$171.\$ 7 \$43.\$ 8 \$37 \$10.\$ 9 \$78.\$ 20.\$ 9 \$78.\$ 274.\$ 9 \$15.\$ 50.\$ 3 \$14.0 \$18 \$114.\$ 5 \$85.\$ 79 \$172.\$ 7 \$43.\$ 1 \$38 \$130.\$ 9 \$7.\$ 6 \$25.\$ 3 \$97 \$182.\$ 175.\$ 6 \$9.\$ \$14.\$ 1 \$114.\$ 1 \$15.\$ 1 \$15.\$ 5 \$1.\$ 6 \$79 \$172.\$ 7 \$43.\$ 1 \$38 \$130.\$ 9 \$7.\$ 6 \$1.\$ 9 \$1.\$ 9 \$1.\$ 1 \$75.\$ 1 \$75.\$ 9 \$1.\$ 1 \$75.\$ 1 \$7	54	52.4		!#	110.6	27.0	74	100.8	43, 1	34	227.0	50.6	94	285. 3	71. 1
57 53.3 13.8 17 113.5 88.3 77 171.7 44.8 37 38.30.0 57.3 97 288.2 71.9 85 50.3 14.0 18 114.5 28.5 73 172.7 43.1 38 230.0 57.0 50 289.1 72.1 59 57.2 14.3 19 115.5 28.8 79 173.7 43.1 3 39 231.9 57.8 99 290.1 72.3 60 50.2 14.5 20 110.4 29.0 89 174.7 43.5 40 232.9 50.1 300 291.1 72.5 Dist. Dep. Lat. Lat. Dist. Dep. Lat. Lat. Dist. Dep. Lat. Dist. Dep. Lat. Dist. Dep. Lat.	뭥	35.4	13. 3	1 18	112.6	1 26.	1 🔏	170.8	44.8	1 23		1 57. 1	1 23 1	287. 0	71.8
60 58. a 14. 5 so 116. 4 sp. 0 80 174. 7 43. 5 40 232. 9 58. 1 300 291. 1 72. 6 Dist. Dep. Lat. Dist. Dep. Lat. Dist. Dep. Lat. Dist. Dep. Lat. Dist. Dep. Lat.	57	\$5.3	13.8	17	113.5	88, 3	77	171.7	42.8	37	830.0	57.3	97	288.2	71.9
60 58. a 14. 5 so 116. 4 sp. 0 80 174. 7 43. 5 40 232. 9 58. 1 300 291. 1 72. 6 Dist. Dep. Lat. Dist. Dep. Lat. Dist. Dep. Lat. Dist. Dep. Lat. Dist. Dep. Lat.	58	56. 3	14.0		114. C	88. Š	78	,172. 7			230.7	57. 6			72. 1
Dist. Dop. Lat.	1 22	57. 2			115.5	25. 5	72	173.7		39	231.9	57.8	.99		72. 3
		30. 2	44.5		110.4	29. 0	ـــّــا	174.7	43.5	40	232. 9	30. 1	300	291. I	72.0
For 16 Decrees.	Dist.	Dep	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat	Dist.	Dep.	Lat.
					·								[Fa	76 Denz	985.

DIFFERENCE OF LATITUDE AND DEPARTURE FOR 15°.

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Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist	Lat.	Dep.	Dist.	Lat.	Dep.
-	1.0	0.3	61	58.9	15.8	121	116. 9 117. 8	31. 3	181	174.8	46, 8	241	232.8	62.4 62.6
2	1.9	0.5	62	59.9	16.0	22	117. 8 118. 8	31. 3 31. 6	82	175. 8 176. 8	47. I	42	233.8	62.6
3	2. 9		63	60, 9 61, 8	16. 3 16. 6	23	118, 8	31.8	83	176.8	17.6	43	234. 7	62. 9 63. 2
4	3. 9 4. 8	1.0	64	62, 8	16, 8	24	119, 8 120, 7	32, I 32, 4	84	177. 7 178. 7	47.0	44	235. 7 236. 7	63.4
ş	4.8 5.8	1.3 1.6	65 66	63.8	17. 1	25 26	121.7	32,6	85 86	179.7	47. 9 48. 1	45	236. 7 237. 6 238. 6	63. 7
	6.8	1.8	67 68	64.7	17. 3 17. 6	27 28	122. 7	32.9	87 88	179. 7 180. 6	48. 4	47	238.6	63.9
3	7. 7 8. 7	2. 1		65. 7 66. 6	17.6		123. 6	33. I		181.6	42.7		239.5	64.2
9	8. 7	2. 3 2. 6	69	66, 6 67, 6	17.9 18.1	29	124. 6 125. 6	33. 4 33. 6	89 90	182, 6 183, 5	48.9 49.2	49 50	240. 5 241. 5	64.4
11	9.7	2, 8	70 71	68, 6		30 131	126. 5	33.9	191	184.5	49.4	251	242.4	65.0
12	11.6	3.1	72		18. 4 18. 6	32	127. 5	34.2	92	185. 5	49.7	52	243.4	65.2
13	12, 6	3.4	73	69. 5 70. 5	18.9	33	127. 5 128. 5	34-4	93	186.4	50.0	53	244-4	65.5
14	13. 5	3. 4 3. 6	74	71.5	19. 2	34	129.4	34-7	94	187. 4 188. 4	50.2	54	245. 3 246. 3	65.7
15	14. 5 15. 5 16. 4	3.9	75 76	72.4	19.4	35 36	130, 4 131, 4	34- 9 35. 2	95 96	189. 3	50. 5 50. 7	55 56	240.3	66.3
17	16.4	4.1 4.4	70	73- 4 74- 4	19.7	30	132. 3	35.5	97	190.3	51.0	37	247. 3 248. 2	66.5
18	17.4	4.7	77 78	75.3	20, 2	37 38	133. 3	35. 7 36. 0	97 98	191.3	51. 2	57 58	249.2	66. § 66. 8
19	17. 4 18. 4	4-9	79	75.3 76.3	20. 4	39	134. 3	36. ó	99	192. 2	51. 5 51. 8	59	250.2	07.0
20	19. 3	5. 2		77-3	20. 7	40	135. 2	36. 2	200	193. 2	51.8	261	251, I 252, I	67. 3 67. 6
21 22	20. 3	5.4	81 82	78. 2	21.0	141	136, 2	36. § 36. 8	20I 02	194.2	52. 0 52. 3	62	252. I	67.8
23	21, 3	5. 7 6. 0	83	79. 2 80. 2	21. 5	42 43	137. 2 138. 1	37.0	03	195. 1 196. 1	52.5	63	254.0	67.8 68.1
24	23. 2	6.2	84	81, 1	21.7	44	139.1	37. 3	04	197. 0 198. 0	52. § 52. 8	انشا	255.0	68.3 68.6
25 26	24. [6.5	85 86	82, 1	22, 0	45 46	140. I	37- 5	05 06	198.0	53. I	65	256.0	68.8
	25. I 26. I	6.7	86	83. 1 84. 0	22. 3	40	141.0 142.0	37. 5 37. 8 38. 0	00	199.0	53. 3 53. 6	67	256.9	69.1
27 28	20.1	7.0	87 88	85.0	22. 5 22. 8	47 48	143.0	38.3	07 08	200, 9	53.8	67 68	258.9	69.4
29	27. 0 28. 0	7.5	89	8ŏ. o	23. 0	49	143.9	28.6	09	201, 9	54. I	69	257. 9 258. 9 259. 8 260. 8	69.6
30	29.0	7. 5 7. 8	90	86.9	23. 3	50	144.9	38. 8	10		54-4	70	200.8	69.9
31	29.9	8.0	91	87. 9 88. 9 89. 8	23, 6	151	145. 9 146. 8 147. 8 148. 8	39. I	211	203, 8 204, 8	54.6	27I 72	261.8 262.7	70. I 70. 4
32 33	30. 9	8.3	92 93	80.9	23. 8 24. I	52 53	140. 8	39. 3 39. 6	13	205.7	54. 9 55. I	72	262.7	70.7
33	31. 9 32. 8	8.5	94	90.8	24.3	54	148.8	39.9	14	206.7	55. 4 55. 6	74	264. 7 265. 6	70.9
35 36	22.8	9.1	95 96	91.8	24. 3 24. 6	55 56	149.7	40, I	15 16	207.7	55.6	74 75 76	265.6 266.6	71.2
36	34.8	9.3 9.6	96	92. 7	24.8	50	150. 7 151. 7	40.4	10	208.0	55. 9 56. 2	70	267.6	71.4
37 38	35. 7 36. 7	9.6	97 98	93-7	25. P	57 58	152.6	40.9	17 18	210,6	56.4	77 78	267. 6 268. 5	72.0
39	37· 7 38. 6	10, 1	99	94°7 95.6 96.6	25. 4 25. 6	59	153.6	41. 2	19	211.5	56. 7	79	269.5	72. 2
40	38. 6	10.4	100	96.6	25.9		154. 5	41.4	20	212.5	56.9	281	270.5	72.5
41	39.6	10, 6	101	97. 6 98. 5	26, I 26, 4	161 62	155. 5 156. 5	41.7	22 I 22	213. 5	57. 2 57. 5	281 82	271.4 272.4	72. 7 73. 0
43 43	40.6	10.9	02 03	98.5	26. 7	63	157.4	42. 8	23	215.4	37. 7	82	273.4	72.2
44	42.5		04	100.5	26.9	64	157. 4 158. 4	42.4	24	216.4	57. 7 58. 0	84	274.3	73. 5 73. 8
45 46	43- 5	11.4	05 06	101.4	27. 2	65	159.4	42. 7	25 26	217. 3	58. 2	85 86	275.3 276.3	73.8
46	44-4	11.9	00	102, 4	27.4 27.7	67	160, 3	43. 0 43. 2	20	218.3	58. 5 58. 8	87	277. 2	74-3
47 48	45. 4 46. 4	12, 2	97 08	104.3	28.0	67 68	161.3 162.3	43. 5	27 28	220, 2	59.0	87 88	278.3	74.5
49	47.3 48.3	12. 7	09	105. 3	28, 2	69	163.2	43-7	29	221.2	59-3	89	279. 2 280. I	74.8
50		12.9	10		28, 5	70	164.2	44.0	30	222, 2	59. 5 59. 8	90	280, 1	75. 1
51	49- 3	13.2	111	107. 2	28. 7	171	165.2 166, 1	44-3 44-5 44-8	231	223. I 224, I	59. 8 60. 0	29I 92	281.1	75-3 75-6 75-8 76.1
52 53	50. 2 51. 2	13.5	13	109. 1	29.0 29.2	72 73	167. 1	1 44.8	32 33	225. 1	60.3	93	283.0	75.8
54	52. 2	14.0	14	110.1	29.5	74	167. 1 168. 1	45.0	34	226.0	60. 3 60. 6	94	284.0	76.1
54 55 56	53. 1	14.2	15	111.1		75 76	169.0	45. 3 45. 6	35 36	227. 0 228. 0	60.8	95 96	284.9 285.9	
56	54. 1	14. 5 14. 8	10	112.0	30, 0 30, 3	J 7º	170.0	45. 8	30	228.9	61. 2	97	256.0	76.6
57 58	55. I 56. 0	15.0	17 18	114.0	30.5	77	171.9	45.8 46.1	37 38	229.9	61.3	97 98	287. 8 288. 8	77. 1
59	57. 0	15.3	19	1149	30. 5 30. 8	79	172.9	46. 3 46. 6	39	230. 9 231. 8	61.9	99	288,8	77-4
60	57. 0 58. 0	15.5	30	115.9	31. I	80	173.9	46.6	40	231.8	62, 1	300	289.8	77.6
Dist.	Dep.	Let.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Let.
Г'						•				•		[Fo	r 75 Degi	ecs.

<u> </u>														
Diet.	Lat.	Dep.	Dist.	Lat	Dep.	Dist.	Let.	Dep.	Dist.	Lat	Dep.	Dist.	Lat	Dep.
1 :	1.0	23	6i 62	58.6	16, 8	121	116.3	33. 4 33. 6	181 82	174.0	49.9	241	231. 7 232. 6 233. 6	66.4
3	1.9	0.8	63	59.6 60.6	17.1	22 23	117. 3	33.9	82	174.9	50. 8	42 43	332.6	67.0
4	2.9 3.8	1, 1	64	61.5	17. 4	24	119. 2	34.3	83 84	175.9 176.9 177.8	50. 4 50. 7	44	234. 5	67. 3
ş	3.8 4.8 5.7	1:4	65	62. 5 63. 4	17.9	25 26	120, 2	34. 5 34. 7	85 86	177.8	51.0	45	234- 5 235- 5 230- 5	67. § 67. 8
7	6.7	1.9	67 68	64.4	18. 5	27 28	122, 1	35. 0	87 88	179.8	51. 5 51. 8	47	237.4 238.4	100.I
,	1.7	1 ::	69	65.4 66.3	18.7	98 90	123.·0 124. 0	35. 3 35. 6	88 89	180. 7	51.8	48 49	238.4 239.4	68.4 68.6
10	9.6	2.5	70	67.3	19.3	3ó	125.0	35.8	90	182. 6	52.4	50	240. 3	68.9
111	10, 6	3.0	71	68, 2	19.6	131	125. 9 126. 9 127. 8 128. 8	36, I	191	183.6	52.6	251	241. 3 242. 2	69.2
13	11.5	3.3	72 73	70. 2	19. 8 20. I	32 33	127. 8	36. 4 36. 7	92 93	184. 6 185. 5	52, 9 53, 2	52 53	243. 2	69. 5 69. 7
اغتا	12. 5 13. 5	3.9	74	71.1	20.4	34	128.8	36. 7 36. 9	94	l 186. s	53-5	I 54 I	244. 2	70.0
15 16	14.4	44	75	72. I 73. I	20. 7 20. 9	35 36	129.8	37. 2 37. 5	95 96	187.4	53. 7 54. 0	55 56	245. I. 246. I	70. 3 70. 6
17	15.4 16.3	4.7	77	74.0	21.2	37 38	130. 7 131. 7	37. 8	97 98	189.4	54.3 54.8	57 58	247.0 248.0	70.8
38 10	17.3	5.0 5.2	78	75.0	21.5	38	132. 7 133. 6	38, 0	98 99	190. 3 191. 3	54.6 54.9	58	245. 0 249. 0	71. 1 71. 4
20	19. 2	5.5	79	75.9 76.9	22, 1	39 40	134.6	38. 3 38. 6	200	192.3	55.1	32	249.9	71.7
31	20, 2	8.3	81	77. 9 78. 8	22. 3 22. 6	141	135. 5 136. 5	38.9	201	193. 2	55. A	261	\$50. Q	71.9
23 23	21. I 22. I	6.1	82 83	78.8	22. 6	42 43	136. 5	39. I 39. 4	02	194.8	55. 7 56. 0 56. s	6a 63	251. 9 252. 8	72. 2
84	23. I	6.6	84	80.7	83.8	44	137. 5 138. 4	39-7	04	195. I 196. I	56. 2	64	253. 8	72.8
25	24.0	6. 9 7. 2	84 85 86	81. 7 82. 7	23. 4 23. 7	45	139. 4	40.0	95	197.1	56. 5 56. 8	45.8	254 7	73.0
27	25. 0 20. 0	7.4	87 88	83.6	24.0	47	140. 3 141. 3 142. 3 143. 2	40.5	97	199.0	57. 1	67 68	255. 7 256. 7 257. 6 258. 6	73. 3 73. 6
28 20	26, q	7.7	88 89	84.6	24.3	47 48	142. 3	40.5		199.9	57. 1 57. 3 57. 6		257.6	73-9
30	27. 9 28. 8	8.3	99	85. 6 86. 5	24. 5 24. 8	49 50	144. 2	41. I 41. 3	09 10	201. 0	57.6	69 70	259.5	74- I 74- 4
31	· 29. 8	8. ş 8. 8	91	87. 5 88. 4	25. 1	151	145. 2	41,6	211	202. 8	57·9 58.2	271	260, E	74-7
32 33	30. 8 31. 7	8.8 9.1	92 93	89.4	25. 4 25. 6	5a 53	146. I 147. I	41.9 42.2	12	203. 8 204. 7	58.4 58.7	72 73	261 5 262, 4	75. 0 75. 2
34	32.7	9.4	94	90.4	25. 9 26. 2	54	148,0	42.4	14	205.7	59.0	74	961.A	75. 5
34 35 36	32. 7 33. 6 34. 6	9.4 9.6	95 96	91. 3 92. 3	26.5	55 56	149.0	42.7	15	206. 7	59-3	75 76	264.3	75.8
37	35.6	9.9	97	92.3	20. 5	30	150. 0 150. 0	43.0	17	207. 6 207. 6 208. 6	59. 5 59. 8 60. 1	77	265. 3 266. 3	76.4
37 38	35. 6 36. 5	10.5	97 98	94. 2	27. 0	57 58	150. 9 151. 9 152. 8	43. 3 43. 6	17	209, 6	60, 1	77 78	267. 2 268. 2	75. B 76. 4 76. 9
39 40	37. 5 38. 5	10. 7 11. 0	100	95.4 96.1	27. 3 27. 6	50	152. 8 153. 8	43.8 44.1	19	210. 5 211. 5	60. 4 60. 6	79 80	269. 2	70.9 77.2
41	39-4	11.3	101	97. I 98. o	27. 8 28. 1	161	154.8	44-4	221	212.4	60.9	281	270. I	77.5
42 43	40. 4 41. 3	11.6	03 03	98.0 99.0	28. 1 28. 4	62 63	155. 7 156. 7	44.7	22	813.4 214.4	61. 2 61. 5	82 83	271. I 272. O	77.7 78.0
44	42.3	12. 1	04	100.0	28. 7	64	157. 6 158. 6	44.9 45.2	23	215.3	61. 7	84 I	273.0	78. 3 78. 6
45	43-3	12.4	જુ	100.9	28. 9	3.2.8	158.6	45.5	25	216.3	68. 0	85 86	274.0	78.6 78.8
47	44. 2 45. 8 46. 1	13.0	37	101.9	29. 2 29. 5 29. 8	67 68	159. 6 160. 5	46.0	27 28	218. 2	62. 3 62. 6	87 88	274- 9 275- 0	78. 8 79. 1
47	46. 1	13.2		102, 9 103, 8 104, 8	ag. B		161.5	46. 3 46. 6		219. 2	62, 8	88	275. 9 270. 8	79-4
49 50	47.1	13.5	99	105.7	30. 0 30. 3	69 70	162. 5 163. 4	46. 9	30	220, I 221, I	63. I 63. 4	89 90	277. 8 278. 8	79-7
51	49.0	14.1	111	106. 7	30,6	171	164.4	47-1	231	222. I	63.7	291	279. 7	79-9 80.2
52 53	50. ø	14.3 14.6	12	107. 7	30, 9 31, 1	72	165. 3 166. 3	47-4	32	223.0 824.0	63.9	98 93	280. 7 281. 6	80. 5 80. 8
54	51.9	14.9	14	109.6	31.4	73 74	167. 3 168, s	47. 7 48. 0	33 34	824.0	444	94	282.6	81, 0
55 56	58.9	15.2	15	110.5	31. 7	75	168, s 169, s	48.21	35 36	225. 9 226. 9 227. 8	64.8	95 96	283. 6 284. 5	81. 3 81. 6
57	K4. 8	15.4	17 18	111.5	32, 8	70	170. I	48. 5 48. 8	37	227. 8 227. 8 228. 8	65. 3 65. 6	97	285. 5 286. 5	81. q
57	55.8 50.7	16.0		113.4	32, 5 32, 8	77	171. 1	49. 1	37 38	228, 8	65. 6	97 98	286. 5	82. i
32	56. 7 57. 7	16. 3 16. 5	19	114.4	32. 8 33. 1	79	172. 1 173. 0	49.3 49.6	39 40	229. 7 230. 7	65. 9 66. 2	300	287. 4 288. 4	82. 4 82. 7
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	Dist. Dep. Lat.													
L												f Lot	74 Degr	res.

	DIFFERENCE OF LATITUDE AND DEPARTURE FOR 17°.													
Dist.	Lat	Dep.	Dist.	Lat.	Dep.	Dust.	Lat.	Dop.	Dist.	Lat.	Dep.	Dist.	lat.	Dep.
1	1.0	23	61 62	58. 3	17.8	121	115.7	35-4	181 82	173. I 174. 0	52, ¢	241 43	#30. 5 #31. 4	70. 5 70. 8
3	2. 9 3. 8	0.9	63	\$9. 3 60. 2	18.4	23	116. 7 117. 6 118. 6	35. 7 36. 0	81	175.0	53.5	43	232.4	71.0
4		1	64	61, 2	18.7	1 **	118.6	1 76. 7	84	176.0	53. 5 53. 8	1 44	233.3	71.3
ş		1.5	65	63.1		25	120, 5	36. 5 36. 8	85 86	177.9	54.1	45	234. g 235. g 236. 2	71.9
7	§. 7	2.0	67	64.1	19.3 19.6	27	121.5	37. I	87 88	178.8	54-4 54-7	47	236.2	72. 2
٥	7.7	2.3	69	65.0	19. 9 20. 2	29	122, 4	37·4 37·7	89	179. 8 180. 7	55. o	49	237.2 238.1	72.5
10	9.6	2.9	70	66.9	20.5	30	124.3	37.7 38.0	96	181.7	55. 3 55. 6	50	239. 1	73. 1
11	10. 5 11. 5	3.2	71 72	67. 9 68. 9 69. 8	90. 8 31. 1	131	125. 3 126. 2	38. 3 38. 6	191 92	181. 7 183. 6	55. 8 56. 1	251 52	240. 0 241. 0	73· 4 73· 7
13	12.4	3. § 3. 8	73	69.8	21.3	33	127. 2	38.9	93	1 1R4 6	56.4	53	241.0	74.0
14	13.4 14.3	4.1	74	70.8	21.6	34	128. I 129. I	39. 2	94	185. 5 186. 5	56. 7 57. 0	54	242.9	74-3 74-6
15 16	15. 3	4.7	73	72.7	22, 2	35 36	130.1	39. § 39. 8	95 96	187.4	57. 3 57. 6	55 56	243. 9 244. 8	74.8
17	16, 2	5.0	77	73.6.	22. 5 22. 8	37 38	131.0 132.0	40, I	97 98	188.4	57.6	57 58	245. 8 246. 7	1 7 C. I
.19	17. 2 18. 2	5.3	72	75- 5 76- 5	23. I	39	132.0	40. 3 40. 6	99	190. 3	57. 9 58. 8	59	247. 7 248. 6	75.4 75.7 76.0
20	19.1	5.8	86 81	76.5	23.4	40	133.9	40.9	200	191.3	58. 5	261		76.0
21	20, 1 21, 0	6.1	81 82	77.5 78.4	23. 7 24. 0	141	134. 8 135. 8	41.3	201	192. 2 193. 2	58.8	62	249. 6 250. 6	76.3 76.6
23	22. 0	6.7	83	79.4 80.3	24.3 24.6	43	135.8 136.8	41. 5 41. 8	03	194. I	59. 4 59. 6	63	251.5	176.a
24	23. 0 23. 9	7.0	84 85	81.3	24.0	44	137. 7 138. 7	42. 1 42. 4	04 05	195. I 196. o	59.0 59.9	64	252. 5 253. 4	77. 2
25 26	24. 9	7.3	85 86	82.2	25. 1	45	139.6	42. 7	3	197.0	60, 2	5	254.4	77. 5 77. 8 78. 1
27	24. 0 25. 8 20. 8	7.9	87 88	83. 2 84. 2	25.4	47	140. 6 141. 5	43.0	3	198.0	60, 5 60, 8	67 68	255. j 256. j	78. I
29	\$7.7 \$8.7	8.5 8.8	89	85. I 86. I	25. 7 26. 0	49	142.5	43. 3 43. 6	9	199.9	61. I	69	257.2 258.2	78.4 78.6
30			90	86. I	26. 3	50	143. 4	43.9	10		61.4	70		78.9
31 32	29. 6 30. 6	9.1	91 92	87. 0 88. 0	26, 6 26, 9	151 52	144-4 145-4	44. 1 44. 4	211	201.8	61. 7 62. 0	271 72	259. 2 200. I	79.8
33	31.6	9.4 9.6	93	88.a	27. 2	53	145. 4 146. 3	44.7	13	203.7	62. 3 62. 6	73	261. I	79-5 79-8 80-1
34	3a. 5 33- 5	9.9	94	89. 9 90. 8	27. 5 27. 8 28. 1	54	147. 3 148. 2	45.0	14	204.6	62.9	74	262, 0 263, 0	80.1
35 36	34.4	10, 5 10, 8	95 96	91.8	28, 1	55 56	149. 2	45. 3 45. 6	15	205.6 206.6	63. 3	75	263.9	80.7
37 38	35· 4 36. 3	10. 8	97 98	92. 8 93. 7	28. 4 28. 7	57 58	150, 1 151, 1	45.9 46.2	17	207. 5 208. 5	63.4 63.7	77	264.9 265.0	81.0
39	37· 3 38. 3	11.4	99	94- 7 95. 6	1 28. g	59	152, 1	46.8	19	209.4	64.0	72	265. 0 266. 8	81. 3 81. 6
40		11.7	100	95.6	89. 8	161	153.0		20	210.4	64. 6	80 281	267. 8 268. 7	81.9
41 42	39. s 40. s	12, 0	101	97.5	29. 5 29. 8	62	154. 0 154. 9	47. I 47. 4	221	211.3	64.9	82	269. 7 269. 7 270. 6	82.4
43	41. I	12.3 12.6	03	97. 5 98. 5	30. I	63	155. 9 156. 8	47. 7	23	213.3	65.2	83 84	270. 6 271. 6	82. 7 83. 0
44	42. I 43. 0	12.9 13.2	O4 O5	99. 5 100, 4	30.4	456	157.8	47.9 48.2	24 25 26	214.2	65. 5 65. 8 66. 1	85 86	272.5	82.2
45 46	44.0	13.4	ુ જ	101.4	31.0	66	157. 8 158. 7	48. 5 48. 8	26	215. 2 216. 1	66. 1	86	273.5	83.6
47	44. 9 45. 9	13.7	97 08	102. 3	31. 3	67 68	159. 7 160. 7	48. 8 49. I	27 28	217. I 218. 0	66.4 66.7	87 88	274. 5 275. 4	83. 9 84. 2
49	45. 9 46. 9 47. 8	14.3	09	104. 2	31.9	69	161.6	49.4	29	219.0	67. 0	89	275. 4 276. 4	84.5
50 51	47. 8	14.6	111	105. 2 106. I	32. 2	70 171	162. 6	49-7 50-0	30 231	220, 0	67. 2	90 291	277. 3 278. 3	84. 8 85. 1 85. 4 85. 7 86. 0
52	49.7	15. 2	12	107. 1	32. 7	72	164. 5	50. 3 50. 6	32	£21. 0	67. 5 67. 8 68. 1	92	279. 2 280. 2	85.4
53 54	50. 7 51. 6	15. 5 15. 8	13	108, 1	33. 0	73	165.4 166.4	50. 6 50. 9	33	222, 8 223, 8	68. ı 68. 4	93	280, 2 281, 2	85. 7 86. 0
**	52, 6	16. 1	14 15	110.0	33- 3 33- 6	74 75	167. 4 168. 3	51. 2	34 35	224.7	68.7	94 95 96	282, I	86, s
55 56	53.6	16.4	15 16	110.9	33 9	75 76	168. 3	51.5	35 36	225. 7 226. 6	69.0	96	283, I 284, O	86. 5 86. 8
57 58	54- 5 55- 5	16. 7 17. 0	17 18	111.9	34. 2 34. 5	77 78	169. 3 170. 2	51. 7 52. 0	37 38	227.6	69.3 69.6	97 98	285.0	87. 1
59 60	55. 5 56. 4	17.2	19	113.8	34.8	79	171. 2	52. 3 52. 6	39	227. 6 228. 6	69.9	99	285. 9 286. 9	87.4
\vdash	57-4	17.5	20	114.8	35. 1		172. 1		40	229. 5	70. 8	300		87. 7
Dist.	Dist. Dep. Lat. FFO 73 Degrees.													
		-										[rot	13 regr	oca.

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DIFFERENCE OF LATITUDE AND DEPARTURE FOR 18°.

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	1.0	a 3	61	58.0	18.9	121	115. 1	37-4	181	172. 1	55.9	241	229. 2	74.5
2	1.9		62	59.0	19. 2	22	116.0	37. 7 38. o	82	173.1	56.2	42	230, 2	74. 5 74. 8
3	2.9 3.8	0.9	63 64	59.9	19. 5 19. 8	23 24	117.0	30.0	83 84	174.0 175.0	56. 6 56. 9	43 44	231. I 232. I	75. 1 75. 4
5	4.8	1.5	65	60.9	20. I	25 26	118.0	38. 3 38. 6	85 86	175.9	57. 2	45 46	233.0	75.7
	ş. <u>7</u>	1.9		62.8	20, 4		119.8	38.9	86	176.9	57. 5	46	234. 0	75. 7 76. 0
7	2.6	2.3	68	63. 7	20.7	27 28	120, 8	39. 2 39. 6	. 87 88	175. 9 176. 9 177. 8 178. 8	57. 5 57. 8 58. 1	47	234.9	76. 3 76. 6
9	5. 7 6. 7 7. 6 8. 6	2. 5 2. 8	69	64. 7 65. 6 66. 6		29	122. 7	39.9	89	179.7	58.4	49	235. 9 236. 8	76.9
10	9.5	3.1	70	66, 6	21. 3 21. 6	30	123.6	40, 2	90	180. 7	58. 7	50	237.8	77-3
11	10.5	3.4	71 72	67. 5 68. 5	21.9	131	124.6	40. 5 40. 8	191	181.7	59. 0	251	238. 7	77.6
13	11.4	3.7	73	69.4	22.6	32 33	125. 5 126. 5	41.1	92 93	181.6	59. 3 59. 6	52 53	239. 7 240. 6	77.9 78.2
14	13.3	4.3	74	70.4	22.9	34	127.4	41.4	94	184.5	59.9	54	241.6	78. 5 78. 8
15	14.3	4.6	75 76	71.3	23.2	35 36	128.4	41.7	95 96	185. 5	59. 9 60. 3 60. 6	55 56	242. 5	
	15. 2 16. 2	4.9	7º	72.3	23. 5 23. 8	30	129. 3	42.0	90	187.4	60.9	50	243. \$ 244. 4	79.1
17 18	17.1	5. 3 5. 6	77	74.3	24. 1	37 38	131.2	42.3	97 98	187. 4 188. 3	61. 2	57 58	245.4	79-4 79-7 80.0
19		5.9 6.2	72	75. 1 76. 1	24.4	39	132, 2	43.0	99	189.3	61.5	59	245.4 246.3	80.0
20	19.0	0. 2	81	70.1	24.7	40	133.1	43-3	200	190, 2		261	247.3	80. 3
2 I 22	20.0	6, 5	82	77. ° 78. °	25.0	141 42	134. I	43.6 43.9	201 02	191. 2 192. I	62, 1 62, 4	62	248, 2 249, 2	80. 7 81. 0
23	21.9	7. 1	83	78. q	25. 3 25. 6 26. 0	43	135. I 136. 0	44.2	03	193. 1	62. 7	63	250. I	81.3 81.6
24	22, 8	7.4	I 8₄	79.9	26.0	44	137.0	44.8	04	194.0	63.0	64	251. 1	81.6
25 26	23.8 24.7	7.7	85 86	81.8	26. 3 26. 6	45	137. 9 138. 9	44.8	05 06	195.0	63.3	65	252. 0 253. 0	81.9 82, 2
27	25. 7	8.2	87 88	82. 7	26.9	47	139.8	45. 1 45. 4	07	196.9	64.0	67	253. 0	82. 4
28	25. 7 26. 6	8.7		83. 7 84. 6	27. 2	47 48	140.8	45. 7 46. 0	.27	197. 8	64.2	67	254. 9 255. 8	82. 5 82. 8
29	27. 6 28. 5	9.0	89	84.6	27. 5	49	141.7	46.0	09	198, 8	64.6	69	255.8	83. I
30 31	20.5	9.3	90 91	86.5	28. 1	50 151	142. 7	46.4	211	199. 7 200. 7	64.9	70 271	256.8	83.4 83.7
32	30.4	9.9	92	87.6	28.4	52	144.6	47.0	112	200, 7 201, 6	65.5	72	257. 7 258. 7 259. 6 260. 6	84. 1
33	31.4	10, 2	93	88.4	88.7	53	145.5 146.5	47.3 47.6	13	202.6	65. 5 65. 8	73	259.6	84. 4 84. 7
34	32. 3 33. 3	10.5	94	89.4 90.4	29.0	54	146.5	47.6	14	203. 5 204. 5	66. 1 66. 4	74	200.0 261.5	84. 7 85. 0
35 36	24. 2	11.1	95 96	91.3	29.7	55 56	147.4	47.9 48.2	136	205.4	66.7	75 76	262. C	85. 2
37 38	35. 2 36. I	11.4	97 98	92.3	30.0	57 58	149.3	48. 5 48. 8	. 17 . 18	205.4 206.4	67. 1	77 78	262.4	85. 3 85. 6
38 39	36. 1	11.7	98 99	93.2	30. 3 30. 6	58	150, 3 151, 2	48.8	19	207. 3	67.4	78	264.4 265.3	85.9 -86.2
40	37. 1 38. 0	12. 4	1000	95. 1	30.9	59	152.2	49.4	20	200.3	67.7	72	266. 1	86.
41	39.0	12. 7	101	96, 1	31.2	161	153. I	49.8	221	210, 2	68. 3	281	267. 2 268. 2	86.8
42	39-9	13.0	02	97.0 98.0	31.5	62	154. 1	50. I	22	211.1	68. 3 68. 6	82	268, 2	87. 1
43 44	40. 9 41. 8	13. 3 13. 6	03 04	98.0	31. 8 32. I	63	155. o 156. o	50. 4 50. 7	23 24	212. I 213. 0	68. g 69. z	83 84	269. I 270. I	87.5
45	42.8	13.9	05	99.9	32.4	55	156.9	51.0	25 26	214.0	69.5	85 86	271.1	87. 5 87. 8 88. 1
45 46	43. 7	14. 2	05 06	100, 8	32.8		157. 9 158. 8	51.3		ا عند و	69. § 69. 8	86	272.0	88. ₄
47	44-7 45-7 46-6	14. 5 14. 8	% %	101.8	33. I 33. 4	67 68	158.8	51.6	27 28	215. 9 216. 8	70. I	87 88	273. 0 273. 9	88. 7 89. 0
49	46.6	15.1	9	103. 7	33-4	66	159.8	52.2	29	217.8	70.5	89	274. 0	89. 1
šó	47.6	15.5	10	104.6	34.0	70	161.7	52.5	30	217. 8 218. 7	71. 1	90	274. 9 275. 8	89. 3 89. 6
51	48.5	16. 1	111	105.6	34.3 34.6	171	162.6	52, 8	231	219. 7 220, 6	71.4	29 I	276.8	89.9
52 53	49. 5 .50. 4	16. 4	12	106. 5	34.9	72 73	163. 6 164. 5	53.2	32 33	220, 0	71. 7 72. 0	92 93	277.7 278.7	90.2
54	51.4	16. 7	14	107.5	35. 8	74	165.5	53. 5 53. 8	34	222.5	72. 3 72. 6	94	279. 6 280. 6	90.9
55 56	52. 3	17.0	16	109.4	35. 5	75 76	166.4	54. I	35 36	#23. S	72. 6	95 96	280. 6	91.2
50	53- 3 54- 2	17.3	.16	110.3	35. & 36. 2	70	167.4 168.3	54.4 54.7	30	224. 4 225. 4	72. 9 73. 2	90	281. 5 282. 5	91.5
57 58	55.2	17. 9	17	112.2	36.5	77 78	169. 3	55.0	37 38	226.4	73.5	97 98	287.4	91. 5 92. I
59 60	55. 2 56. 1	17.9 18.2	19	113. 2	36, 5 36, 8	79	170.2	55. 3 55. 6	39	227. 3 228. 3	73.9	99	284.4	92.4
60	57. 1	18. 5	20	114.1	37. 1	80	171. 2	55.6	40	228. 3	74-2	300	285. 3	92. 7
Dist.	Dop.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Diet.	Dep.	Lat.	Dist.	Dep.	Lat.
				ـــــا		·		[For	72 Degr	ces,				

[For 72 Degrees.

DIFFERENCE O	F LATITUDE	AND DEPARTURE	FOR 19°.
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Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Let.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	0.9	0.3	61	57. 7 58. 6	19.9	121	114.4	39.4	181	171.1	58.9	241	227. 9 228. 8	78. 5 78. 8
3	r. 9 2, 8	0. 7 1. 0	62 63	50.6	20, 2	82 23	115.4	39. 7 40. 0	82 83	172. I 173. 0	59. 3 59. 6	42 43	228. 8	70.0 79.1
4 1	3.8	1.3	64	60.5	20. § 20. 8	24	117. 2	40.4	1 84 I	174.0	59.9	44	230, 7	79.4
8	4.7	1.6	65 66	61. 5 62. 4	21. 3	25 26	118. 2	40.7	85 86	174.9	60, 2 60, 6	45 46	231. 7 232. 6	79. 8 80. 1
	5. 7 6. 6		67	63.3	21. 5 21. 8	27	119. I 120. I	41.0 41.3	87 88	175. 9 176. 8	60.9	40	232. 6 233. 5	80.4
7	7.6	2.3	67 68	64.3	22. I	27 28	121.0	41. 7	88	177. 8 178. 7	61.3	47 48	234.5	80.7
9	8. 5 9. 5	2.9 3.3	70	65. a 66. a	22. 5 22. 8	29 30	122.0 122.9	42.0 42.3	89 90	178. 7 179. 6	61.5	49 50	235.4 236.4	81. I 81. 4
11	10, 4	3.6	71	67. I 68. I	23. 1	131		42.6	191	180.6	62, 2	251	237. 3	81.7
12	11.3	3.9	72	68. ı	23. 4 23. 8	32	123. 9 124. 8	43.0	92	181. 5	62, 5 62, 8	52	237. 3 238. 3	82. o
13	12. 3 13. 2	4.8	73 74	69.0 70.0	23. 8 24. I	33 34	125. 8 126. 7	43. 3 43. 6	93	182. 5 183. 4	62. 8 63. 2	53	239. 2 240. 2	82. 4 82. 7
15	14.2	49	75 76	70.0	24.4	35	127. 6 128. 6	44.0	94 95 96	184.4	63.5	54 55 56	241.1	83.0
	15. I 16. I	5. 2	76	71.9 72.8	24.7	35 30	128, 6	44.8	96	185. 3 186. 3	63.8	56	242.1	83.3
17	17.0	5.5	77 78	73.8	25. I 25. 4	37 38	129. 5 130. 5	44.0	97 98	187. 2	64.1	57 58	243.0 243.9	83. 7 84. 0
19	17. 0 18. 0	5. 9 6. 2	79 80	74-7	25. 7 26. 0	39	131.4	45.3	99	187. 2 188. 2	64.5	59	244.0	84.0 84.3 84.6
20	18.9	6. 5 6. 8	80			40	132.4	45.6	200	189, 1	65. 1			84.6
21	19. g 20. 8	7.2	82	76.6 77.5	26. 4 26. 7	141	133. 3	45.9 46.2	20L 02	190.0	65. 4 65. 8 66. 1	261 62	246. 8	85. 0 85. 3 85. 6 86. 0
23	21.7	7.5	83 84	78. ()	27.0	43	134. 3 135. 2 136. 2	46.6	03	101.0	66. 1	62	247. 7 248. 7	85. 3 85. 6
24	22. 7 23. 6	7. § 7. 8 8. 1	84	79.4 80.4	27.3	44	136, 2	46. 9 47. 2	04	192. 9 193. 8	66. 4 66. 7	64	240.6	86. o 86. z
25 26	24.0	8. ş 8. 8	85 86	81. 2	27. 7 28. 0	44 45 46	137. 1 138. 0	47.5	05 06	194. 8	67. 1	65 66	250. 6 251. 5	86. 6
27 28	25. 5 26. 5	8, 8	87 88	82. 3	28. 3 28. 7	47 48	139.0	47. 9 48. 2	្ន	195. 7	67.4	67 68	252. 5	86. q
20	20.5	9.1	89	83. 2 84. 2	28. 7 29. 0	48	139.9	48. 5	9	196. 7	67. 7 68. 0	69	253. 4 254. 3	87. 3 87. 6
30	27. 4 28. 4	9. 4 9. 8	90	85. 1	29. 3	50	140.0	48. 8	ió	197. 6 198. 6	68. A	70	255.3	87.9
31	29. 3	10, 1	91	86. o 87. o	29.6	151	142.8	49. 2	211	199. 5	68. 7	271	256. 2	88. 2 88. 6
32 33	30. 3 31. 2	10.4	92 93	87. 0	30, 0	52 53	143. 7 144. 7	49. 5 49. 8	12 13	200. 4	69. 0 69. 3	72 73	257. 2 258. 1	88. a
34	32. 1	11.1	94	87. 9 88. 9 89. 8	30. 3 30. 6	54	144. 7 145. 6	50. I	14	202. 3	69.7	74	259. 1	89.2
35 36	33. I 34. 0	11.4	95 96	90.8	30.9	54 55 56	146.6	50. 5 50. 8	15	203. 3	70.0	75 76	260, 0 261, 0	89. 5 89. 9
37 38	35.0	12.0	97 98	91.7	31. 3 31. 6	57	147. 5 148. 4	51, 1	17	205. 2 206. I	70. 3 70. 6	77	261.0	89. 9 90. 8
38	35.9	12.4		92. 7 93. 6	31.9	57 58	149.4	51.4 51.8		200. 1	71.0	77 78	262. 9 263. 8	90. 5
39 40	35. 9 36. 9 37. 8	12.7	99	93.6 94.6	32. 2 32. 6	59 60	150. 3 151. 3	51.0	19 20	207. I 208. 0	71. 3 71. 6	72	204.7	90. B 91. #
41	38, 8	13.3	101	95. 5 96. 4	32. 9	161	152. 2	52.4	221	209.0	72. 0	28I	265. 7 266. 6	91.5
42 43	39. 7	13.7	02	96.4	33. 2	62	153. 2 154. 1	52. 7 53. 1	22 23	209.9	72. 3 72. 6	82 83	260.6 267.6	91. 8 92. 1
44	40. 7 41. 6	14.3	04	97.4 98.3	33. § 33. 9	63 64	155. 1	53.4	24	210. 9 211. 8	72. 9	83 84	268, 5	92. 5
45 46	42, 5	14. 7	95	99-3	34.2	65 66	156.0	53. 4 53. 7	25 26	212. 7	73. 3 73. 6	85 86	269. 5	
40	43. 5 44. 4	15.0	07	100, 2	34. 5 34. 8	67	157.0	54. 0 54. 4	27	213. 7 214. 6	73. 0 73. 9	87	270.4 271.4	93. I 93. 4
47 48	45. 4 46. 3	15. 3 15. 6 16. 0	oŝ	102, 1	35. 2	67 68	157. 9 158. 8	54-7	27 28	215.6	74. 2 74. 6	87 88	272.3	93.8
49 50	40. 3 47. 3	16. 3	10	103. I 104. 0	35. 5 35. 8	69	159. 8 160. 7	55. o 55. 3	29 30	216. 5 217. 5	74.6 74.9	89 90	273. 3 274. 2	94. I 94. 4
51	48. 2	16.6	111	105. 6	26. 1	171	161.7		231	218.4	75. 2	291	275.1	94-7
52	49. 2	16. 9	12	105. 9	36. 5 36. 8	72	162.6	55. 7 56. 0	32	219.4	75.5	92	276. 1	1 .70 I
53 54	50. I 51. I	17. 3 17. 6	13 14	100.8	36. 8 37. I	73 74	163.6 15:- 5	56. 3 56. 6	33 34	220. 3 221. 3	75. 5 75. 9 76. 2 76. 5	93 94	277.0 278.0	95. 4 95. 7 96. 0
55 56	52.0	17.9	15 16	107. 8	37·4 37·8	75	165. 5	57.0	35 36	222, 2	76. 5	95	278.0	96. 0
56	52.9	18, 2 18, 6	16	109. 7 110. 6	37. 8 38. 1	75	166.4	57. 3 57. 6	36	223. I 224. I	70.8	96	279. 9 280. 8	96.4 96.7
57 58	53. 9 54. 8	18. 9	18	111.6	28. ₄	77	167. 4 168. 3	1 cs. o	37 38	225. 0	77. 5	97 98	281.8	97. 0
59	55.8	19. 2	19	112.5	38. 7	79	160.2	58. 3 58. 6	39	226, 0	77. 8 78. 1	99	282. 7	97-3
00	56. 7	19. 5	20	113.5	39. 1	80	170, 2	58. 0	40	226.9	78, 1	300	283. 7	97. 7
Dist.	Dep.	f.at.	Dict.	Dep.	Lat	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.
												[For	71 Degre	es.

DIFFERENCE OF LATITUDE AND DEPARTURE FOR 20°.

Dist.	Lat.	Dep.	Diet.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat	Dep.	Dist.	1.41.	Dep.
,	0.9	0.3	61	57· 3 58. 3	20.9	121	113. 7 114. 6	41.4	181	170. 1	61.9	241	226, 5	82. 4 82. 5
3	1. 9 2. 8	0.7	62	58. 3	21.2	22	114.6	41. 7	82	171.0	62, 2	42	227. 4 228. 3	8a. 8
3	2.8	1.0	63	59. 2 60. I	21.5	23	115.6	42, I	83 84	172. 0	62.6	43	228. 3	83. t 83. 5 83. 8
	3.8	1.4	64	61.1	21.9 22.2	24	117.5	42. 4 42. 8	않	172.9 173.8	62.9	44	229. 3	83. 5
ş	4. 7 5. 6 6. 6	2, 1	65 66	64.0	22.6	25 26	118.4	43. I	85 86	174.8	63. ś 63. 6	45 46	230. 2 231, 2	
	6.6	2.4	67	63.0	32. Q		119.3	43.4	87	175.7	64.0	47	232, 1	84.5
Z	7.5	2. 7	67 68	63. 9 64. 8		27 28	120. 3	43. 4 43. 8	87 88	175. 7 176. 7	64.3	47	233.0	84.8
9	7· 5 8· 5	3. 1	69	64.8	23. 3 23. 6	29	121, 2	44. I	89	177.6	64.6	49	234.0	84.5 84.8 85.8
10	9.4	3-4	70	65.8	23.9	30	122, 2	44.5	90	178. 5	65. o	50	234.9	85.5
11	10. 3	3.8	71	66.7	24.3 24.6	131	123, 1	44.8	191	179. 5 180. 4	65. 3	251	235. 9 236. 8	85. 8 86. a
12	11.3	4.1	72	67. 7 68. 6	24.0	32	124.0	45. I	92	181.4	65. 7 66. 0	52 53	230. 8	86.5
13 14	13. 2	4.4	73 74	69.5	25.0 25.3	33 34	125.0	45. 5 45. 8 46. 2	93 94	182, 3	66.4	33	237. 7 238. 7	86.9
1 :: 1	14. I	5, 1	1 % 1	70.5	25. 7	35	120.0	46.2		183. 2	66. 7	54 55	238. 7 239. 6	87.2
15	15.0	5.5	75 76	71.4	25. 7 20. 0	35 36	125. 9 126. 9 127. 8	46.5	95 96	184, 2	67.0	50	240.6	87.6
17	16.0	5.50 5.60 2	77 78	72.4	26. 2	37 38	125.7	46.9	97 98	185. 1 186. I	67.4	57 58	241.5	87. 9 88. s
18	16.9	6, 2	78	73-3	26. 7	38	129. 7	47. 2		186, I	67. 7 68. 1	58	242. 4	88. s
19	17. 9	6. § 6. 8	123	74.3	27. 0	39	130.0	47-5	99	187. 0	68, I 68, 4	59 60	243. 4	
20				75. 2	27.4	40	131.6	47.9	200	187. 9	68.7	261	244-3	88.9
21	19. 7	7.2	81 82	76. 1	27. 7 28. 0	141	132. 5	48.2	201 02	188. 9 189. 8	69.1	63	245. 3 246. 2	89. 3 89. 6
22 23	20. 7 21. 6	7.5	8,	77. I 78. o	28, 4	42 43	133. 4 134. 4	48.9	03	190.8	66.	63	240. 2	90.0
4	22.6	7.9	83 84	78.9	28. 7	44	125. 1		O.	191.7	69. 4 69. 8	641	247. I 248. I	90.3
25 26	23.5	8.6	85 86	79. 9 80. 8	29. I		135. 3 136. 3	49. 3 49. 6	oş oğ	191. 7 192. 6	70. I	65 66	249.0	90.6
26	24.4	8.9	86	80.8	29.4	45 46	137. 2 138. 1	49.9	જ	193.6	70. 5 70. 8	66	250.0	91.0
27 28	25. 4 26. 3	9.2	87 88	81.8	29.8	47	138, 1	50, 3 50, 6	27	194. 5	70.8	67 68	250. 9 251. 8	91. 3
28	26. 3	9.6	88 89	82. 7 83. 6	30, I	48	139, 1	50.6	8	195. 5 196. 4	71. 1	69	251. 8 252. 8	91.7 92.0
29 30	27. 3 28. 2	9. 9 10. 3	90	84.6	30. I 30. 4 30. 8	49 50	140. 0 140. 0	51.0 51.3	100	197. 3	71. 5 71. 8	70	253. 7	92.3
31	29. I	10.6	91	85.5	31.1	151	141 0	51.6	211	198. 3	72, 2	271	254.7	92.7
32	30. 1	10.9	98	85. 5 86. 5	31. 5	52	141.9 142,8	52.0	13	199. 2	72. 5	72	254. 7 255. 6 256. 5	93.0
33 1	31.0	11.3	93	87. 4 88. 3	31. 5 31. 8	53	143.8	52. 3	13	900, 2	72. 9		256. 5	93.4
34	31.9	11.6	94	88. 3	32. I	53 54 55 56	144. 7	52. 7	14	201.1	73.2	73 74 75 76	257. 5 258. 4	93-7
35 36	32, 9 33, 8	12.0	95 96	89.3	32, § 32, 8	55	145. 7 146. 6	53. 0	15 16	202. 0	73-5	75	258.4	94. 1
30		12. 3	90	90. 2	32, 8	50	140.0	53-4	10	203.0	73-9	70	259. 4 260. 3	94-4 94-7
37 38	34. 8	13.0	97 98	91. 2 92. 1	33. 2 33. 5	57 58	147. 5 148. 5	53- 7 54- 0	17	203.9	74-2 74-6	77 78 79	261. 8	95. 1
39	35. 7 36. 6	13.3	99	93.0	33.9	100	149.4	44.4	10	204. 9	74.9	70	262, 2	95.4
40	37.6	13.7	100	94.0	34. 2	59 60	150.4	54-7	20	206. 7	75. 2		263. 1	95. 4 95. 8
41	38. 5	14.0	101	94.9	34- 5	161	151.3	55. 1	221	207. 7 208. 6	75.6	281	264. 1	96. I
42	39.5	14.4	03	95. 8 96. 8	34.9	63	152. 2	55. I 55. 4	22	208.6	75.9 76.3 76.6	82	265. 0	96. ¢ 96. 8
43	40.4	14.7	03	96, 8	35. 8	63	153. 2	55. 7 56. 1	23	209, 6	70.3	83	265. 9	90.8
44	41.3 42.3	15.0	04	97. 7 98. 7	35.6	64	154.1 155.0 150.0	50.1	24	210. 5	77.0	358	265. 9 266. 9 267. 8 268. 8	97. I 97. 5
45 46	43.2	12.7	엻	98. 7 99. 6	33. 3	65 66	156.0	56. 4 56. 8	25 26	212.4	77. 2	86	268. 8	97. 5 97. 8
47	44.2	15.4 15.7 16.1	07	100, 5	35. 9 36. 3 36. 6	67 68	110.0	57. 1	27 28	213. 3	77.3 77.6 78.0	87 88	269. 7	. A .
47	45. I 46. 0	16. 4 16. 8	97 98	101.5	26. o. 1		157. 9 158. 8	57-5		214.2	78.0		269. 7 270. 6	98. 5 98. 8
49	46.0		9	102.4	37. 3 37. 6	69	158.8	57. 5 57. 8 58. 1	29	215. 2 216. 1	78, 1	89	271.6	98.8
50	47.0	17.1	10	103. 4	37. 6	70	159.7	58. I	_30	210, 1	78. 7	90	272.5	99. 3
51	47. 9 48. 9 49. 8	17.4 17.8 18.1	111	104. 3	38. o 38. 3 38. 6	171	160, 7 161, 6	58. 5 58. 8	231	217. 1 218. 0	79.0	291	273. 5	99-5 99-9
52	49.8	17.0	13	105.2	30. 3	72 73	162, 6	59. 2	32 33	218.0	79-3 79-7 80.0	92 93	274- 4 275- 3	100 3
[21	50.7	18. <	14	107. 1	39.0	74	163.5	59.5	34		86.6	94	270.3	100.6
53 54 55 56	51.7	18. 5 18. 8	15	107. I 108. I	39- 3	75 76	164.4	59.9	35	219. 9 220. 8	80,4	95 96	277. 2	100.9
56	52.6	19. 2	16	109.0	39. 7	70	165. A	60.2	35 36	221.8	80.7	96	278. 1	101. 2
57 58	53.6	19. 5 19. 8	-17	109.9	40.0	77 78	100, 3	60. 5	37 38	322. 7	81. 1	97 98	279. I 280. 0	101.6
50	54- 5	19.8	18	110.9	¥0.4 40.7	70	167. 3 168. 2	60. 9 61. 2	35	223. 6 224. 6	81.4 81.7	98 99	280. 0 281. 0	101.9
59	55. 4 56. 4	20, 2	20	111.8	40. 7 41. 0	79	169.1	61.6	39 40	224. 0	82. 1	300	281.0	102. 3 102. 6
لتبا	3+	٠,			1			1		3.3		ات.	y	
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.
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DIFFERENCE OF LATITUDE AND DEPARTURE FOR 21°.

Dist.	Lat.	Dep.	Dist.	Let.	Dep.	Dist.	Lat.	Dep	Dist.	Lat	Dep.	Dist.	Lat.	Dep.
-	0.9	0.4	61	56.9	249	121	113.0	43 4	181	169.0	64.9	241	225. 0	86, 4
2	1. 9 2. 8	0.7	62	57.8	22, 2	22	113.9 114.8	43.7	82	169.9 170.8	65. 2	42	225. 9	86. 7
3	3.7	1.1	63 64	58.8	22. 6 22. 9	23 24	114.8	44.1	83 84	170.8	65. 6 65. 9	43	220. 9	87. 1
- (1	4.7	1.4 1.8	6¢	59.7 60.7	23.3	2	116.7	44-4 44-8	85 86	172. 7	66, 3	44	227. 8 223. 7	87. 4 87. 8
8	4. 7 5. 6 6. 5	2.2	66	61.6	23. 7	25 20	117.6	45. 2	86	173.6	66. 7	45 46	229. 7 230. 6	28.9
7	6.5	2.5	67 68	62, 5	24.0	27 28	118,6	45- 5	87 88	174.6	67. 0	47 48	230, 6	88, 5
9	7: 5 8. 4	2.9 3.2	60	63.5	24. 4 24. 7	20	119.5	45. 9 46. 2	89	175. 5 176. 4	67.4	49	231. 5 232. 5	88, 9 89, 2
10	9.3	3.6	70	64.4	25. 1	30	121.4	46.6	90	177.4	67. 7 68. 1	50	233. 4	89.6
11	10. 3	3.9	71	66, 2		131	122. 3	46.9	191	178. 3	68. 4 68, 8	251	234-3	90.0
12	11. B	4.3	72	67. 2 68. 2	25.4 25.8 26.2	32	123. 2	47-3	92	179. 2	68, 8	52	235. 3	90.3
13 14	12, I 13, I	4.7 5.0	73 74	69.1	20.2	33 34	124. 2 125. I	47. 7 48. 0	93 94	180. 2 181, 1	69. s 69. 5	53 54	236. 2 237. I	90. 7
15	14.0	8.4	75	70.0	s6.0	35	120.0	48.4	8	182.0	69.9	22	238. 1	91.4
	14.9	5.7	75 76	71.0	27. 2	35 36	127. 0	48. 7	95 96	182.0	70. 2	55 56	239. 0	91. 7
:7	15. 9	6.1	77	71.9 72.8	27. 6 28. 0	37 38	127. 9 128. 8	49. I	97 98	183. 9 184. 8	70.6	57 58	239.9	92. I
10	17.7	6.5 6.8	78	73.8	28. 3	38 39	120. 8	49.5	99	185. 8	71.0	50	240. 9 241. 8	92.5
30	18.7	7. 2	20	74-7	28. 7	40	130. 7	49. 5 49. 8 50. 2	200	186. 7	71.7	52	242. 7	93. 2
21	19.6		81	75.6 76.6	29.0	141	131.6	50. 5	201	187.6	72.0	261	243- 7	93-5
22	20.5	7.5 7.9 8.2	82	76.6	29.4	42	132.6	50.9	02	188.6	72.4	62	244.6	93-9
23 24	21. 5 22. 4	8.6	83 84 85 86	77:5 78:4	29. 7 30. I	43 44	133. 5 134. 4	51.2 51.6	03 04	189. 5 190. 5	72. 7 73. 1	63 64	245. 5 246. 5	94. 3 94. 6
25	23.3	9.0	85	79.4	30. 5		135.4	52.0	05	191.4	72.5	66	247.4	05.0
	24.3	9.3	86	79.4 80.3	30. § 30. 8	45	136.3	52. 3	05 06	192. 3	73. § 73. 8	65 66	247. 4 248. 3	95.3
27	25. 2 26. I	9.7	87 88	81.2	31. 2	47 48	137. 2	52. 7	3	193. 3	74. 2	67 68	249. 3	95. 3 95. 7 96. 0
20	20. I	10.0	80 80	82. 2 83. 1	31.5	45	130. 2	53.0	9	194. 2 195. I	74·5 74·9	60	250, 2 251, 1	90.0
30	27. I 28. 0	10.4	90	84.0	32. 3	50	140.0	53. 4 53. 8	10	196. 1	75.3	70	252. 1	96. 4 96. 8
31	28, 9	11. I	.91	85. o	32. 6	151	141.0	54. 1	211	197. 0	75.6 76.0	271	253.0	97. 1
32	29.9 30.8	11.5	92	85. 9 86. 8	33.0	52	141.9	54. § 54. 8	12	197. 9	76.0	72	253.9	97. § 97. 8 98. 2
33 34	30. 0 31. 7	12.2	93 94	87.8	33- 3	53 54	143.8	55. 8	13 14	198, 9 199, 8	76. 3 76. 7	73 74	254. 9 255. 8	97.0
33	32. 7	12, 5	~	88. 7	33.7 34.0	**	144. 7	\$ C. C	1 3	200.7	77.0	73	250. 7	98,6
35 36	32. 7 33. 6	12.9	95 96	88. 7 89. 6	34. 4 34. 8	5\$ 56	144. 7 145. 6	55.9	15 16	201.7	77-4	75 76	257. 7 258. 6	98.9
37 38	34-5	13.3 13.6	97 98	90.6	34.8	57 58	140.0	55. 9 56. 3 56. 6	17	202.6	77. 4 77. 8 78. 1	77	258, 6	99. 3 99. 6
39	35. 5 36. 4	14.0	99	91. 5 92. 4	35. I	50	147. 5 148. 4	57.0	10	203. 5 204. 5	78. 5	70	259. 5 260. 5	100.0
40	37- 3	14.3	100	93-4	35. 5 35. 8	\$9 60	149.4	57-3	20	205.4	78. 5 78. 8	79	261.4	100. 3
41	38+3	14.7	101	94-3	26.2	161	150. 3	57. 7 58. 1	221	206. 3	79.2	281	262. 3	100. 7
42	39. 2	15. 1	02	95. 2 96. 2	36, 6	68	151.2	58. I	22	207. 3	79.6	82	263.3	101.1
43	40. I 41. I	15.4 15.8	03 04	90.2	36.9	63 64	152, 2 153, 1	58.4 58.8	23 24	205. 2 209. I	79.9 80.3 80.6	83 84	264. 2 265. I	101.4
45	42.0	16.1	8.8.5	97. I 98. 0	37. 3 37. 6	8.25	154.0	50. I	25 26	210. I	80.6	85	266. I	102. 1
46	42.9	16. 5 16. 8	જ	99.0	18.0 i	66	155.0	59. 5 59. 8 60. 2	26	211.0	81. o	88	267. 0	102. 5
47	43. 9 44. 8	16.8	3	99.9	38. 3 38. 7	67 68	155. 9 156. 8	\$9.8	27	211.9	81. 3 81. 7	87 88	267. 9 268. 9	102. 9
49	45.7	17.6	8	101.8	30.7	69	157.8	60, 6	20	212. 0 213. 8	82, 1	80	269. 8	103. 2
50	45.7 45.7	17.9	10	102. 7	39.4	70	157. 8 158. 7	60.9	30	214.7	82, 4	90	270. 7	103. 9
51	47.6 48.5	18. 3 18. 6	111,	103.6	39. 8	171	159.6	61.3 61.6	231	215. 7	82, 8	29I	271. 7	104. 3 104. 6
52	48.5	18.6	12	104.6	40, 1	72	160, 6	61.6	32	216.6	83. 1	92	272.6	104.6
53 54	49. 5 50. 4	19.4	13 14	105.5	40.5	73 74	162.4	62.4	33 34	217.5	83. 5 83. 9	93 94	273. 5 274. 5	105. 0
55	51.3	19.7	15	107. 4	41.2	75	163.4	62. 7	33	219.4	84.2	95	275. 4	105. 7
55 56 57 58	52. 3	20. I	16	108. 3	41.6	76	164.3	62.1	35 36	220, 3	84.6	اةوا	275.4 276.3	106. 1
-5 <u>7</u>	53. 2 54. I	20, 4 20, 8	17 18	109. 2	41.9	77	165. a 166, a	63.4 63.8	37 38	221. 3	84.9	98 98	277.3 278.2	106.4
50	55. 1	21. I	19	111.1	42. 3 42. 6	72	167. 1	64.1	39	223. I	85. 3 85. 6 86. 0	99	279. I	107. 2
60	55. 1 56. 0	21. 5	90	112,0	43.0	86	168. 0	64.5	40	224. I	86. 0	300	279. I 280. I	107. 5
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Let.	Dist.	Dop.	Lat.	Dist.	Dep.	Lat.
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DIFFERENCE OF LATITUDE AND DEPARTURE FOR 22°.

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Cist.	Lat.	Dep.	Dist.	Les.	Dep.	Dist.	Lat.	Dop
3	0.9	0.4	61	56.6	22.9	121	112. 2	45.3	181 82	167. 8 168. 7	67. 8 68. 2	241	223.5	90. 3 90. 7
3	1. 9 2. 8	1.1	62 63	57· 5 58. 4	23. 2 23. 6	22 23	114.0	45.7	82	169. 7	68.6	42 43	224. 4 225. 3	91.0
4	3-7	1.5	64	59. 3 60. 3	24.0	24	115.0	46. 5 46. 8	84	170.6	68.9	44	225. 3 220. 2	91.4 91.8
8	3. 7 4.6	1.9	55	61.2	24.3	25	115.9	46.8	85 86	171.5	69. 3	45	227. 2 228. 1	91.8
	5.6 6.5	2.2	800	63. 1	24. 7 25. I	27	117.8	47.6	87	172. 5 173. 4	69. 7 70. I	1 47	\$20, I	92.5
3	7.4	3.0	67	62.0	25. 5	27 28	117.8 118.7 119.6	47.9 48.3	87 88	174-3	70.4	47	229.9	92.9
9	£ 4	3-4	69	64.0	25. 5 25. 8 20. 2	29	119.6	48.3 48.7	89	175. 2 176. 2	70.8	49	230. 0 231. 8	93-3
10	9.3	3.7	70	64.9	26.6	131	120. 5	49.1	191	177.1	71.2	50 251	232. 7	93-7
12	11.1	41	71 72	65.8 66.8	27.0	32	122. 4	49.4	29.	178.0	71.9	52	233. 7 234. 6	94.4 94.8
13	12, 1	40	73	67. 7	27. 3	33	123. 3	49. 4 49. 8	93	178.9	72. 3	53	234.6	94.8
14	13.0	5,2	74	69.5	27.7 28.1	34	124, 2 125, 2	50, 2 50, 6	24	179. 9	72. 7 73. 0	54	235. 5 236. 4	95. 2 95. 5
15	13. 9 14. 8	5, 2 5, 6 6, 0	75	70.5	28, 5	35 36	126. 1	50.9	25	181.7	73-4	55 56	237.4	95.9
17	15.8	6.4	77	71.4	28, 5 28, 8	37 38	127. 0	51.3	97 98	182. 7	73- 4 73- 8	57 58	238. 3	95. 9 95. 3 96. 6
18	10. 7	6. 7 7. I		72.3 73.2	29. 2 29. 6	35	128.9	\$1.7 52.1	90	183. 6 184. 5	74.2 74.5	1 50	239. 2 240. I	97.0
20	15.8 16.7 17.6 18.5	7.5	79	74.2	30.0	40	129. 8	52.4	200	185.4	74.9	22	241. 1	97-4
21	19.5	7.9	81	75. I 76. o	30. 3	141	130.7	52, 8	201	150.4	75-3	261	242. 0	97. 8 98. 1
23 23	20.4	8.6	82 83	76.0 77.0	30. 7 31. I	42 43	131. 7 132. 6	53. 2 53. 6	03 03	187. 3 188. 2	75.7 76.0	62 63	242. 9 243. 8	98.1 98.5
24	22. 3	9.0	84	77.9	31.5	44	133. 5	53.9	ايةها	189, 1	76.4	64	844.8	98.9
25 26	23. 2	9.4	85 86	77. 9 78. 8	31. 5 31. 8	45 46	134-4	54-3	558.53	190, 1	76.8	65	245. 7 246. 6	99. 3 99. 6
	24.1	9.7 10.1	86 87	79.7 80.7	32, 2 32, 6	40	135. 4 136. 3	54- 7 55. I	8,	191.0	77. 8 77. 5	67	240, 0	100,0
27 28	25.0 26.0	10.5	88	81.6	33.0	47	137. 8	85.4		192. 9 193. 8	77.9 78.3	67 68	247.6 248.5	100. 4
29	26. 9 27. 8	10.9	89	82. 5	33- 3	49		55. 8 56. 2	99		78. 3 78. 7	69	249.4	100, 8 101, 1
30	28.7	11. 6	90	83.4 84.4	33-7	151	139.1	56,6	211	194. 7	79.0	70 371	250. 3 251. 3	101.5
32		12.0	92	85.3 86.2	34.5 34.8	52	140.0	56.9	13	196.6	79.4	72	252. 2	101.9
33	29 7 30. 6	12.4	93	86.2	34.8	53	141.0 142.8	57.3	13	197.5	79-4 79-8 80, 2	73	253. 1	102. 3
34	31. 5 32. 5	12. 7 13. I	94	87. 2 88, 1	35.2	54	142 7	<u>\$2.7</u>	14	199.3	80, 5	74	254. 0 255. 0	103. 0
35 36	33-4	13.5	95 96	89.0	35.6 30.0	55 56	143. 7 144. 6	(8. ₄	15	200, 3	80.9	75 78	255. 9 256. 8	103.4
37 38	34-3	13.9	97	89.9	36. 3 36. 7	57 58	145. 6 146. 5	58.8	17	201. 2 202, I	81.3 81.7	77 78	250.8	103. 8 104. I
39	35. 2 36. 2	14.6	99	90.9 91.8	37. 1	50	147.4	59. 2 59. 6	19	203. 1	82.0	250	257. 8 258. 7 259. 6	104.5
40	37. 1	15.0	100	92.7	37.5			59.9	80	204. 0	82.4		259.6	104.9
41	38, o 38, g	15.4	101	93. 6 94. 6	37. 8 38. 2	161 62	149. 3 150. 2	60. 3	221 82	204. 9 205. 8 200. 8	82, 8 83, 2	281 82	260, 5 261, 5	105. 3 105. 6 106. 0
42 43	30. 9	15. 7	03	94.6	38.6	63	151.1	61, i	23	200.8	83.5	82	262, 4	100.0
44	39. 9 40. 8	16. 5	O.	95. 5 96. 4	39.0	64	152. 1	61.4	24	207. 7	83.9	84	263.3	106. 4 106. 8
45	41.7	16.9	95	97.4 98.3	39. 3 39. 7	65	153.0	62. 2	25 26	205, 0	84.3 84.7	85 86	264. 2 265. 2	106, 8
47	42. 7 43. 6	17.6	07	99.2	40.1	67	153. 9 154. 8	62.6	27	210.5	85.0	87 88	265, 2 266, 1	107. 5
	44.5	18.0	08 00	100, 1	40.5	68 60	155. 8 156. 7	62.9		211.4	85.4	88 89	267. 0 268. 0	107.9
49 50	45. 4 40. 4	18.7	1 29	102.0	41.2	70	157.6	63. 3 63. 7	30 30	212. 3 213. 3	85. 4 85. 8 86. 2	89	268. q	107. 9 108. 3 108. 6
51	47:3 48:2	19. I	111	103. 9	41,6	171	158.5	64. 1	231	214. 2	86. 5	291	269, 8	100.0
52	48, 2	19.5	12	103.8	42.0	72	159.5	64.4	32	215. I 216. 0	86.9	92 93	270. 7	109. 4 109. 8
53 54	49. I 50. I	19.9	13	104.8	42.7	73 74	161. 3	65. 2	33 34	217.0	87. 3 87. 7	93	271. 7	110, I
55 56	51.0	20,6	15 16	106.6	43. 1	75	162, 3	65.6	35	217. 9 218. 8	87. 7 88. 0	95 96	273.5	110.5
56	51. 9 52. 8	21. 0 21. 4		107.6	43. § 43. 8	76	163. 2 164. I	65.9	36	218.8	88. 4 88. 8	90	274.4	110.9
57 58	(2.8	21.7	17	109.4	44.2	77	165.0	66. 7	37 38	220. 7 221. 6	89, 2	97 98	275.4 276.3	111.3
59	54. 7 55. 6	22, I	19	110, 3	44.6	Z	166, 0	67. 1	39		89.5	99	277.2 278.2	112.0
_∞	55.6	22. 5	20	111.3	45.0	_ 80	166, 9	67.4	40	222, 5	89.9	300	275, 2	112. 4
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Let.	Dist.	Dep.	1
												[Fo	or 68 Deg	rees.

DIFFERENCE OF LATITUDE AND DEPARTURE FOR 23°.

Dist.	Lat.	Dep.	Dhet.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
-	0.9	0.4	61	56. 2	23.8	121	111.4	47.3	181	166, 6	70.7	241	221.8	94.8
2	1.8		62	57. 1 58. 0	24.2 24.6	22	113.3	47.7	82 83	167. 5 168. 5	71. I 71. S	42 43	222. 8	94.6 94.9
3 4	2.8	1.2 1.6	63	58.0	25.0	23	114.1	48.5	84	169.4	71.9	44	223. 7 224. 6	05.2
5	3-7 4-6	2.0	65	58, 9 50, 8	25. 4 25. 8 26. 2	25	115. 1	48. 5 48. 8	85 86	170. 3	72. 3	45 46	225. 5 226. 4	95.7 96.1
	5.5 6.4	2. 3	66	60.8	25.8	96 97	116.0	49. 2 49. 6	87	171.2	72. 7 73. I	40	227. 4	96.5
3	7.4	8.7 3.1	68	61. 7 62, 6	26, 6	27 28	116. 9 117. 8 118. 7	50.0	87 88	173. 1	73.5	47 48	227. 4 228. 3	96.5 96.9
9	8.3	3.5	69	63.5	27.0	29	118.7	50. 4 50. 8	89	174.0	73.8	49	229. 2	97-3 97-7
10	9, 2	3.9	70	64.4	27.4	30	119.7	51.2	90 191	174-9 175-8	74. 2	50 251	230.1	08. 1
11	10.1	43	71 72	65. 4 66. 3	27. 7 28. I	131	121.5	51.6	92	176.7	75.0	52	232.0	98.5 98.9
13	12.0	5.1	73	67. 2 68, 1	28, 5	33	122. 4	52.0	93	177.7 178.6	75.4 75.8 70.2	(3	232, 9 233. 8	98.9 99.2
14	12. 9 13. 8	5. 5 5. 9 6. 3 6. 6	74	68,1	28, 9 29, 3	34	123.3	52.4 52.7	94	170.0	75.3	54 55 56	233.0	99.2
15 16	13.0	8.3	75 70	70.0	29.7	35 36	125. 2	53. 1	95 96	179.5 180.4	76.6	36	234. 7 235. 6 236. 6	99.6 100.0
17 18	14. 7 15. 6	6.6	77	70.9 71.8	30.1	37 38	126, 1	53-5	97	181.3	77-0	57 58	236.6	100. 4 100. 8
19	10.6	7.0	78	71.8	30.5	38	127.0	53.9 54.3	98 99	182, 3 183, 2	77.4 77.8 78.1	1 %	237. 5 238. 4	101.2
20	17. 5 18. 4	7. 4 7. 8	79	72. 7 73. 6	31.3	40	128.9	54.7	200	184. I	78. 1	59 60	239-3	101.6
21	19. 3	8. 2	81	74.6	31.6	141	129. 8	55. I	201	186.0	78. 5	261 62	240. 3	102.0
22	20,3	8.6	84 81	75. 5 76. 4	32,0	42	130. 7 131. 6	55.5	02 03	185.9	78.9 79.3	63	241.3 242.1	102. 4 102. 8
23 24	21. 2 22. 1	9.0	1 22	77.3	32. 4 32. 8	43 44	132.6	55.9 56.3	04	185. 9 186. 9 187. 8 188. 7	79. 7 80. 1	64	243.0	103.2
95 26	23.0	9.4 9.8	84 85 86	77.3 78.2	33.2	45	133.5	56.7	엻	188. 7	80. t	65	243.9	103.5
26	23.9	10.2	86	79. 2 80. 1	33.6 34.0	40	134.4	57.0	007	189. 6 190. 5	80. 5 80. 9	67	244. 9 245. 8	103.9
27 28	25.8	10.5	87 88	81.0	34-4 34-8	47	135. 3 136. 2	57.4 57.8 58.2	27	191.5	81.3	67 68	246. 7 247. 6	104-7
29	24.9 25.8 20.7 27.6	11.3	89	81.9 82.8	34.8	49	137. 2	58. 2 58. 6	09	192. 4	81. 7 82. 1	69	247.6 248.5	105. 1
30	27.6	11.7	90	82.8	35.2	50	136.1	59.0	211	193.3		70 271	249.5	
31 32	28. 5 29. 5	12, 1 12, 5	91 92	84.7	35.6	151 52	139.0	59.4	12	195. I 196. I	82. 4 82. 8	72	250.4	105. 9 106. 3
33	30.4	12.9	93	84.7 85.6 86.5	35.9 36.3	53	139. 9 140. 8	59.4 59.8	13	196. 1	83.2	73	251.3	106. 7 107. I
34	31. 3	13.3	94	86.5	36. 7 37. 1	54	141.8	60. 2	14	197.0	83.6 84.0	74	252. 2 253. 1	107. 5
35 36	32. g 33. l	13.7 14.1	95	87.4 88.4	37. 5	55 56	142. 7 143. 6	61.0	15 16	197. 9	84.4 84.8	75	254.1	107. 5
37 38	34. I	14.5	97 98	89-3	37-9	57 58	144-5	61.3	17	199. 7 200. 7	84.8	77	255.0	108.2
38 39	15.0	14. 8 15. 2	98 99	90, 2 91, 1	38. 3 38. 7	58	145.4	61.7	10	200. 7 201. 6	8¢. 6	72	255. 9 256. 8	109.0
40	35. 9 36. 8	15.6	100	92. 1	39.1	59	147.3	62.5	20	202. 5	86. o		257.7	109.4
41	37-7	16.0	101	93.0	39-5	161	148. 2	62.9	221	203.4	86. 4 86. 7	28t 82	258. 7 259. 6 260. 5	109. 8 110. 2
42	37· 7 38. 7 39. 6	16. 4 16. 8	02	93. 9 94. 8	39.9	62 63	149. 1 150. 0	63. 3 63. 7	22 23	204. 4	87. I	83	200.5	110,6
43	40.5	17. 2	03 04	95.7	40.6	64	151.0	64.1	24	205. 3 206. 2	87. 5	82	1 201.4	111.0
45 46	41.4	17.6	05 06	96.7	41.0	65	151.9 152.8	64.5	25	207. 1 208. 0	87. 9 88. 3	85 86	262. 3 263. 3	111.4
46	42. 3	18.0	06	95. 7 96. 7 97. 6 98. 5	41. 4 41. 8	65	152.8	64.9	27	200,0	88.7	87	264.2	112.1
47 48	43-3 44-2	18, 4 18, 8	97 98	99-4	42. 2	67	153. 7 154. 6	65. 3 65. 6 66. 0	28	209. 9 210. 8	8g, i	88	265. 1 266. 0	112.5
49	45. I 46.0	19. I	99	100, 3	42,6	69	155. 6 156. 5	66.4	29 30	210.8	89.5 89.9	89 90	266.0	112.9
50 51	46.9	19.5	111	101. 3 102, 2	43.0	171	157.4	66. 8	231	212.6		291	267. 9 268. 8	113.7
52	47.9	20, 3	112	103. 1	43. 4 43. 8	72	158.3	67. 2	32	213.6	90. 3 90. 6	92	268.8	114.1
52	47. 9 48. 8	20, 7	13	104.0	44.2	73	159.2	67.6 68.0	33	214.5	91.0	93 94	269. 7 270. 6	114.5 114.9
54	49. 7 50. 6	21. 1	14	104.9	44.5 44.9	74 75	161. 1		34 35	216.3	91.4 91.8	3	271.5	115.3
55 56	51.5	21.9	15	105. 9	45. 3	75 76	162.0	68.8	35 36	217. 3	92.2	96	272.5	115.7
57 58	52.5	22. 3	.17 .18	107. 7	45. 7 46. I	77	162. 9 163. 8	69. 2 69. 6	37 38	218.2 210.1	92. 6 93. 0	37	273.4 274.3	116.4
%	53-4 54-3	22. 7 23. I	19	109.5	46.5	ź	164.8	69.9	39	219. l 220. 0	93. 4 93. 8	99	275.2 270.2	
52	55.2	23.4	aó i	110.5	46. 9	86	165. 7	70.3	40	\$20.9	93.8	300	270.2	117.2
Diet.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Diet.	Dep.	Lat.	Dist.	Dep.	Lat.
												[F	or 67 Deg	Toos.

DIFFERENCE OF LATITUDE AND DEPARTURE FOR 24°.

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Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat	Dep.	Dist.	Lat.	Dep
1	a. 9 1. 8	0.4 0.8	61	55. 7 56. 6	24.8	121	110. 5	49. 2	181	165. 4 166. 3	73.6	241	220. 3	98. o
*			02	56.6	25. 2	22	111.5	49.6	82	166. 3	74-0	42	221. 1	98.4 98.8
3	2. 7 3. 7	1. 2 1. 6	63	57. 6 58. 5	25. 6 26. 0	23 24	112.4	50.0	83 84	167. 2 168. 1	74.4	43 44	222. O	95.8
5	4.6	2.0	65 66	59.4	26.4 26.8	25	114.2	50. 4 50. 8	85	160.0	75. 2	45	223.8	99.7
6	5.5	2. 4 2. 8	66	59.4 60.3	26.8	26	115.1	51. 3	86	169. 9 170. 8	75. 7 96. 1	45 46	224. 7 225. 6	100. I
7	6.4		67 68	61. 2 62. 1	27.3	27 28	116.0	51. 7	87 88	170.8	96. I	47	225. 6 226. 6	100. 5
اۋا	7:3	3-3 3-7	69	63.0	27. 7 28. 1	20 29	110.9	52. i 52. 5	80	171. 7	76. 5 76. 9	49	220. 0	100. 9
10	9.1	41	70	63.9	28.5	30	116. 9 117. 8 118. 8	52.9	90	173.6	77.3	50	228.4	101. 7
11	10.0	4.5	71	64.9	28.9	131	119. 7 120. 6	53-3	191	174.5	77:7	251	229. 3	102. I
12	11.0	49	72	64.9 65.8 66.7	ag. 3	32	120.6	53-7	92	175.4 176.3	78. 1	52	230. 2	102. 5
13	11. 9 12. 8	5.3	73 74	66. 7 67. 6 68. 5	39. 7 30. I	33 34	121.5 122.4	54.1	93 94	170.3	78. 5 78. 9	53	231. I 232. 0	102. 9
13	12.7	5.7	12	68. 4	30.5	35	123. 3	54-5 54-9	8	178.1	79-3	54	233.0	103. 7
15 16	13. 7 14. 6	6.5	75 76	69.4	30.9	35 36	124. 2	55. 2	95 96	179. 1 180. 0	79. 7 80. 1	55 56	233. 9 234. 8	104.1
17	15.5 16.4	6.9 7.3	77 78	70.3	31. 3	37 38	125. 2 126. 1	55. 7 56. 1	97	180.0	80. I	57 58	234.8	104.5
18	10.4	7.3	70	71.3	31. 7 32. I	39	120. 1	56. S	98 99	180. 9 181. 8	8a. 5 8a. 9	58	235. 7 236. 6	104.9
30	17. 4 18. 3	7.7	72	73.1	32.5	40	127.9	56.9	200	182. 7	81.3	59	237-5	105. 8
31	19. 2	8. 5	81	74.0	12. 0	141	128. 8		201	182.6	81.8	261	238.4	105. 3 105. 8 106. 2
22	20. I	8.9	82	74-9 75-8 70-7	33. 4 33. 8	43	129. 7 130. 6	57· 3 57· 8 58· 2	O2	184. 5 185. 4 186. 4	82. 2	62	230.3	106.6
23 24	21.0	9.4	83	75.8	33. 8	43	130. 0	58. 2 58. 6	03	185.4	82, 6	63	240.3	107.0
2	21. 9 22. 8	10.2	84 85 86	70.7	34. 8 34. 6	44	131.0	50.0	04	187. 2	83. o 83. 4	64 65	241. 2 242. 1	107.4
25 26	22.8	10.6	86	77.7	35.0	45	133-4	59-4	o5	187. 3 188. 2	83.8	65 66	243.0	108.2
27 28	24.7	11.0	87 88	79. 5 80. 4	35.4	47	134.3	59. 8 60. 2	°7	189. 1	84.2	67 68	243. 9 244. 8	108.6
28	24. 7 25. 6 26. 5	11.4 11.8	88	80. 4 81. 3	35. 4 35. 8 36. 2	45	135. 2 136. 1	60.6	08	190. 0 190. 0	84. 6 85. 0	69	244. 8 245. 7	109.0
30	27.4	12. 2	90	82.2	36.6	50	137.0	61.0	10	191.8	85.4	70	240.7	109. 4
31	28. 3	12.6	91	83. 1	27. 6	151	137. 0	61.4	211	192, 8	85.8	271	247.6	110. 2
38	29. 2	13.0	92	84.0	37. 4 37. 8 38. 2	52	137. 9 138. 9 139. 8	61.8	13	193. 7 194. 6	86.2	72	248.5	110.6
33	30. I 31. I	13. 4 13. 8	93	85.0	37.8	53	139. 8	62. 2 62. 6	13	194.6	86. 6 87. 0	73	249. 4	111.0 111.4
34 35	32.0	14.2	왔	85. 9 86. 8	38.6	54	140. 7 141. 6	63.0	14	195. 5 196. 4	87.4	74 75	250. 3 251. 2	111.0
35 36	32. 9	14.6	95 96	87. 7 88. 6	39.0	55 56	142. 5	63. 5	. 15 16	197. 3 198. 2	87.0	75 76	252. I	112.3
37 38	32. 9 33. 8	15.0	97 98	88.6	39.5	57 58	143. 4	63.9	17	198. 2	88. 1	77 78	253. I	112.7
38	34 7	15.5	98	89. 5 90. 4	39.9 40.3	58	144-3	64.3	18	199. 2 200. I	88. 7 80. 1	78	254.0	113.1
40	34- 7 35- 6 36- 5	15.9	180	91.4	40.7	59	145. 3 146. 2	65. i	20	201.0	89.5	7 9	254. 9 255. 8	113.9
41		16. 7	101	92. 3	41. I	161	147. 1	65. 5	221	201.9	89.9	281	256. 7	114-3
42	37· 5 38. 4	17. 1	02	93. 2	41.5	62	1 148.0	65. 9 66. 3	22	202. 8	90.3	82	257.6	114.7
43	39. 3 40. 2	17.5	03	94. I 95. 0	41.9	63	148. 9 149. 8	66. 7	23 24	203. 7 204. 6	90. 7 91. I	83	258. 5 259. 4	115. I 115. 5
44	41. I	17.9 18.3	04	95.0	42.3 42.7	66	150. 7	67. 1	24	205. 5	91.5	84 85 86	200.4	116.0
45 46	42.0	18. 7	05	95. 9 96. 8	43. I	65 66	150. 7 151. 6	67. 5	25 26	205. 5	91.9	86	261.3	115. 9 116. 3
47 48	42. 9	19. 1	្ល	97.7	43.5	67 68	152.6	67. 9 68. 3	27	207. 4 208. 3	92. 3	87 88	262. 2	116.7
48 49	43. 9 44. 8	19.5	08	97. 7 98. 7 99. 6	43.9 44.3	69 69	153. 5 154. 4	68. 7	28 20	209. 2	92. 7 93. I	80	263. I 264. 0	117. 1
50	45.7	20.3	10	100.5	44.7	70	155.3	69. 1	30	210.1	93.5	99	264.9	117.5
51	46.6	20. 7	111	101.4	45. 1	171	156. 2	69.6	231	211.0	94.0	291	265.8	
52	47.5 48.4	21.2	12	102. 3	45. 6 46. 0	72	157. 1 158. 0	70.0	32	211.9	94-4 94-8	92	266.8	118.4
53 54	48.4	21.6	13	103. 2 104. I	40.0	73 74	158.0	70.4	33 34	212.9	95.2	93 94	267. 7 268. 6	119.2
55	50.2		l iš	105. 1	46. 4 46. 8	73	159.9	71. 2	35	214.7	35.6	1 %	269.5	120.0
55 56	51.2	22. 4 22. 8	15	105. I 100. 0	47.2	75 76	159. 9 160. 8	71.6	35 36	215.6	95.6 96.0	95 96	270.4	120. 4
57 58	52. 1	23. 2	17	106. 9	47. 6 48. 0	77 78	161. 7 162. 6	72.0	37 38	216.5	96.4	97	271.3	120.8
50	53. 0 53. 9	23.6 24.0	18	107. 5	48.4	70	163.5	72. 4	38 39	217.4 218.3	97. 2	98	272. 2	121. 2
59 60	53. 9 54. 8	24.4	20	106. 9 107. 8 108. 7 109. 6	48. 4 48. 8	79 80	164.4	73. 2	40	219.3	97.6	300	274.1	122.0
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Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.
•												[Fe	or 66 Deg	rees.

DIFFERENCE OF LATITUDE AND DEPARTURE FOR 25°.

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Let.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	0.9	0.4	61	55-3 56.2	25.8	121	109. 7	51. 1	181	164.0	76.5	241	218, 4	101.9
2	1.8		62	56.2	20, 2 26, 6	82		51.6	82	164.9	76.9	42	219. 3	102. 3
3 4	2.7 3.6	1.3	63 64	57. I 58. o	27.0	23 24	111.5	52.0	83 84	165. 9 166. 8	77.3	43 44	220, 2 221, 1	102. 7 103. I
- 31	4.5	2. 1	65	58. 9 59. 8	27. 5	25 26	113. 3	52.4 52.8	85 86	167. 7	77-3 77-8 78.2	45	222.0	103.5
5	4.5 5.4 6.3	2.5	66	59.8	27. 9 28. 3	26	114. 2	53. 2		167. 7 168. 6	78.6	45 46	223.0	104.0
7	6.3	3.0	67 68	60. 7 61. 6	28.3	27 28	115. 1	53-7	87 88	169. 5	79.0	47	223. 9 224. 8	104.4 104.8
9	7:3	3. 4 3. 8	69	62.5	28. 7 29. 2	20	116.0	54. 1	89	170.4	79-5	48	224. 0	104.8
10	9.1	4.2	70	63.4	29.6	30	116. 9 117. 8	54-5 54-9	3	172. 2	79. 9 80. 3	49 50	225. 7 226. 6	105.2
11	10,0	4.6	71	64. 3	30. 0-	.131	118. 7		191	173. 1	80. 7	251	227. 5	106. I
12	10. 9	5.1	72	65. 3 66. 2	30.4	32	119.6	55. 4 55. 8	92	174.0	81.1	52	228.4	106.5
13	11.8	6.6	73	66.2	30.9	33	120. 5	1 56. 2	93	174 9 175 8 176 7	81.6	53	229. 3	106.9
14	12. 7 13. 6	ş. 9	74	67. I 68. o	31.3	34	121.4	56.6	94	175.8	82, 0	54	230. 2	107. 3
15	14.5	5 5 7 7 8 6.	75 76	68.0	31.7	35 36	123. 3	57. 1 57. 5	95 96	170. 7	82. 4 82. 8	55 56	231. I 232. O	107. 8
17	15.4	.7.2	77 78	68. 9 69. 8	32.5	37	124. 2	57. 9	97	178. 5	82.2	57	232.0	108.6
18	15.4 16.3	7.6	78	70. 7 71. 6	33.0	37 38	125. 1	57. 9 58. 3	97 98	179. 4 180. 4	83. 7 84. I	57 58	232. 9 233. 8	109.0
19	17. 2 18, 1	8.0	79 80	71.6	33- 4 33- 8	39	126.0	58.7	99	180.4	84.1	59 60	234. 7 235. 6	109.5
20		8.5		72. 5		40	126.9	59. 2	200	181. 3	84. 5		235.6	109.9
21 22	19.0	8.9	81 82	73-4	34. 2	141	127. 8 128. 7 129. 6	59.6 60.0	201	182. 2	84.9	261 62	236. 5	110. 3 110. 7
83	19. 9 20, 8	9.3 9.7	83	74- 3 75- 2	34- 7 35. I	42 43	120.7	60.4	02	183. I 184. 0	85. 4 85. 8 86. 2	63	237. 5 238. 4	111. 1
24	21.8	10.1	87	76. I	25. 5	44	130. 5	60.9	%	184. 9 185. 8 186. 7	86. 2	64	239-3	111.6
25 26	22. 7 23. 6	10,6	85 86	77.0	35.9	45 46	131.4	61. 2	ું	185. 8	86.6	65 66	240. 2	112.0
	23.6	11.0		77. 9 78. 8	35. 9 36. 3 36. 8	46	132. 3	61.7		186. 7	87. 1	66	241. I	112.4
27 28	24. 5	11.4	87 88	70.0	37. 2	47 48	133. 2	62. 5	97 98	187. 6 188. 5	87.5	67 68	242.0	
29	25.4 26.3	12. 3	80	79.8 80.7	37. 6	49	134. I 135. 0	63.0	8	189.4	87. 9 88. 3	60	242. 9 243. 8	113.3
30	27. 2	12.7	90	81.6	37. 6 38. 0	50	135.9	63.4	10	190.3	88.7	70	244. 7	114 1
31	28. I	13.1	91	82. 5	28. 5	151		63.8	211	191.2	89. 2	271	245.6	114.5
32	29.0	13.5	92	83.4	38.9	52	136. 9 137. 8 138. 7	64.2	12	192. 1	89.0	72	246. 5	115.0
33	29. 9 30. 8	13.9	93	84.3	39- 3	53	138. 7	64.7	13	193. 0	90.0	73	247.4 248.3	115.4
34	21. 7	14.4 14.8	94	85. 2 86. 1	39. 7 40. I	54	139, 6 140, 5	65. I 65. S	14	193. 9	90.4	74	249. 2	116.2
35 36	31. 7 32. 6	15. 2	95 96	87. o	40.6	55 56	141.4	65. 9	15	194. 9 195. 8	91.3	75 76	250. 1	116.6
37 38	33-5	15.6	97 98	87. 9 88. 8	41.0	57 58	142. 3	65. 9 66. 4 66. 8	17	196. 7 197. 6 198. 5	91.7	77	251.0	117. 1
38	34-4	1.01		88, 8	41.4 41.8	58	143. 2	66.8		197. 6	92. 1	78	252.0	117.5
39 40	35. 3 36. 3	16. 5 16. 9	99 100	89. 7 90. 6	42.3	59	144. I 145. 0	67. 2 67. 6	19	199.4	92.6 93.0	123	252. 9 253. 8	117.9
41	37. 3	17.3	101	91.5	42.7	161	145.0	68. o	221	200. 3		281	254. 7	118.8
42	37. 2 38. 1	17.7	02	92.4	43. 1	62	145. 9 146. 8	68. 5	22	201. 2	93. 4 93. 8	82	254. 7 255. 6	119.2
43	30.0	18. 2	03	93.3	43-5	63	147. 7	68, q	23	202. I	94.2	83 84	256. 5	119.6
44	39. 9 40. 8	18, 6	04	94-3	44.0	64	148.6	69.3	24	203.0	94-7	84	257. 4 258. 3	120.0
45	40.0	19. 0 19. 4	05 06	94-3 95-2 96-1	44. 4 44. 8	65 66	149. 5 150. 4	69. 7 70. 2	25 26	203. 9 204. 8	95. I 95. 5	85 86	250. 3 259. 2	120.4
47	41.7 42.6	19.9	07	97.0	45. 2	67 68	151.4	70.6	27	205. 7	95. 0	87 88	200. I	121.3
47	43-5	20, 3	97 98	97. 9 98. 8	45. 6 46. I		152. 3	71.0	28	205. 7 206. 6	95. 9 96. 4 96. 8	88	261.0	121.7
49	44-4	20. 7	09	98.8	46. I	69	153. 2	71.4 71.8	29	207. 5 208. 5	96.8	89	261. 9 262. 8	122. 1
50	45.3	21, 1	10	99. 7	46.5	70	154-1		30		97.2	90		122.6
51 52	46. 2	21.6	111	100. 6	46.9	171 72	155.0	72.3	231 32	209.4	97. 6 98. 0	291 92	2637 264. 6	123.0
53	47. I 48. 0	22.4	13	102.4	47. 3 47. 8 48. 8	73	155. 9 156. 8	73. 1	33	211.2	08.5	93	265. 5	123. 4 123. 8
34	48. 9 49. 8	22. 4 22. 8	14	103. 3	48.8	74	157.7	73-5	ĭ4	212. I	98.9	04	266. 5	124.8
54 55 50	49.8	23. 2	15	104. 8	48.6	74 75 76		74.0	34 35 36	213.0	99-3	95	267. 4 268. 3	124.7
50	50.8	23. 7 24. I	16	105.1	49.0	70	159. 5	74.4	30	213.9 214.8	99- 7 100- 2	90	268. 3 269. 2	125. I
57 58	\$1. 7 58. 6	24. 5	178	100.0	49.4	77	161.3	75. 2	37 38	215. 7	100. 6	97 98	270. I	125.9
59	53.5	24.9	19	107. 0	50.3	2	164, 4	75. 2 75. 6 76. 1	39	#15. 7 #16. 6	101.0	99	271.0	196. 4 186. 8
60	54.4	25.4	só.	106, 8	50.7	80	163, 1	76. z	40	217.5	101.4	300	a71. 9	126. 8
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Plat.	Dop.	Lat	Dist.	Dep.	Let.	Dist.	Dop.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Let.

DIFFERENCE OF LATITUDE AND DEPARTURE FOR 26°.

Dist.	Lat	Dep.	Dist.	Lat.	Dep.	Dist.	Lat	Dep.	Dist.	Lat.	Dep.	Dist.	Lat	Dep.
1	a. 9 1. 8	0.4	61	54.8	26. 7	121	108.8	53.0	181	162. 7	79-3	241	216.6	105.6
3	1.8	0.9	62	55. 7 56. 6	27. 2	22	109. 7	53- 5	83	163.6	79- 3 79- 8 80- 2	42	217.5	106. 1
3	2.7 3.6	1.3	63	50.0	27. 6 28. I	23 24	111.5	53.9	83 84	164. 5	80.7	43	219.3	106. 5
ş	4.5	2.2	65	57· 5 58· 4	28. 5	25	112.3	54. 4 54. 8	85 86	166. 3	81.1	45	220. 2	107.4
	63	2.6	66	59.3	28. 9	26	113.2	55.2	86	167. 2	81.5	45 46	221. I	107. 4
7	0.3	3.1	67 68	61.1	29. 4	27 28	114.1	55. 7 56. 1	87 88	168.1	82. 0 82. 4	47	222. 0 222. 9	108. 3
9	Z: 2	3.5	69	62.0	29. 8 30. 2	29	115.0	56.5	80	160.0	82. 9	49	223.8	100.7
10	9.0	44	70	62.9	30. 7	30	115.9	57.0	90	169.9 170.8	83.3	50	224.7	109.6
11	9.9 10.8	4.8	71	63.8	31. 1	131	117.7	57-4	191	171. 7	83.7	251	225.6	110.0
12	10.8	5.3	72	64. 7 65. 6	31.6	32	118.6	57. 9 58. 3	92 93	172.6	84. 2 84. 6	52	226. 5	110. 5 110. 9
14	11. 7 12. 6	5. 7 6. 1	73 •74	l 66.5	32.4	33 34	120.4	58. 7	94	174.4	85.0	53 54	228. 3	111.3
15 16	13.5	6.6	75	67.4 68.3	32. 0	35 36	121.3	59. 2	95	175.3	85.5	55 56	229. 2	111.3
16	14.4	7.0	76	68. 3	33. 3 33. 8	36	122. 2	59.6 60.1	96	176. 2	85.9	56	230. 1	112. 2
17	15.3	7.5	77 78	69. 2 70. I	33. 8	37 38	123. I 124. 0	60.5	97 98	177. 1	86. 4 86. 8	57 58	231.0	112. 7
19	17. 1	7.9 8.3 8.8	Į į	71.0	34.6	30	124.9	60. ŏ	99	178.9	87. 2	1 50	232.8	113.5
20	18.0			71.9	35. I	36	124. 9 125. 8	61.4	200		87.7	59 60	233.7	114.0
21 22	18. 9 19. 8	9.2	81 82	72. 8	35-5	141	126. 7	61.8	201	180. 7 181. 6	88. I 88. 6	261	234.6	114-4
23	20.7	9.6 IQ.1	83	73. 7 74. 6	35.9	42 43	127.6	62. 2	02 03	182. 5	89.0	62 63	235. 5 236. 4	114.9
24	20. 7 21. 6	10.5	84	75.5	35. 9 36. 4 36. 8	44	129.4	63. 1	04 04	183.4	89.4	64	237.3	115.7
25 26	22.5	11.0	85 86	75.5 76.4	37-3	45	130. 3	63.6	οş	184.3	89.9	65		116.2
20	23.4 24.3	11.4	86	77. 3 78. 2	37. 7 38. 1	46	131. 2	64.0	06 07	185. 2 186. 1	90.3	66	239. I 240. 0	116.6
28	85.2	12.3	87 88	70. 3	38.6	47 48	133.0	64.9	1 %	186. a	91.2	67 68	240.0	117.0
29	25. 2 26. 1	12. 7	89	79. I 80. 0	39.0	49	133. 9 134. 8	65. 3 65. 8	09	187. 8	91.6	69	241.8	117. 0
30	27. 0	13.2	90	80.9	39. 5	50	134.8	65. 8	10	188. 7	92. 1	70	242. 7	118.4
31	27. 9 28. 8	13.6 14.0	91 92	81. 8 82. 7	39.9	151	135. 7 136. 6	66, 2 66, 6	211	189. 6 190. 5	92. 5 92. 9	271	243.6	118.8
32 33	20.7	14.5	93	83.6	40. 3 40. 8	52 53	137. 5	67. 1	13	191.4	92.4	72 73	244. 5 245. 4	119. 2 119. 7
34	29. 7 30. 6	14.9	94	84.5	41.2	54	137. 5 138. 4	67. 5	14	192. 3	93. 4 93. 8	74	246.3	120. 1
35 36	34. 5	15. 3 15. 8	95 96	85.4 86.3	41.6 42.1	55 56	139. 3 140. 2	67. 9 68. 4 68. 8	15	193. 2 194. I	94.2	75	247. 2 248. I	120.6
37	33-3	18.2	97	87.2	42.5	57	141. 1	68. 8	17	195.0	95.1	1 77	249.0	121.4
. 37 38	34.3	16. 7	97 98	87. 2 88. 1	43.0	57 58	142. 0	69.3	18	195. 9 196. 8	95.6	77 78	249. 9 250. 8	121.9
39	35. I 36. 0	17.1	99	89.0	43. 4 43. 8	59	142. 9 143. 8	69. 7	19	196.8	96. o 96. 4	79 80	250.8	122. 3
40 41	36.9	18.0	101	89.9 90.8	43.8	161	143. 8	70. 1	20	197. 7	96. 9	281	251. 7 252. 6	122. 7
42	37.7	18.4	02	91.7	44- 7	62	145.6	71.0	222	199.5	97.3	82	253.5	123.6
43	37· 7 38. 6	18. 8	03	92:6	45. 2	63	146.5	71.5	23	200. 4	97. 3 97. 8	83	254.4	124.1
44	39- 5	19. 3 19. 7	04	93-5	45. 6 46. 0	64	147.4 148.3	71.9	24	201. 3	98. 2 98. 6	84	255. 3 256. 2	124.5
45 46	40.4 41.3	20. 2	05	94-4	46.5	65 66	149. 3	72. 3 72. 8	25 26	203. 1	99.1	85 86	250. 2	124.9
47 48	42. 2	20.6	07	95. 3 96. 2	46.0	67 68	150. 1	73. 2	27	204.0	99.5	87	257. I 258. O	125. 4 125. 8
48	43. 1	21.0	08	97. I 98. o	47.3		151.0	73.6	28	204.9	99.9	88	258.9	126.3
49 50	44.0 44.9	21.5	10	98.0 98.0	47. 3 47. 8 48. 2	69 70	151.9 152.8	74. I 74. S	29 30	205. 8	100. 4	89 90	259. 8 260. 7	126. 7 127. I
51	45. 8	22. 4 22. 8	111	99.8	48. 7	171		75.0	231	207. 6	101. 3	291	261.5	127.6
52	45.8		12	100. 7	49. 1	72	153. 7 154. 6	75. 4 75. 8 76. 3	32	208.5	101.7	92	262. 4	128,0
53 54	47. 6 48. 5	23. 2 23. 7	13	101.6	49. 5 50. 0	73	155. 5 156. 4	75.8	33	209.4	102. 1	93	263. 3 264. 2	128. 4 128. 9
55	49-4	24.1	14 15	103.4	50.4	74	157.3	76. 7	34	211. 2	103.0	94 95	265. I	
55 56	50. 3	24.5	15 16	104.3	50.9	75 76	158. 2	77. 2	35 36	212. 1	103. 5	96	266. o	129. 3 129. 8
57 58	51. 2 52. 1	25. 0 25. 4	17	105. 2	51. 3	77 78	159. I 160. o	77. 6 78. 0	37 38	213.0	103.9	97	266. 9	130. 2
59	53.0	25.4	10	107.0	51. 7 52. 2	70	160.0	78.5	38 39	213. 9 214. 8	104. 3	98	267. 8 268. 7	130.6 L31.1
66	53. 9	26. 3	20	107.9	52. 6	79 80.	161.8	78.9	40	215. 7	105. 2	300	269.6	131.5
Dist.	Dep.	Lat.	Dist.	-		-			—			-		
	Dep.		DIR.	Dep.	Lat	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.
												[Fe	or 64 Deg	rees.

DIFFERENCE OF LATITUDE AND DEPARTURE FOR 27°.

Dist.	Lat.	Dep.	Dhit.	Lat.	Dop.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	0. 9 1. 8	0.5	61	54-4	27. 7 28. 1	121	107.8	54-9	181	161.3	82. 2	241	214. 7 215. 6 216. 5	109.4
2	1.8	0.9	62 63	55. 2 56. I	28, 1	22	108. 7	55.4	82 83	162.2	82. 6 83. 1	42	215.0	109.9
3	2. 7 3. 6	1.4	64	57.0	29. I	23, 24	110.5	55. 4 55. 8 56. 3	84	163. 1	83. 5	43 44	217.4	110.3 110.8
5	4.5	2.3	65 66	57. 9 58. 8	29.5	25 20	111.4	56. 7	85 86	163. 9 164. 8	84.0	45	217.4 218.3	111.2
	4·5 5·3 6·2	2.7		58.8	30.0	26	112. 3	57. 2	86	165. 7 166. 6	84.4	45 46	219. 2	111. 7
3	0.2	3.2 3.6	67 68	59. 7 60. 6	30. 4	27 28	113.2	57· 7 58. I	87 88	100.0	84.9	47 48	220, I 221, 0	112.1
ا ۋا	7. I 8. o	4.1	66	61.5	30. 9	20	114.0	58.6	89	167. 5 168. 4	85. 4 85. 8	49	221.0	113.0
16	8.9	4.5	70	62.4	31. 3 31. 8	30	114.9 115.8	59.0	90	169. 3	86. 1	50	222. 8	113.5
11	9.8	5.0	71	63. 3	32. 2	131	116. 7 117. 6 118. 5	59- 5	191	170.2	86. 7	251	223.6	1140
12	10. 7 11. 6	5-4	72	64.2	32. 7	32	117.6	59.9	92	171. 1	87.2	52	224. 5	114.4
13 14	12.5	5.9 6.4 6.8	73	65.0	33. I	33	118.5	60.4 60.8	93	172.0	87. 6 88. 1	53	225. 4 226. 3	114.9
1 3	13.4	1 6.8	74 75	65. 9 66. 8	33. 6 34. 0	34	119.4	61.3	94	172.9 173.7	88.5	54	220. 3	115.3
15	14.3	7.3	75 76	67. 7 68. 6	34-5	35 36	121. 2	61. 7	95 96	174.6	89.0	55 56	228. I	110.2
17	15. I 16. 0	7.7	77 78	68.6	35.0	37 38	122. 1	62. 2	97 98	175.5	89.4	57 58	229.0	116. 7
18	10.0	8.6	78	69.5	35-4	38	123.0	62. 7		176.4	89.9	58	229. 9 230. 8	117. 1
20	16. 9 17. 8	9.1	79	70.4	35. 9 36. 3	39 40	123.8	63. I 63. 6	99°	177. 3 178. 2	90.3	59	230.0	117.6
21	18. 7	9.5	81	72. 2	36.8	141	125.6	64.0	201	179.1	91.3	261	232.6	118.5
22	19.6	10.0	82	73.1	37. 2	42	126.5	64.5	02	180.0	91.7	62	233.4	118.9
23	20. 5	10.4	83	74.0	37. 7 38. 1	43	127.4	64.0	03	180. 9	92.2	63	234-3	119.4
24	21.4	10.9	84	74.8	38. 1	44	128. 3	65.4	04	181.8	92.6	64	235. 2	119.9
25 26	22. 3 23. 2	11. 3	85 86	75. 7 76. 6	38. 6 39. 0	45 46	129. 2 130. I	65. 4 65. 8 66. 3	05 06	182. 7 183. 5	93. I 93. 5	65 66	236. I 237. 0	120, 3 120, 8
27 28	24. I	12. 3	87 88	77·5 78.4	39.5	47	131.0	66. 7	07	184.4	94.0	67	237. 0	121. 2
	24.9	12. 7		78.4	40.0	47 48	131.0	67. 2	% %	185. 3	94-4		237. 9 238. 8	121. 7
29	24. 9 25. 8 26. 7	13. 2	89	79. 3 80. 2	40.4	49	132.8	67. 6 68. I	9	186.2	94-9	69	239. 7 240. 6	122, 1
30	20. 7	13.6	90	81. 1	40.9	50 151	133-7	68.6	10	187. 1 188. o	95.3	70		122. 6
31 32	27.6 28.5	14. I 14. 5	91 92	82.0	41. 3 41. 8	52	134- 5 135- 4	69.0	211 12	188.0	95. 8 96. 2	271 72	241. 5 242. 4	123. 0 123. 5
33	29.4	15.0	93	82. 9	42. 2	53	136.3	69.5	13	188. 9 189. 8	96.7	73	243.2	123.9
1 34	30. 3	15.4	l· 94	83.8	42. 7	54	137. 2	69.9	14	190.7	97. 2	74	244 I'	124.4 124.8
35 36	31. 2 32. I	15.9	95 96	84.6	43. 1	55 56	138.1	70. 4 70. 8	15 16	191.6	97.6 98. t	75	245.0	124. 8
37	33.0	16.3	97	85. 5 86. 4	43. 6 44. 0	27	139.0	71.3	17	192. 5	98.5	1 70	245. 9 246. 8	125. 3
37 38	33.9	17. 3	97 98	87. 3	44-5	57 58	139. 9 140. 8	71.7	17	194. 2	99.0	77 78	247. 7	126. 2
39	34- 7	17.7	99		44.9	59	141.7	72. 2	19	195. 1	99.4	79	247. 7 248. 6	126.7
40			100	89.1	45-4		142.6	72.6	20	196.0	99-9		249.5	127. 1
41 42	36. 5	18. 6 19. 1	101	90.0	45. 9 46. 3 46. 8	161 ' 62	143. 5	73. 1	22 I 22	196. 9 197. 8 198. 7	100. 3	281 82	250.4	127.6 128.0
43	37· 4 38. 3	19.5	03	90. 9 91. 8	46.8	63	144. 3 145. 2	73- 5 74- 0	23	108.7	101. 2	83	251. 3 252. 2	128.5
44	39. 2	20.0	04	92. 7	47. 2	64	146. 1	74.5	24	199. 0	101.7	84	253.0	128.9
44 45 46	40. 1	20.4	05 06	93.6	47. 7 48. 1	65 66	147.0	74-9	25 26	200. 5	102, 1	85 86	253. 9 254. 8	129.4
# <u>^</u>	41.0	20.9	00	94-4	48.1	60	147. 9	75. 4 75. 8 76. 3	20	201.4	102.6	86	254.8	129.8
47	41.9 42.8	21. 3 21. 8	07 08	95. 3 96. 2	49.0	67 68	149.7	12.2	27 28	203. I	103. 5	87 88	255. 7 256. 6	130. 3 130. 7
49	43. 7 44. 6	22. 2	09	97. 1	49-5	69	150.6	76.7	29	204.0	104.0	89	257.5	131.2
50	44.6	22. 7	10	98.0	49.9	70	151.5	77. 2	30	204.9	104.4	90	257. 5 258. 4	131.7
51	45. 4 46. 3	23. 2	111	98. 9 99. 8	50. 4 50. 8	171	152.4	77. 6 78. 1	231	205. 8	104.9	291	259. 3	132. I
52 52	40.3	23. 6 24. 1	13	100.7	50.8	72 73	153. 3 154. I	78.5	32 33	206. 7 207. 6	105. 3	92 93	260. 2 261. I	132.6 133.0
53 54	47. 2 48. 1	24.5	14	101.6	51.3 51.8	74	155.0	79.0	33	208.5	106.2	94	262.0	133.5
55	49.0	25.0	15	102. 5	522	75 76	155. 9 156. 8	79-4	35 36	209.4	106. 7	95 96	262.8	133.9
56	49. 9 50. 8	25.4	16	103. 4	52. 7	76	156.8	79. 9 80. 4		210.3	107. 1	96	263. 7	134.4 134.8
55 56 57 58	50. 8	25.9	17 18	104. 2	53. 1 53. 6	77 78	157. 7 158. 6	80.4	37- 38	211. 2 212. I	107.6	97 98	264.6	134.8
59 60	51. 7 52. 6	26. 3 26. 8	19	106.0	54.0	79 80	159.5	81.3	39	213.0	108.5	99	265. 5 266. 4	135.7
66	53- 5	27. 2	zó	106.9	54-5	8ó	159. 5 160. 4	81.7	40	213.8	109. ó	300	267. 3	135. 7 136. 2
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dèp.	Lat.
												[Fo	or 63 Deg	rees.

	D	FFE	REN	CE O	F LA	TIT	UDE	AND	DE	PART	URE	FOR	. 28°.		
Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Let.	Dep.	Dist.	Lat.	Dep.	Diet.	Lat	Dep.	
1 2	a. 9 1. 8	0.5	61 62	53- 9 54- 7	28. 6 29. I	121	106. 8	56. 8 57- 3	131 82	159. 8	85. o 85. 4	24I 43	212.8	113.1	
3	2.6	1.4	63	54 7 55 6 56 5	29.6	23	107. 7 108. 6	57· 7 58. 2	83 84	160. 7 161. 6 162. 5	85. 9 86. 4	43	213. 7 214. 6	114 1	
4 5	3. 5 4. 4	1.9 2.3 2.8	\$58	57: 4 58: 3	30.0 30.5	24 25 20	109. 5 110. 4	58.7	85 86	163. 3	86. o	44 45 46	215.4 216.3	114.6 115.0	
5	5.3		66	58.3	31. 0 31. 5	26 27	111. 3	59. 2	86 87	164. 2 165. I	87. 3 87. 8 88. 3	46 47	217. 2 218. I	115.5	
8	7. 1	3.3 3.8	67 68	59. 2 60. 0	31.9	27 28	113.0	59.6 60.1 60.6	87 88 89	166. o	88. 3 88. 7	47 48	219.0 219.9	116.4	
9	7. 9 8. 8	4.2 4.7	69 70	60. 9 61. 8	32. 4 32. 9	29	113.9 114.8	61. o	90	166. 9 167. 8	89.2	49 50	220. 7	117.4	
11 12	9.7 10-6	5, 2 5, 6	71 72	62. 7 63. 6	33- 3 33- 8	131 32	115.7 116.5	61. 5 62. 0	191 92	168. 6 169. 5	89. 7 90. I	251 52	221. 6 222. 5	117.8	
13	11.5	6.1	73	64.5	34-3	33	117.4	62.4	93	170.4	90.6	53	223.4	118.3	
14	12.4 13.2	6.6 7.0	74 75 76	65. 3 66. 2	34- 7 35- 8	34 35	119. 2	62. 9 63. 4 63. 8	94 95 96	171. 3 172. 2	91. I 91. 5	54 55 56	224. 3 225. 2	119.2 • 119.7	
16	14. I 15. o	7.5	76	67. 1 68. o	35. 7 36. 1	35 36	120. I 121. 0	63.8 64.3	96	173.1	92. 0 92. 5	56	226. 0 226. 0	120. 2 120. 7	
17	18 13.9 8.5 78 68.9 79. 69.8 37.1 39 122.7 65.3 99 174.8 03.0 58 227.8 121.1 [9] 16.8 8.9 79 69.8 37.1 39 122.7 65.3 99 175.7 93.4 59 228.7 121.6 10 17.7 9.4 80 70.6 37.6 40 123.6 65.7 200 176.6 93.9 00 229.6 122.1														
20	20 17. 7 9. 4 80 70. 6 37. 6 40 123. 6 65. 7 200 176. 6 93. 9 60 229. 6 122. 1 21 18. 5 0. 9 81 71. 5 28. 0 141 124. 5 66. 2 201 177. 5 94. 4 261 230. 4 122. 5														
21	20 17.7 9.4 80 70.6 37.6 40 123.6 65.7 200 176.6 93.9 60 220.6 122.1 21 18.5 9.9 81 71.5 38.0 141 124.5 66.2 201 177.5 94.4 261 230.4 122.5 22 10.4 10.1 2.8 22 22 10.4 10.1 2.8 22 23 24.8 25 23 25 24 25 25 25 25 25 25 25 25 25 25 25 25 25														
23	22 10 4 10 2 82 72 4 28 5 42 125 4 66 7 02 178 4 04 8 62 231 2 122 0														
24 25 26	23 20.3 10.8 83 73.3 39.0 43 126.3 67.1 03 179.2 95.3 63 232.2 123.5 24 31.2 11.3 84 74.2 39.4 44 127.1 67.6 04 180.1 95.8 64 233.1 123.9 25 12.1 11.7 85 75.1 39.9 45 128.0 68.1 05 181.0 96.2 65 234.0 124.4														
26 27	23. 0 23. 8	12.2	86 87	75. 9 76. 8	40. 4 40. 8	45 46	128. 9 129. 8	68. 5 69. 0	06 07	181. 9 182. 8	96. 7 97. 2	66	234. 9 235. 7	124.9	
28	. 24. 7	12.1	87 88	77. 7 78. 6	41. 3 41. 8	47 48	130. 7 131. 6	69.5	07 08	182.7	97. 7 98. I	67 68	235. 7 236. 6	125. 3 125. 8	
29 30	25. 6 26. 5	13. 6 14. 1	89 90	79-5	42. 3	49 50	131. 0	70.0	10	184. 5 185. 4	98.6	69 70	237. 5 238. 4	126. 3 126. 8	
31 32	27. 4 28. 3	14. 6 15. 0	91 92	80. 3 81. 2	42. 7 43. 2	151 52	133. 3 134. 2	70.9	211	186. 3 187. 2	99. I 99. 5	271 72	239. 3 240. 2	127. 2	
33 34	29. I	15. 5 10. 0	93	82. 1	43-7	53	135. I 136. 0	71. 4 71. 8	13	188. I	100.0	73	241.0	127. 7 128. 2 128. 6	
34 35 36	30. 0 30. 9 31. 8	16.4	94 95 96	83. 0 83. 9 84. 8	44 î 44 6	54 55	136.0	72. 3 72. 8	14 15	189. 0 189. 8	100. 5 100. 9	74 75 76	241. 9 242. 8	129. 1	
36	31. 8 32. 7	16.9	96	84. 8 8c. 6	45.1	55 56	137. 7 138. 6	73- 2 73- 7	16	190. 7 191. 6	101.4	76	243. 7 244. 6	129. 6 130. 0	
37 38	33. 6	17. 4 17. 8 18. 3	97 98	85. 6 86. 5	45. 5 46. 0	57 58	139.5	74. 3	17 18	192. 5	102. 3	77	245-5 246-3	130.5	
39 40	34· 4 35· 3	18. 3 18. 8	99 100	87. 4 88. 3	46. 5 46. 9	59	140. 4	74.6 75. I	19 20	193. 4 194. 2	103. 8	79	247. 2	131. 0 131. 5	
41 42	36. 2	19. 2	101	89. 2 90. I	47.4	161 62	142. 2 143. 0	75.6 76.1	23 I 22	195. I 196. o	103. 3 103. 8 104. 8	281 82	248. 1 249. 0	131. 9 132. 4	
43	37. I 38. o	20. 2	03	90.9 91.8	47. 9 48. 4 48. 8	63	143. 0 143. 9 144. 8	76.5	23	196. 9	104.7	83 84	249. 9 250. 8	132.9	
44 45 46	38.8 39.7 40.6	20. 7 21. I	8.8.8	91.8	49-3	8.8.8	144-8	77. 0 77. 5	4 278	198.7	105. 2	84 85 86	251.6	133. 3 133. 8	
46	40. 6 41. 5	21. 6 22. 1	06 07	92. 7 93. 6 94. 5	49. 8 50. 2	66	145. 7	77.9 78.4	26	199. 5	106. I 106. 6	86 87	252. 5 253. 4	134-3 134-7	
47 48	42. 4	22. 5	% %	95.4 96.8	50.7	67 68	147. 5 148. 3	78.9	27 28	201. 3	107. 0	88	254-3	135. 2	
49 50	43-3 44-1	23. 0 23. 5	10	90. 2 97. I	51. 2 51. 6	69 70	149. 2 150. 1	79-3 79-8	29 30	202. 2 203. I	107. 5	\$9 90	255. 2 256. 1	135. 7 136. I	
51 52	45. 0	23. 9 24. 4	111	08.0	52. 1 52. 6	171 72	151.0	80.3 80.7	231 32	204. 0 204. 8	108.4	291	256. 9 257. 8	136.6	
53	45. 9 46. 8	24.9	13	98. 9 99. 8	53. I	73	151.9 152.7 153.6	81.2	33	204. 8 205. 7 206. 6	109-4	92 93	257. 8 258. 7 259. 6	137. 1 137. 6	
54 55	47. 8	25. 4 25. 8 86. 3	14	100. 7	53. 5 54. 0	74	153.6	81. 7 82. 2	34	205.6	109.9	94	259.6 260.5	138.0	
55 56	49-4 50-3	26. 3 26. 8	15 16	102.4	54-5	75 26	155. 4 156. 3	82.6	35 36	207. 5	110. 3 110. 8 111. 3	95 96	261. 4 262. 2	139.0	
57 58	51. 8	27. 2	17 18	103. 3 104. 2	54-9 55-4	77 78	150. 3 157. 2 158. 0	83. 1 83. 6	37 38	209. 3 210. 1	111.7	97 98	263. 1	139-4 139-9	
8	52. I 53. O	27. 7 28. 2	19 20	105. 1 100. 0	55. 9 56. 3	79	158. 0 158. 9	84.0 84.5	39 40	211.0 211.9	112.2	99 300	264. 0 264. 9	140. 4 140. 8	
Dist.	Dep.	Lát.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	
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DIFFERENCE OF LATITUDE AND DEPARTURE FOR 29°.

Dist.	Lat.	Dep.	Dist.	Lat	Dep.	Dist.	Lat.	Dép.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
\vdash		<u> </u>				-			-		<u> </u>			
	0.9	0.5	61	53-4	29.6	121 22	105.8	58. 7	181 82	158. 3	87. 8 88. 2	241	210.8	116.8
2	1. 7 2. 6	1.0	62 63	54.2	30. I 30. 5	22	106. 7 107. 6	59. 1	83	159. 2 160. I	88. 7	42 43	211.7	117. 3
3		1.5	64	55. I 56. o	31.0	24	103.5	59. 6 60. I	84		89.2	44	213.4	118. 2
1 2	3. 5 4. 4	2.4	65	56.9	31.5	25	109. 3	60.6	85 86	160. 9 161. 8	89.7		214.3	118. 3 118. 8
5	č. 3	2.9	66	57. 7 58. 6	32.0	26	110.2	61. I	86	162. 7	90.2	45 46	215. 2	119.3
7	5.2 6.1	3.4	67	58.6	32. 5	27	111.1	61.6	87 88	163.6	90.7	47	216.0	119. 7
	7.0	3.9	68	59. 5	33.0	28	112.0	62. 1		164.4	91. 1		216. 9 217. 8	120. 2
18	7.9 8.7	4.4	69	60. 3 61. 2	33. 5	29	112.8	62. 5 63. 0	89 90	165. 3 166. 2	91. 6 92. 1	49 50	217. 0	121. 2
		4.8	70	62. 1	33.9	30	114.6	63.5	191	167. 1	92. 6	251	219.5	121.7
11	9.6 10.5	5. 3 5. 3 6. 3 6. 8	71 72	63.0	34-4 34-9	131 32	115.4	64.0	.93	167. 0	93. 1	52	220.4	122. 2
13	11.4	6.2	1 73	62.8	25.4	33	116.3	64.5	93	167. 9 168. 8	93.6	53	221. 3	122. 7
14	12. 2	6.8	74	64.7	35. 9	34	117. 2	65.0	94	169. 7	94-1	53 54	222. 2	123. I
15	13. 1	7. 3 7. 8 8. 2	75	64. 7 65. 6 66. 5	35. 9 36. 4 36. 8	35 36	118.1	65.4	95 96	170.6	94-5	55 56	223.0	123.6
	14.0	7.8	76	66. 5	36. 8	30	118.9	65. 9 66. 4	90	171.4	95.0	50	223. 9 224. 8	124. I 124. 6
17	14.9	8. 7	77 78	67. 3 68. 2	37. 3	37 38	120.7	66. 0	97 98	173. 2	95. 5 96. 0	57 58	225. 7	125. 1
10	15. 7 16. 6	9.2	/°	69. 1	36. 2	39	121.6	67.4	99	174.0	96.5	59 60	226. 5	125.6
20	17.5	9.7	79	70.0	37. 3 37. 8 38. 3 38. 8	40	122.4	67. 9	200	174-9	97. ó		227. 4	126. I
21	18.4	10. 2	81	70.8		141	123. 3	68. 4 68. 8	201	175.8	97-4	261	228. 3	126.5
22	19. 2	10. 7	82	71. 7 72. 6	39. 3 39. 8	42	124. 2	68. 8	02	170.7	97. 9 98. 4	62	229. 2	127.0
23	20. 1	11.2	83	72.6	40.2	43	125. 1	69. 3 69. 8	03 04	177.5	98.4 98.9	63 64	230. O	127. 5 128. 0
24	21.0 21.0	11.6 12.1	84	73.5	40. 7 41. 2	1 44	125. 9 126. 8	70.2		179.3	99.4	6	230. 9 231. 8	128.5
25 26	21.9	12.6	85 86	74-3	41.7	45 46	127. 7	70.3 70.8	3	180. 2	99.9	65 66	232.6	129.0
27	22. 7 23. 6	13. 1	87 88	75. 2 76. 1	42. 2	47	127. 7 128. 6	71. 3 71. 8	97 08	181.0	100.4	67 68	233. 5	129.4
28	24.5	13.6		77.0	42.7	47 48	129.4			181.9	100. 8		234-4	129.9
29	25.4	14.1	89	77. 8 78. 7	43. 1	49	130. 3	72. 2	99	182. Š 183. 7	101. 3 101. 8	69 70	235. 3 236. 1	130.4
30	26. 2	14.5	90		43.6	50	131.2	72. 7	211	184.5	101.8	271	237.0	131.4
31	27. 1 28. 0	15.0	91	79.6 80.5	44. I 44. 6	151 52	132. 1	73. 2	112	185. 4	102. 3 102. 8	72	237. 0	131.9
32 33	28.9	15. 5 16. 0	93	81.3	45. 1	53	132. 9 133. 8	73· 7 74· 3	13	186. 3	103. 3	73	237. 9 238. 8	132.4 132.8
34	29. 7	16.5	94	82.2	45. 6 46. 1	54	134.7	74-7	14	187. 2	103. 7	74	239. 6	132.8
35 36	29. 7 30. 6	17.0	95 96	83. 1	46. 1	55 56	135.6	75- 1	15	188.0	104. 2	75 76	240. 5 241. 4	133. 3 133. 8
36	31.5	17.5	96	84.0	46. 5	50	136.4	75.6 76. i		189.8	104.7	70	242.3	133.0
37 38	32. 4	17. 9 18. 4	97 98	84.8	47.0	57 58	137. 3 138. 2	76.6	13	190. 7	105. 7	77 78	243. I	134. 3 134. 8
39	33. 2 34. 1	18. 9	<u>چو</u>	85. 7 86. 6	47. 5 48. 0	50	139. 1	77. 1	19	191.5	105. 7	79	244.0	135.3
46	35. 0	19.4	100	87.5	48.5	66	139.9	77.6	20	192.4	106. 7		244-9	135.7
41	35.0	19.9	101	88.3	49.0	161	140.8	78. 1	221	193. 3	107. 1	281	245.8	136.2
42	36. 7 37. 6 38. 5	20. 4 20. 8	02	89.2	49-5	62	141. 7 142. 6	78. 5	22	194.2	107.6	82 83	246.6	136. 7 137. 2
43	37.6	20. 8	03	90.1	49.9	63 64	142.0	79.0	23 24	195. 0	108.6	84	247. 5 248. 4	137.7
44	38. 5 39. 4	21.3	04	91.0	50.4 50.9	65	143. 4 144. 3	79. 5 80. 0		196.8	109. 1	85 86	249-3	137.7 138.2
45	40.2	22. 2	ુક	92. 7	51.4	65 66	145. 2	80.5	25 26	197. 7 198. 5	109.6	86	250. I	138.7
47	41.1	22. 3 22. 8	07	92. 7 93. 6	51.9	67	146. 1	81. ō	27 28	198.5	110. 1	87 88	251.0	139.1
47	42.0	23. 3 23. 8	08	94-5	52. 4 52. 8	68	146. 9 147. 8	81.4		199.4	110.5	88 80	251. 9 252. 8	139. 6 140. I
49	42.9	23.8	09	95.3 96.3	52.8	69 70	147.8	81.9 82.4	29 30	200. 3	111.0	90	252. 6	140.6
50	43.7	24. 2	111		53. 3 53. 8	171	149.6	82.9	231	202. 0	112.0	291	254·5	141.1
51 52	44.6	24. 7 25. 2	111	97. 1 98. 0	33.8	72	150.4	83.4	32	202. 9	112.5	92	255. 4 256. 3	141.6
53	45. 5 46. 4	25. 7	13	98.8	54- 3 54- 8	73	151.3	83. Q	33	203. 8	113. 0	93	256. 3	142.0
14 l	47. 2 48. 1	25. 7 26. 2	14	99. 7 100. 6	55. 3 55. 8	74	152, 2	84. 4 84. 8	34	204. 7	113.4	94	257. I 258. O	142.5
55 56	48. 1	26. 7	15 16	100.6	55.8	75	153. 1	84.8	35 36	205. 5	113.9	95 96	258.0	143. 0 143. 5
56	49.0	27. 1		101.5	56. 2 56. 7	70	153. q 154. 8	85. 3 85. 8	30	207. 2	114.4	37	258. 9 259. 8	144.0
57 58	49.9	27. 6 28. 1	17	103. 2	57. 2	77	155.7	86. 3 86. 8	37 38	207. 3	115.4	97 98	260.6	144.5
1 6	50. 7 51. 6	28.6	10	104. I	57.7	72	155. 7 156. 6	86. 8	39	209.0	115.9	99	261. 5	145.0
59 60	52. 5	29. I	20	105.0	57. 7 58. 2	86	157.4	87. 3	40	209. 9	116.4	300	262.4	I45. 4
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Let.
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DIFFERENCE OF LATITUDE AND DEPARTURE FOR 80°.

Dist.	Lat.	Dop	Diet	lat	Dep	Dist	Lat.	Dep	DM.	1 at.	Dep	DML	l.at.	Delr
-	0.9	0.5	61	52. 8	30.5	121	104. 8	60 5	181	156.8	90.5	241	208.7	120. 5
1 3	1.7	1.0	62	53-7	31.0	22	105. 7	61.0	82	157.6	91.0	42	209.6	121.0
3	1.7	1.5	63	53- 7 54- 6	31.5	23	106.5	61. 5	83	158.5	91.5	43	210.4	121. 5 122. 0
l :	3·5 4·3	2.0	64	55. 4 56. 3	32. 0 32. 5	24	107.4	62. 0 62. 5	84 8c	159. 3 160. 2	92.0	44	211. 3 212. 2	122.5
ş	Ç 2	33	65 66	57.2	33.0	26	109. I	63.0	85 86	161. 1	93.0	45 46	213.0	123.0
7	6.1	3.5	67 68	57. 2 58. 0	33-5	27	110.0	63.5	87 83	161.9	93-5	47 48	213. 9 214. 8	123. 5
,	6. 9 7. 8	40	69	58 9	34 0 34 5	28 29	110.9	64.0 64.5	80	162. 8 163. 7	94.0	49	214.0	124-0 124-5
10	8.7	5.0	70	58 g 59. 8 60. 6	35.0	30	112.6	65. o	90	164.5	95.0	50	216.5	125. 0
11	9.5	5. 5 6. 0	71	61.5	35· 5 36· 0	131	113.4	65. 5 66. 0	191	165. 4	95. 5 96. 0	251	217.4	125. 5
12 13	10.4	6.0	72	62 4 63. 2	36. 0 36. 5	32 33	114.3	66.5	92 93	166. 3	96.5	52 53	218.2	126.0
14	11. 3 12. 1	6. 5 7. 0	73 74	64.1	37. 0	34	115.2 116.0	67. 0	94	167. I 168. o	97.0	54	220.0	127. 0
15	13.0	7.5	75	650	37. 5 38. 0	35 36	116.9	67. 5 68. 0	95 96	168.9	97.5 98.0	55 56	220, 8	127. 5 128. 0
10	13.9	8.5	70	65 8 66 7	38. 0 38. 5	30	117.8	68.5	90 97	169. 7 170. 6	98.5	50	221. 7 222. 6	128.5
17 18	14. 7	9.0	77 78	67. 5 68 4	39.0	37 38	119.5	69.0	98	171.5	ە.وو	57 58	223.4	129.0
19	10.5	9.5	79		39-5	39	120.4	69.5	99	172. 3	99-5	59 60	224 3	129.5
20	17.3	10.0		69.3	40.0	40	121. 2 122. I	70.0	200	173. 2	100.0	261	225. 2 226. 0	130.0
21 22	10.2	10. 5 11 0	81 82	70 I 71.0	40. 5 41. 0	141 43	123. 1	70. 5 71. 0	201	174-1	100. 5	62	226. 9 227. 8	131.0
23	19.9	11.5	83	719	41.5	43	123.8	71.5	03	174-9 175-8 176-7	101.5	63	227. 8 228. 6	131.5
24	30.8	12. 0	84	72 7	42.0	44	124. 7 125. 6	72.0	04	176.7	102.0	64	228. 6 229. 5	132 O 132. 5
25 26	21. 7 22. 5	12. 5 13. 0	85 86	73 6 74 5	42. 5 43. 0	45	126.4	72-5 73-0	05 06	177.5	102. 5	65 66	230.4	133.0
27 28	23.4	13.5	87 88	75 3	43-5	47 48	127. 3	73-5	07 08	179.3	103.5	67 68	231.2	133.5
	24. 2	14.0	88		44.0	48	128. 2	74- 0		180, 1 181, 0	104.0	68	232. I 233. 0	134. 0 134. 5
39 30	25. 1 26. 0	14.5 15.0	89 90	77. 1 77. 9	44. 5 45. 0	49 50	129. 0 129. 9	74 5 75. 0	10	181.9	104. 5 105. 0	70	233.8	135.0
31	26. 8	15. 5 16. 0	91	78.8	45. 5 46. 0	151	130.8	75. 5 76. 0	211	182, 7 183. 6	105. 5	271	234.7	135.5
32	27. 7 28. 6	16.0	98	79 7 80.5	46.0	52	131.6	76.0	12	183.6	106.0	72	235.6 236.4	136. o 136. 5
33 34 35 36	28.0	16. 5 17. 0	93 94	80. 5 81.4	46. 5 47. 0	53 54	132. 5	76. 5 77. 0	13	184.5	106,5 107.0	73 74	230.4	137.0
35	30. 3	17.5	95 96	82. 3	47. 5 48. 0	55 56	134.8	77.5 78.0	15	185. 3 186. 2	107. 5	75 76	237. 3 238. 2	137. 5 138. 0
36	31.2	18. 0	96	83. I 84. O	48.0 48.5	56	135. I 136. O	78.0 78.5		187. 1	108.0	76	239.0	138.0
37 38	32. 0 12. 0	18. 5 19. 0	97 98	84.0	49.0	57 58	1 16, 8	79.0	17	187. 9 188. 8	109.0	77 78	239. 9 240. 8	139.0
39	32. 9 33. 8	19.5	99	85. 7 86. 6	49.5	59 60	137. 7 138. 6	79- 5 80- 0	19	189.7	109. 5	79	241.6	139. 5
40	34.6	20.0	100	86. 6	50.0			80.0	20	190.5	110.0	281	242.5	140.0
41 42	35· 5 36· 4	20. 5 21. 0	101	87. 5 88. 3	50. 5 51. 0	161 62	139. 4 140. 3	81.0	22 I 22	191.4	110.5	83	243. 4 244. 2	141.0
43	37. 2 38. I	21.5	03	89.2	51.5	63	141. 2	81.5	23	193. 1	111.5	83	245. I 246. O	141.5
44	38. 1	22. 0	04	90.'1	52.0	64	142.0	82. 0 82. 5	24	194.0	112. 0 112. 5	84	246. 8 246. 8	142. 0 142. 5
45 46	39. 0 39. 8	22. 5 23. 0	05	90. 9 91. 8	52. 5 53. 0	65 66	142. 9 143. 8	83.0	25 26	194.9	113.0	85 86	247.7	143.0
47	40. 7 41. 6	23.5	97 08	92. 7	53-5	67 68	144.6	83.5	27 28	195. 7 196. 6	113.5	87 88	248.5	143.5
48	41.6	24.0		93-5	54.0	68 69	145. 5 146. 4	84.0 84.5	28 29	197. 5 198. 3	114.0	88 80	249. 4 250. 3	144.0
49 50	42. 4 43. 3	24. 5 25. 0	10	94-4	54. 5 55. 0	70	147. 2	85. o	30	199. 2	115.0	90	251.1	145.0
51	44-2	25.5 20.0	111	96. I	55. 5 56. 0	171	148. I	85. 5 86. 0	231	200. I	115.5	291	252.0	145.5
52	45.0	26. Ó	12	97.0	56. o	72	149. 0 149. 8	86. o 86. s	32	200. 9 201. 8	116.0	9 8 93	252.9	146.0 146.5
됐	45.9 46.8	26. 5 27. 0	13	97.9	57.0	73 74	150.7	87.0	33 34	201. 6	117.0	94	253. 7 254. 6	147.0
55	47. 6 48. 5	27.5 28.0	15 16	97. 9 98. 7 99. 6	57. 5 58. o	75 76	151.6	87. 5 88. o	35 36	203.5	117.5	95 96	255.5	147.5 148.0
56	48. 5	28.0	16	100. 5	58. o 58. 5	76	152. 4 153. 3	88. o 88. 5	36	204. 4	118.0	90	256. 3	148.0
53 54 55 56 57 58	49- 4 50- 2	20.5	17	101. 3	59.0	77	153.3	89.0	37 38	205. 2 206. I	119.0	97 98	257. 2 258. I	149.0
59	51. 1	29.5	19	103. 1	59-5	79	155.0	89.5	39	207. 0	119.5	99	258. Q	149-5
60	52. 0	30.0	.20	103. 9	60.0	80	155. 9	90.0	40	207. 8	120. 0	300	259. 8	150.0
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.
												[F	or 60 Deg	rees.
1														

	D	IFFE	REN	CE O	F L	TIT	UDE	AND	DE	PART	URE	FOR	81°.	-
Dist.	Lat	Dep.	Dist.	Lat.	Dep.	Diet.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep
I	0.9	0.5	61	52. 3	31.4	121	103. 7	62. 3	181	155. 1	93. 2	241	206. 6	124. 1
3	I. 7 2. 6	1.0 1.5	62 63	53. I 54. 0	31.9. 32.4	22 23	104.6	62. 8 63. 3	82 83	156. 0 150. 9	93-7	42 43	207.4	124.6
4	3-4	2. 1	64	54.9	33.0	24	106. 3	63.9	84	157. 7 158. 6	94-3 94-8	44	209. 1	125. 7 126. 2
ş	4.3	2. 6 3. I	65 66	55. 7 56. 6	33- 5 34-0	25 26	107. 1	64.4	85 86	150.0	95. 3 95. 8	45 46	210. 0 210. 9	126. 7
7	5. î	3.6	67 68	57.4 58.3	34-5	27	108. 9	65.4	87	100.3	96. 3 96. 8	47 48	211. 7	127. 2
ै	6.9	41	69	50.3	35. O	28 29	109. 7 110. 6	65. 9 66. 4	88 80	161. I 162. 0	90. 8 97. 3	48 49	213.6	127. 7
10	7. 7 8. 6	5. 2	70	59. 1 60. 0	35. 5 36. 1	30	111.4	67.0	90	162.9	97-9	50	214.3	128. 8
II I2	9.4 10.3	5. 7 6. 2	71 72	60.9 61.7	36. 6 37. I	131	112. 3 113. 1	67. 5 68. o	191 92	163. 7 164. 6	98.4 98.9	251	215. 1 216. 0	129. 3 129. 8
13	11. 1	6:7	73	62.6	37.6 38.1	32 33	114.0	68.5	93	165.4	99-4	52 53	216. 9	1 130. 3
14	12. 0 12. 9	7.2	74	63.4 64.3	38. 1 38. 6	34	114.9	69.6	94	166. 3 167. 1	99.9 100.4	54	217. 7	130.8
15	13.7	7.7	75	65.1 66.0	39. 1	35 36	115. 7 116. 6	79.0	95 96	168. o	100.4	55 56	219.4	131.8
17		8.8	77	66.9	39-7	37	117.4 118.3	70.6	97 98	168. 9 169. 7	101.5	57	220. 3 221. 1	132.4
19	15.4 16.3	9.3 9.8	78	67. 7 68. 6	40. 2 40. 7	38 39	110. 3	71. 1	99	170.6	102. 5	58 59	221. 1	132. 9 133. 4
20	17. 1	10. 3			41.2	40	120. 0	72. 1	200	171.4	103.0	59 60	222.9	133.9
21 22	18.0	10.8	81 82	69.4. 70.3	41. 7 42. 2	141 42	120. 9 121. 7	72. 6 73. 1	201	172. 3 173. 1	103. 5 104. 0	261 62	223. 7 224. 6	134. 4 134. 9
23	19. 7	11. 3 11. 8	83	71.1	42. 7	43	122. 6	73-7	03	174.0	104.6	63	225. 4	135. 5
24 25	-20. 6 21. 4	12.4 12.9	84	72.0 72.9	43. 3 43. 8	44	123. 4 124. 3	74 2 74 7	04	174-9	105. 1	64	226. 3 227. 1	136. 0
26	22. 3	13.4	85 86	73. 7 74. 6	44-3 44-8	45 46	125. 1	75. 2	o6	175. 7	106.1	65 66	228.0	137.0
27 28	23. I 24. 0	13.9	87 88	74.6	44.8	47 48	126. 0 126. 0	75. 7 76. 2	% 8	177.4	106.6	67 68	228. 9 229. 7	137. 5 138. 0
20	24.9	14.4 14.9	89	75.4 76.3	45. 3 45. 8	49	127. 7	76.7	8	170. 3	107. 6	60	230.6	138.5
30	25. 7	15.5	90	77. 1	40.4	50	128.6	77.3	Ió	180. 0	108.2	70	231.4	139.1
31 32	26.6	16. o 16. 5	91	78. o 78. o	46. 9 47. 4	151 52	129. 4 130. 3	77.8 78.3 78.8	211 12	180.9	108. 7	271 72	232. 3 233. 1	139. 0 140. I
33	27. 4 28. 3	17.0	93	79.7 80.6	47.9 48.4	53	131. 1	78.8	13	181. 7 182. 6	109.7	73	234.0	140.6
34	29. I 30. 0	17. 5 18. 0	94 95	80. 6 81. 4	48.4 48.9	54	132. 0 132. 9	79. 3 79. 8 80. 3	14	183. 4 184. 3	110.2	74	234.9	141. 1 141. 6
35 36	30.9	18.5	96	82.3	49-4	55 56	133. 7	80.3	16	185. 1	111. 2	75	235. 7 236. 6	142. 2
37 38	31. 7 32. 6	19. I 19. 6	97 98	83. i 84. o	50.0	57 58	134.6	80.9	17 18	186. o 186. g	8 .111	77 78	237.4	142. 7
30	33.4	20. 1	99	8 i. o	50. 5 51. 0	59 60	135.4	81.4 81.9	19	187. 7	112.3	7°	238. 3 239. I	143. 2
40	34-3	20.6	100	85. 7	51.5		137. 1	82. 4	20	188.6	113.3	79 80	240, 0	144. 2
41 42	35. I 36. 0	21.1	101	86. 6 87. 4	52. 0 52. 5	161 62	138. o	82. 9 83. 4	221	189. 4 190. 3	113.8 114.3	281 82	240. 9 241. 7	144- 7 145- 2
43	36.9	22. I	03	87. 4 88. 3	53.0	63	139. 7 140. 6	84.0	23	191.1	114.9	83	242.6	144.8
44	37· 7 38. 6	22. 7 23. 2	3	89. i 90. o	53.6 54.1	6 <u>4</u>	140.6	84. 5 85. 0	24	192. 0 192. 9	115.4	84 8c	243. 4 244. 3	146. 3 146. 8
45 46	39-4	23.7	06	90.9	54.6	65 66	142. 3	85. 5 86. 0	26	193. 7	116.4	85 86	245. 1	147.3
47	40. 3 41. I	24.8 24.7	07 08	91. 7 92. 6	55. I	67 68	143. I 144. 0	86. o 86. s	27 28	194.6	116.9	87 88	246.0 246.9	147. 3 147. 8 148. 3 148. 8
49	42.0	25. 2	09	93.4	55. 6 56. 1	69	144.9	87.0	29	195. 4 196. 3	117.9	89	247. 7 248. 6	148.8
50	42.9	25.8	10	94-3	56. 7	70	145. 7	87.6 88.1	30	197. 1		90		149-4
51 52	43- 7 44- 6	26. 3 26. 8	111	95. 1 96. 0	57. 2 57. 7	171 72	146. 6 147. 4	88. i 88. 6	231 32	198. 0 198. 9	119.0	291 92	249. 4 250. 3	149. 9 150. 4
53	45· 4 46· 3	27. 3 27. 8	13	96.9	57· 7 58. 2	73	148.3	89. I	33	199. 7	120.0	93	251. 2	150.9
54	40.3	27. 8	14	97. 7 98. 6	58. 7 59. 2	74	149. I 150. 0	89.6 90.1	34	200. 6	120. 5 121. 0	94	252. 0 252. 9	151. 4 151. 9
55 56	47. I 48. o	28. 3 28. 8	16	99-4	59-7	75 76	150.9	90.6	35 36	202. 3	121.5	95 96	253. 7 254. 6	152. 5
57 58	48.9 49.7	29. 4 29. 9	17 18	100. 3 101. 1	60. 3 60. 8	77 78	151. 7 152. 6	91. 2 91. 7	37 38	203. I 204. 0	122. I 122. 6	97 98	254. 6 255. 4	153. 0 153. 5
59 60	50.6	30.4	19	102. 0	61.3	79 80	153.4	92.2	39	204.9	123. 1	99	256.3	154.0
60	51.4	10. O	20	102. g	61.8	8o i	154-3	92. 7	40	205. 7	123.6	300	257. 1	154.5

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	D	IFFE	ERE	NCE (F L	ATII	UDE	AND	DE	PART	URE	FOR	. 3 ? °.		
Dist.	I.at.	Dep.	Dist.	Lat	Dep.	Dist.	Lat	Dep.	Diet.	Lat	Dep.	Dist.	Lat.	Dep.	
1 2	a. 8 1. 7	0.5	61 62	51. 7 52. 6	32. 3 32. 9	121	102. 6 103. 5	64 I 64 7	181 82	153. 5 154. 3	95-9 94-4	241 42	204.4	127. 7	
3	2.5	1.6	62	53-4	33- 4	23	104.3	65. 2	82	155. 2 156. 0	97.0	43,	205. 2 205. 1 206. 9	128.8	
5	3.4 4.2	2.6	64 65 66	54-3 55-1 56-0	33- 9 34- 4	24 25 80	106. 2 106. 0	65. 7 66. 2	84 85 86	156. 9	97. 5 98. 0	44 45	200. 0 207. 8 208. 6	129. 3 129. 8	
Ž	5. 1 5. 9 6. 8	3.2 3.7	66 67 68	56.8	35.0	26 27 28	106. 9 107. 7 108. 6	66. 8	86 87 88	157 7 158 6	98.6 99.1	40 47 48	200.5	130.4	
8	6.8 7.6	4.8	68 69	57. 7 58. 5	35- 5 36. 6 36. 6	28 20	108.6	67. 3 67. 8 68. 4	88 89	159.4 160.3	99.6	48 49	210. 3	131.4 131.9	
10	7.6 8.5	5-3	70	59-4	37. 1	30	110. 8	68.9	90	161 1	100. 7	50	212. 0	132. 5	
12	9-3 10-2	6.4	71 72	60. 2 61. 1	37.6 38.2	131 32	111.1	69.4	191 92	16a. 8	101. 7	251 52	212.9	133. 0 133. 5	
13 14	12														
15 16	12. 7 13. 6	7.9 8.5	75 76	63.6 64.5	39-7	35 36	114.5		95 96	165. 4 166. 2	103. 3	55 56	216. 3 217 1	135. 1	
17	14.4	9.0	77	65.3 66.1	40. 3 40. 8	37 38	116.3	72.6	97 98	167. 1	104.4	57 58	217. 9	135. 7 136. 2 136. 7	
19	16. 1	9. 5 10. 1	78 79 80	67.0	41.3	39	117.0	73-1 73-7	99	167 9 168 8	104. 9 105. 5 100. 0	58 59	219.6	137. 2	
20 31	17. 0	10.6	80 81	67. 8	42. 4	40 141	118.7	74-2	200	169. 6 170. 5	106. 5	261	220. 5	137. 8	
32	17. 8 18. 7 19. 5	11.7	82	69.5	43.5	42	120.4	75. 2	03	171.3	107 0	6a 63	222. 2 223. 0	138.3 138.8 139.4	
23 24	20. 4	12. 7	83 84	70. 4 71. 2	44.0	43 44	121. 3 122. I	79.8 76.3 76.8	03 04	173.0	107.6	64	222.0	139.9	
25 26	21. 2	13. 2	85 86	72. I 72. Q	45. 0 45. 6	45 46	123. 0 123. 8	76.8	٠ <u>۶</u>	173.8 174.7	108.6	65 66	224. 7 225. 6 226. 4	140. 4 141. 0	
27 28	22. 9	14.3	87 88	72. 9 73. 8 74. 6	45. 6 46. I 46. 6	47 48	124.7	77.9	°7	175. 5 176. 4	109.7	67 68	226. 4 227. 3	141.5	
29	23. 7 24. 6	15.4	89	75- 5 76- 3	47. 2	49	125. 5 126. 4 127. 2	79.0	9	177. 2	110.8	69	228. I 229. 0	142.5	
30 31	25. 4 26. 3	16. 4	90 91	77.2 78.0	47.7	50 151	128, 1	79.5 80.0	211	178.9	111.8	70 271	229. 8	143. 6	
32 33	27. I 28. 0	17. 0	92 93	78. o 78. 9	48.8	52 53	128. 9 129. 8	80. 5 81. I	12	178. 9 179. 8 180. 6	112.3	72 73	230. 7 231. 5	144-1	
34	28. 8 29. 7	18. 5	94	79- 7 80. 6	49. 3 49. 8 50. 3	54	130.6	81.6 8a. 1	14	181. 5	113.4	74	232 4	145. 2	
35 36	30. 5	19. 1	95 96	81.4	50.9	55 56	131. 4 132. 3	82. 7	15	183. 2	114.5	75	234. I	145.7 146.3 146.8	
37 38	31. 4 32. 2	19.6 20.1	97 98	82. 3 83. 1	51.4 51.9	57 58	133. I 134. 0	83. 2 83. 7	17	184.0 184.9	115.0 115.5 116.1	77 78	234- 9 235- 8 236- 6	147. 3 147. 8	
39 40	33. I 33. 9	20. 7 21. 2	99	84.0 84.8	52. 5 53. 0	59	134. 8 135. 7	84. 3 84. 8	19	185. 7 186. 6	116.1	79	236. 6 237. 5	147.8	
41	24.8	21. 7	101	85. 7 86. 5	£1. £	161	136. 5		221	187. 4 188. 3	117. 1	281	238. 3	148. 9	
42 43	35. 6 36. 5	22. 3 22. 8	03	80. 5 87. 3 88. 2	54 6 55 1 55 6 56 2	62 63	137. 4 138. 2	85. 3 85. 8 86. 4	22 23	189. t	117.6	8a 83	239. I 240. 0	149. 4 150. 0	
44	37.3 38.2	23. 3 23. 8	04	80.0	55. I 55. 6	64	139. I	86.9 87.4	24	190.0	118.7	84	240. 8 241. 7	150. 5 151. 0	
45 46	39. 0 39. 9	24. 4 24. 9	95 86	89.0	56. 2 56. 7	65 66	139. 9 140. 8 141. 6	88. o 88. s	25 26	191. 7 192. 5	119.8	85 86 87	242. 5 243. 4	151.6	
47	40. 7 41. 6	25.4	97 98	90. 7 91. 6	67 2	67 68	142. 5	89.0	27 28	193.4	120. 3 120. 8	87 88	344-3	152.6	
49 50	41, 0 42, 4	26.5	10	92. 4 93. 3	57. 8 58. 3	69 70	143. 3 144. 2	89. 6 90. I	29 30	194. 2 195. 1	121.4 121.9	89 90	245. I 245. 9	153. 1 153. 7	
51 52	43-3 44-1	27. 0 27. 6	111	94. I 95. 0	58. 8 59. 4	171	145. 0 145. 9	90. 6 91. I	231 32	195. 9 196. 7	122. 4	291 92	246. 8	154-2- 154-7	
53	44.9	27. 6 28 1 28. 6	13	95. 8 96. 7	59.9 60.4	73	146. 7	91. 7	33	197.6	123.5	93	247.6 248.5	155.3	
54 55 56	46.6	29. I	14 15 16	90. 7 97: 5 98. 4	60.0	74 75 76	145.4	92. 2 92. 7	34 35 36	199-3	124.0 124.5	94 95 96	249. 3 250. 2	1166.2	
56 57	47. 5 48. 3	29. 7 30. 2	16	98.4	61.5 62.0	76 77	149. 3 150. I	93. 3 93. 8	36 37	200, I 201 0	125. 1	96 97	251. Q 251. Q	156. 9 157. 4	
57 58	49. 2 50. 0	30. 7	17 18 19	100. I	62. 5 63. 1	77 78	151.0	94.3	37 38 39	201. 8 202. 7	126. I 126. 7	97 98 99	252. 7 253. 6	157. 9 158. 4	
8	50.9	31. 3 31. 8	20	100. 9 101. 8	63.6	79	152.6	95.4	39 40	203. 5	127. 2	300	254 4	159.0	
Dist.	Dep.	Let.	Dist.	Dop.	Let	Dist.	Dep.	Lat	Dist.	Dep.	Lat.	Dist	Dep.	Lat.	
												[F	or 58 Deg	7005.	

DIFFERENCE OF LATITUDE AND DEPARTURE FOR 83°.

Dist.	Let.	Dep.	Dist.	Let.	Dep.	Dist.	Let	Dop.	Dist.	Let.	Dep.	Dist.	Lest.	- Dep.
1	0.8	0.5	6t	51. 2	33. 2	121	tot. 5	65.9 66.4	181	151. 8	98.6	941	sos. 1	131. 3 131. 8
	1.7 2.5	1.1	62	52. 0 52. 8	33.8	83 83	102. 3 103. 2	67.0	82 82	152. 6 153. 5	99- I 99- 7 100- 2	43	903. 0 903. 8	131. B 132. 3
3 4	3-4	2.2	4	52.7	34.9	24	104.0	67. 5 68. 1	84	104.3	100. 2	4	204.6	132.0
ş	4.2 5.0 5.9 0.7	2.7	28.83	54-5 55-4 56-8	35-4	25	104.8	68.6	బెచికుడ	155. 8 156. 0	100.8	848444	805. 5 800. 3	133-4
7	Ş-9	3. 3 3. 8	67	55-4 50.2	36.5	7	105. 7 106. 5	69.2	87 88	146.8	101. 3 101. 8	47	207. S	134.0 134.5 135.1
9	6.7	44	68	57.0	34-3 34-9 35-4 35-9 30-5 37-6 38-1	98 20	107. 3 108. 2	69.7	\$28 80	157. 7 158. 5	108. 4 108. 9	49	208. o 208. 8	135.1
10	5-7 7-5 8-4	5.4	76	57. 0 57. 9 58. 7	38. 1	30	100.0	69.2 69.7 70.3 70.8	gó	159.3	103. 5	50	209. 7	130. 8
11 12	9. 2 10. I	6.0	71	59.5 60.4	38.7 39.2	131	109. 9 110. 7 111. 5 112. 4	71. 2	191	160. 2 161. 0	104.0 104.6	5883555588	210. 5	136.7
13	10.9	6.5 7.1 7.6	72 73	61.2	20.8	32 33	111.5	7L 9 72.4 73.0	93	161 6	105.1	1 %	311. 3 912. 3 813. 0	137. 8
انقا	10.9 11.7 12.6	7.6	74 75 70	62. 1 62. 9	40.8	34	112.4	73.0	33 4 57 8 57 8	168. 7 163. 5	105. 7 100. 2	54	813.0	138.3
15	12.4	8.7	1 73	62.7	AUA	34 55 56	113. 2 114. I	73.5	22	104.4	106 7	器	313.9 814.7	138.9
17	14.3 15.1 15.9 16.8	9.3	77	64.6	41.9	37 38	114.0	74.6	97 98	164-4 165-8 166-1	107. 3 107. 8 108. 4	57	215.5	140.0
10	15. 1	10.5	70	65.4 66.3	42.5	35	115. 7	75.2	95	100. 1	107.8	8	810.4	140.5
26	16. 8	9.3 9.8 10.3 10.9	20	67. 1	41.9 42.5 43.6	40	117.4	74 6 75 2 75 7 76 2	90	167. 7	105.9		213-9 214-7 215-5 210-4 217-2 218-1	140.0 140.5 141.1 141.6
21 22	17.6 18.5	11.4 12.0	81 82	67. 9 68. 8	44.1 44.7 45.2	141	118.3 119.1 119.9 120.8	76.8	201	168.6	109. 5 110. 0	251 62	318.0	142.3
23	18. 5 19. 3 20. 1	12.5		69.6	45.2	43	119.9	77.3 77.9	03	169. 4 170. 3	110.6	63	219. 7 220. 6	143.3
1 24	19. 3 20. I	121	4	69.6 70.4 71.3	45.7	44	120. 8 121. 6	78.4	04	170. 3 171. I	111. 1	9	221. 4 222. 3	143.8
25	21.0 21.8	13.6 14.8	3453	71. 3 72. I	45.7 44.8 44.8	45	124.4	79.0	95 86	171.9	111.7	1 2	#3, I	144.9
27 28	22.6	147	87 88		47.4	3	123. 3	20. 5 80. 1	97 98	173.6	110.6 111.1 111.7 112.7	9	883. Q	144.4
20	23. 5 24. 3 25. 2	1 12 8	89	73.8 73.8 74.6	47.9 48.5	49	124. I	80. 6 81. 2	08	174-4	113. 3 113. 8	8	224.8	14Å.0
30	25. 2	14.7 15.2 15.8 16.3	90	75-5	49.0	50	125. 0 125. 8	81. 7	10	174-4 175-3 176-1	1144	5488888	200.4	147. 1
31 32	20.0 26.8	16.9	91 92	7.77 10 8 70 70 8	49.6 50.1 50.7 51.8	151 52	126. 6 127. 5	82. 2 82. 8	311	177.0	114-9 115-5 110-0	# 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	287. 3 258. I	147. 6 148. 1
33 34 35 36	27. 7 28. 5	17.4	93	77.2 76.0 76.8	50.7 51.8	53	128.3	83.3	iš	177. 8 178. 6	115.5	73	880.0	148.7
34	28. 5 29. 4	18.5 19.1	94 95 96		Š1. ž	54	189. 2	83. 3 83. 9 84. 4.	14	1 179-5	116.6	2	239.8 230.6	149. 8 149. 8
33	30. 3	19.6	1 23	79.7 80.5	51. 7 52. 3 52. 8	꿇	130.0	84.0	15	181. 3	117.6	1 %	831. S	150. 3 150. 9
37 38 39	11.0	20.2	97 98	81.4	52.8	335858888	131.7	85. 0 85. 5 86. 1	17	18s. o 18s. 8	117. 1 117. 6 118. s 118. 7	7	832. 3 833. 8	150.9
30	31.9 32.7 33.5	20. 7 21. 2	99	82. s 83. o	53- 4 53- 9	1 %	132. 5 133. 3	86.6	10	183. 7	110.7	%°.	814.0	151. 4 152. 0
L 40 I		31.8	100	83.9	1 34 5		134.2	87. 1	8	184.5	119.3 119.8		234.8	152. 5
41 42	34-4 35-2 36-1	22. 3 26. 0	IOI	84.7 85.5	55.0 55.6 56.1 56.6	161 62	135.0	87. 7 88. a	221 22	18¢. 3 186. 2	190. 4 190. 9	251 88 87 84 87 86 87 88	935- 7 936- 5 837- 3	153. 0 153. 6.
		23.4	03	I 86.∡	56. i 56. 6	63	135.9 136.7	I 88.8	83	187.0	121. 5	83	#37: 3 #38. #	154 1 154 7 155 8 156 3 156 9
43 44 45 46	36.9	84.0	2	87. s 88. i	56.6 57.8	8.8.8	137. 5 138. 4	89. 3 89. 9	24	187. 9 188. 7	123. 0 123. 5	1 5	23K. 2	154.7
3	37. Ž	85. Î	3	88. o	57.7	66	130.8	90.4	25 26	189.5	123, I	8	230.0	155.8
47	39- 4 40- 3	25.6 20.1	3Z	89. 7 90. 6	57. 7 58. 3 58. 8	67	140.1 140.9	91.0	27 28	190. 4 191. 2	123. 6 124. 8	2	240. 7 241. 5	156.3
47 48 49 50	41. I	96.7	9	O 1. 4	50.4	69	141. 7 142. 6	91. 5 92. 0 92. 6	30	IQS. I	124.7	1 89	242. %	157. 4
	41.9	27. 2	10	98.3	59-9	70		92.6		198.9	125. 3	90	243. 2	157. 9
;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;	42.8 43.6	27.8 28.3 28.9 29.4	111	93. I 93. 9	61.0	171	143-4	93: 1 93: 7 94: 2 94: 8 95: 3	231 32	193. 7	125. 8 126. 4 126. 9	991 98	841 I	120.0
53	44.4	28.9	13	93-9 94-8 95-6	i 61. 5	73	MEI	94.2	33	195. 4 196. 8	126. 9	es	845. 7 845. 6	159.6
	44.4 45.3	89.4 30.0	14	95.6 96.4	62.1	74	145. 9 146. 8	94.5	33 34 35 36	190. 2	127. 4 128. 0	\$ 55 B	847. 4	159. 6 160. 1 160. 7
56	47. 0	30.5	15	97. 3 98. 1	63.2	%	147.6	95.9	36	197. 9	128. C	ρõ	847. 4 848. 8	
IJ	47. 8 48. 6	31.0 31.6	17	98.1	63.7	74	149.3	95.9 96.4 96.9	37 38	198.8	189. I 129. 6	97 98	249. I 249. Q	161. 8 162. 3 169. 8
99	49-5	38. I	.19	99.8		777477777878	تحفدا	96.9 97.5 98.0	39	800.4	130. 2	90	aco k	16g. 8
<u>~</u>	50. 3	39. 7	20	foor e	65.4	80	151.0	98.0	40	201. 3	130. 7	300	\$51.6	163. 4
Diet.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat	Dist.	Dep.	Lat.	Dist.	Dop.	Let.
												[F	or 57 Deg	7000.

DIFFERENCE OF LATITUDE AND DEPARTURE FOR 34°.

Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Let	Dep.	Dist.	Lat	Dep.
<u> </u>	0.8	0.6	61	50.6	<u> </u>	121	100 4	4	181			-		
2	1.7	1.1	62	51.4	34 I 34 7	22	100. 3 101. 1	67. 7 68. 2	82	150. I 150. 9	101. 2 101. 8	241 43	199. 8 200. 6	134.8 135.3
3	2.5	1.7	63 64	52. 2	35. 2	23	102. 0	68.8	83	151. 7	102. 3	43	201.5	135.0
\$	3.3 4.1	2.8	65	53. I 53. 9	35.8 36.3	24 25	103.6	69.3 69.0	84 85 86	152. 5 153. 4	102. 9	44	202. 3	130.4 137.0
	5. 8 5. 8 6. 6	3.4	66	54-7	26.0	25 26	104.5	69.9 70.5	86	154.2	104.0	45 46	203.9	137.6
3	6.6	3.9. 4.5	67	55. 5 56. 4	37. 5 38. 0	27 28	105.3	71. 0 71. 6	87 88	155.0	104. 6 105. I	47 48	204. 8	138. 1 138. 7
9	7· 5	5. o 5. 6	69	57.2 58.0	38.6	29	106.9	72. 1	89	155.9 156.7	105. 7	49	206.4	130.2
10		6.2	70	58.0	39. 1	_30	107.8	72.7	90	157.5	100. 2	50	207.3	139.8
12	9. I 9. 9	6.7	71 72	58.9 59.7	39-7 40-3	131 32	108.0	73-3 73-8	191 92	158.3	106.8	251 52	205. I 208. 0	140. 4 140. 9
13	10.8	7.3 7.8 8.4	73	59. 7 60. 5	40.8	33	110.3	74-4	93 94	159. 2 160. 0	107.9	53 54	209. 7 210. 6	141.5
14	11. 6 12. 4	[74 75	61. 3 62. 2	41.4 41.9	34	111.1	74-9 75-5	2	160. 8 161. 7	108.5	54	210. b	142.0 142.6
15	13. 3 14. 1	1 8.Q	75 76	63. 0 63. 8	42. 5	35 36	112. 7 113. 6	75.5 70.1 76.6	95 96	162. 5	109.6	55 56	212.2	143. 2
17	14.1	9. Š	77	63.8	43. I 43. 6	37 38	113.6	76.6	97 98	163. 3 164. 1	110.2	57 58	213.1	143-7
19	14.9 15.8 16.6	10.6	79	65. 5	44.2	39	115.2	77. 7	90	165.0		8	213.9	144- 3 144- 8
20	16.6	11.2		65. 5 66. 3	44.7	40	115. 2 116. 1	77. 7 78. 3	99 200	165.8	111.8	\$9 60	215.5	145. 4
21 22	17.4 18.2	11.7	81 82	67. 2 68. o	45.3	141 42	116.9	78.8	201	166.6	112.4	261 62	216.4	145. 9 146. 5
23	19. I	12. 9	83	68.8	45. 9 46. 4	43	117.7	79.4 80.0	03	167. 5 168. 3	113.5	62	217. 2 218. 0	147. X
24	19.9	13.4 14.0	84	69.6 70.5	47.0	44	119.4	80. 5 81. 1	04	169.1	114.1	1 64	218.9	147.6 148.8
25 26	20. 7 21. 6	14.5	85 86	71.5	47. 5 48. 1	45 46	120. 2 121. 0	81.6	95 86	170.0	114.6	65	219.7 220.5	148.7
27 28	22. 4	15.1	87 88	72. I	48.6	47 48	121.9	82. 2	97 98	171.6	115. 2 115. 8 116. 3 116. 9	67 68	221.4	149-3
20	23. 2 24. 0	15.7	80	73.0 73.8	49. 2 49. 8	48	122. 7 123. 5	82. 8 83. 3	08	172.4 173.3	116.3	69	222. 2 223. 0	149.9 150.4
30	24.9	16.8	90	74.6	50. 3	50	124.4	82.0	16	174. 1	117.4	70	223.8	151.0
31 32	25. 7 26. 5	17.3	9r	75· 4 76· 3	50.9	151	125. 2 126. 0	84.4	211	174.9 175.8	118.0	271	224. 7	151.5
33	27.4	17.9	92 93	70. 3 77. I	51.4 52.0	52 53	126.8		13	175.8	118.5	72 73	225. 5 226. 3	152. I 152. 7
34	27. 4 28. 2	19.6 19.6	O4	77. 9 78. 8	52.6	54	127. 7	85. 6 86. 1	14	177-4	119.7	74	227. 2	152.2
35 36	29.0 29.8	19.0 20.1	95 95	78.8	53. I 53. 7	55 56	128. 5 129. 3	86. 7 87. 2	15 16	178.2	120. 2	74 75 76	228. 0 228. 8	153. 8 154. 3
37 38	30. 7	20. 7	97 98	79.6 80.4	E4. 2	57 58	130.2	87.8	17	179.9	121.3	77	220.6	154.0
38	31. 5 32. 3	21. 2 21. 8	98 99	81. 2 82. 1	54. 8 55. 4	58	131.0	88.4 88.9	18	179.9 180.7 181.6	121.9	7 ⁸	230. 5 231. 3	155. 5 156. 0
40	33. 2	22.4	100	82.9	55.9	59 60	132.6	89.5	20	182.4	123.0	72	232.1	156.6
41	34-0	22. 9	101	83. 7 84. 6	£6. 5	161	133.5	90.0	221	183. 2	123.6	281	233.0	157. 1
42 43	34. 8 35. 6	23. 5 24. 0	02 03	85.4	57.0 57.6 58.2	62 63	134.3	90. 6 91. 1	22 23	184.0 184.9	124.1	82 83	233.8 234.6	157. 7 158. 3
انتفا	35. 6 36. 5	24.6	اندها	85.4 86.2	58.2	64 I	135. 1 136. 0	91.7	24	185. 7 186. 5	125.3	1 Sá	235. 4 236. 3	158.8
45	37· 3 38. 1	25. 2	95 96	87. o	58. 7	65 66	126.8	92. 3	25 26	186.5	125.8	85 86	236. 3 237. 1	159-4 159-9
47	39.0	25. 7 20. 3 26. 8	97	87. 9 88. 7	59.8 59.4	67 68	137.6° 138.4	93.4	27 28	187.4 188.2	125. 3 125. 8 126. 4 126. 9	87 88	237.9	160.5
48 49	39.8 40.6	26.8	08 09	88. 7 89. 5 90. 4	60.4	68 60	139. 3 140. 1	93.9	28 29	189. 0 189. 8	127. 5 128. I	88 89	237. 9 238. 8	161. ŏ
50	41.5	27.4 28.0	10	91.2	61.5	70	140.1	94. 5 95. I	30	190.7	128. 6	, 29 90	239. 6 240. 4	161.6 162.2
51	42. 3	28.5	111	92. 0	62. I	171	141.8	95. 6 95. 2	231	191.5	129. 2	291	241. 2	162. 7
52 53	43. 1	29. I 29. 6	12 13	92. 9 93. 7	62. 6 63. 2	72 73	142. 6 143. 4	95. 2 96. 7	32	192. 3	130. 3	92 93	242. I 242. 9	163. 3 163. 8
54	44.8	30.2	14	94.5	03.7	74	144.3	97.3	34	194.0	130.3	94	243.7	104.4
53 54 55 56 57 58	43.9 44.8 45.6 46.4	30.8	15	95. 3 96. 2	64.3	75 76	145.1	97.9	33 34 35 36 37 38	104.8	131.4	94 95 96	244.6	165.0
57	47.3 48.1	31.9	17	97.0	65.4 66.0	77	145. 9 146. 7	99.0	37	195. 7 196. 5	132.0 132.5	97	245.4 246.2	165. 5 166. I
58	48.1 48.9	32.4		97.8	66. 6	77	147. 6 148. 4	99-5	38	197. 3 198. 1	133. I	97 93	247. I	1 *66 6 1
80	49.7	33. 0 33. 6	19 20	98.7 99.5	67. 1	79 80	148. 4 149. 2	100. I 100. 7	39 40	198.1	133.6 134.2	300	247.9 248.7	167. 2 167. 8
Dist.	Dep.	Lat	Dist.	Dep.	Lat.	Dist,	Dep.	Lat.	Diet.	Dep.	Let.	Dist.	Dep.	Lat.
· ·												[Fo	56 Deg	rees.

DIFFERENCE OF LATITUDE AND DEPARTURE FOR 35°.

<u> </u>		,			_					·				
Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	0.8	0.6	61	50.0	35. 0	121	99. I	69.4	181	148. 3	103.8	241	197.4	138. 2
2	1.6	1.1	62	50.8	35. 6	22	99. 9 100. 8	70.0	82	149. 1	104.4	42	198. 2	138.8
3	2. 5	1.7	63	51.6	36. 1 36. 7	23	100. 8	70. 5	83 84	149.9	105.0	43	199.1	139-4
4	3.3 4.1	2.3	64	52. 4 53. 2	37.3	24 25	102.4	71.1	82	150. 7 151. 5	105. 5	44	199. 9 200. 7	140.0
ş	4.9	3.4	65	54. I	37.9	26	103. 2	72. 3	85 86	152.4	106. 7	45 46	201.5	141.1
7	5. 7 6. 6	40	67	54.9	38. 4	27 28	104.0	72. 3 72. 8	87 88	153. 2	107. 3 107. 8	47 48	202. 3	141.7
	6.6	4.6	68	55. 7 56. 5	39.0		104.9	73-4		154.0	107.8		203. I	142.2
9	7. 4 8. 2	5.2	69	56. 5	39.6	29	105. 7	74.0	89	154.8	108.4	49	204.0	142.8
10		5.7	70	57-3	40. 2	30	106. 5	74.6	90	155.6	109.0	50	204.8	143.4
11	9. 0 9. 8	6. g	71 72	58. 2 59. 0	40. 7 41. 3	131 32	107. 3 108. I	75. 1	191 92	156.5	109.6	25I 52	205.6	144-0 144-5
13	10.6	7.5	73	59.8	41.9	33	108.0	75. 7 76. 3	93	157. 3 158. 1	110.7	53		145.1
14	11.5	7. 5 8. o	74	60.6	42.4	34	108. 9 109. 8	76.9	94	158. Q	111.3	54	207. 2 208. I	145.7
15	12. 3	8.6	75 76	61.4	43.0	35 36	110.6	77.4	95 96	159. 7	111.8	55 56	208.9	145.7 146.3 146.8
	13. i	9.2	76	62. 3	43.6	36	111.4	78.0	96	160.6	112.4	56	209. 7	146.8
17 18	13.9	9.8 10.3	77 78	63. i 63. g	44. 2 44. 7	37 38	112.2	78.6	97 98	161.4	113.0	57 58	210.5	147.4 148.0
19	14. 7 15. 6	10.9	70	64.7	45.3	39	113.0	79. 7	99	163.0	113.6	59	212. 2	148.6
20	16.4	11.5	79 80	65.5	45.9	40	114.7	79. 7 80. 3	200	163.8	114.7	66	213.0	149. I
21	17. 2 18. 0	12.0	81	66. 4	46.5	141	115.5	80.9	201	164.6	115. 3	261	213.8	149-7
22	18. 0	12.6	82	67. 2 68. o	47.0	42	116.3	81.4	02	165. 5 166. 3	115.9	62	214.6	150. 3
23	18.8	13. 2	83 84	68. o 68. 8	47. 6 48. 2	43	117. 1	82.0	03	166. 3	116.4	63	215.4	150.9
24 25	19. 7 20. 5	13.8 14.3	85 85	69.6	48.8	44	118.0	82. 6 83. 2	04	167. 1 167. 9	117.0	64	216. 3 217. I	151.4
28	21.3	14.9	86	70.4	49. 3	45 46	119.6	83.7	05 06	168. 7	118.2	65 66	217.9	152.6
27	22. I	15. 5	87 88	71.3	49.9	47	120.4	84.3	% 8	169.6	118.7	67	218.7	153.1
28	22. 9 23. 8	16. 1		72. 1	50. 5	47 48	121.2	1 8a.o.		170.4	119.3	68	219.5	153. 7
29	23.8	16.6	89	72. 9	51.0	49	132. 1	85. ś	09	171.2	119.9	69	220.4	154.3
30	24.6	17.2	90	73- 7	51.6	50	122. 9	86. o	10	172.0	120.5	70	221.2	154.9
31	25. 4 26. 2	17. 8 18. 4	91 92	74-5	52. 2 52. 8	151 52	123. 7 124. 5	87.2	211 12	172. 8	121.0	271 72	222. 0 222. 8	155.4 156.0
32 33	27. 0	18.9	93	75. 4 76. 2	53-3	53	125.3	87.8	13	174.5	122. 2	73	223.6	156.6
34	27. 9 28. 7	19. 5	94	77.0	53.9	54	126. 1	I 88. ₹	14	175.3	122. 7	74	224.4	157. 2
35 36	28. 7	20. 1	95 96	77.8	54-5	55 56	127.0	88. 9	15 16	176.1	123. 3	75	225. 3	157. 7 158. 3
36	29.5	20.6	96	78.6	55. 1	50	127.8	89.5	10	176. 9 177. 8	123.9	70	226. I 226. Q	158. 3 158. 9
37 38	30. 3 31. I	21.8	97 98	79. 5 80. 3	55. 6 56. 2	57 58	129.4	90.1	17	178.6	124.5	77	227. 7	159.5
39	21.0	22. 4	99	81.1	56.8	50	130.2	91.2	19	179.4	125.6		228.5	160.0
40	32. 8	22.9	Ióó	81.9	57-4	59 60	131.1	91.8	20	180. 2	126. 2	79 80	229.4	160.6
41	33.6	23. 5	101	82. 7	57. 9 58. 5	161	131.9	92. 3	221	181.0	126.8	281	230. 2	161.2
43	34 4	24. 1	02	83.6	58. 5	62	132. 7	92.9	22	181.9	127. 3	82	231.0	161.7
43	35. 2 36. 0	24.7	03 04	84.4	59. 1	63 64	133.5	93- 5	23	182. 7 183. 5	127. 9	83 84	231.8	162. 3 162. 9
44	36. g	25. 2 25. 8	05	85. 2 86. o	59. 7 60. 2	65	134-3 135-2	94. I 94. 6	24	184.3	120.5	8	233.5	163.5
45 46	37. 7	26.4	05 06	86.8	60.8	65 66	1 16.0	95.2	25 26	1 184. I	129.6	85 86	234.3	164.0
47 48	37. 7 38. 5	27.0	97 08	87. 6 88. 5	61.4	67 68	136.8	95.8	27 28	185. 9 186. 8	130.2	87 88	235. 1	164.6
48	39-3	27. 5 28. 1		88. 5	61.9		137.6	96.4		186.8	130.8	88	235.9	165. 2
49 50	40. I 41. 0	28. 7	09 10	89. 3 90. 1	62. <u>5</u> 63. I	70	138.4 139.3	96. 9 97. 5	29 30	187.6	131.3	89 90	236. 7 237. 6	165.8 166.3
51	41.8		111	90.9	63. 7	171	140.1	98.1	231	189. 2	132.5	291	238.4	166. o
52	42.6	29. 3 29. 8	12	91.7	64. 2	72	140.9	98.7	32	190.0	133.1	92	239.2	167. 5 168. 1
53	43-4	30.4	13	92.6	64.8	73	141.7	99.2	33	190.9	133.6	93	240.0	168. 1
54	44. 2	31.0	14	93-4	65. 4 66. 0	74	142. 5	99.8	34	191. 7	134.2	94	240.8	168.6 169.2
54 55 56	45.1	31. 5 32. 1	15	94.2	66.5	75 76	143.4	100. 4 T00. 9	35 36	192. 5	134.8	95 96	241.6 242.5	169. 8
37	45. 9 46. 7	32. 7		95. 0	67. 1	77	144. 2 145. 0	101.5	37	193. 3 194. I	135.4	1 67	243.3	170.4
57 58	47.5	33.3	18	96.7	67. 7	77 78	145.8	102. 1	37 38	195.0	1 36. 5	97 98	244.1	170.9
59	47. 5 48. 3	33. 3 33. 8	19	97. 5 98. 3	68. 3 68. 8	79	146.6	102. 7	39	195.8	137. 1	99	244.9	171.5
60	49. I	34-4	20	98. 3	68. 8	80	147-4	103. 2	40	196.6	137-7	300	245· 7	172. 1
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.
				•								[Fo	r 55 Deg	rees.

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DIFFERENCE OF LATITUDE AND DEPARTURE FOR 36°. Depart Lat. Dep. Dist. Dep. Dist. Lat. Dep. Dist. Lat. Dep. Dist. Dep.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	
Dist. Lat. Dop. Dist. Dist	39 80	47.7 48.5			95. 5 96. 3 97. 1	69.9	79		104. 0 105. 2 105. 8	39 40	193.4	140.5	99 300	241. 1 241. 9 242. 7		
Dist. Lat. Dop. Dist. Lat. Dist. Dis	56 57		32. 9 33. 5		93. 8	68.8	76 77	142.4 143.2	104.0	36 37	191. 7	138. 7	96 97	239. 5	174.0 174.6	
Dist. Lat. Dop. Dist. Lat. Dist. Dis	\$4 55	43-7	31. 7 38. 3	14	93.0	67.0	74	141.6	102.9	34 35	189. 3 190. I	137. 5 138. 1	94 95		173-4	
Dist. Lat. Dop. Dist. Dist. Dist. Dist. Dist. Dist.	52	48.9	30. 6 31. 2	13	91.4	65. 8 66. 4	73	139. 2	101. 7	32	187. 7 188. 5	137.0	92 93	237. 0	172. 2	
Dist. Lat. Dep. Dist.	51		20.0	111	89.8	64. 7 65. 2	171	138.3	99-9	231	186. o	135. 2	201	234. 6 235. 4	171.0	
Dist. Lat. Dep. Dist.	49	39.6	25. 8	09	88. 2	64. I	69	135.9	99-3	29	185.3	134.6	89	211. 8	169.9	
Dist. Lat. Dep. Dist.	47	37. 2 38. 0	27. 6	97	86.6	62.0	67	135.1	08.2	27	182.6	133. 4	87	212. 2	168. 7	
Dist. Lat. Dep. Dist.	45	36.4	23.5		84.9	61. 7	65	133.5	97.0	25	182.0	132. 3	85	230.6	167. 3	
Dist. Lat. Dep. Dist.	43	34.0	25. 3	Qg .	83.3	60. 5	63	121.0	95.8	23	180.4	131. 1	83	229.0	166.0	
Dist. Lat. Dep. Dist.	41	22.2	24. I		81. 7 82. E		161	130. 3	01.6		178.8			227. 3 228. I	164. 2	
Dist. Lat. Dop. Dist. Dist. Dist. Dop. Dist. Dis	39 i	31. 6 32. 4	22. 9	99	80.9	58. 2 58. 8	59 60	129.4	93.5	19	177. 2 178. 0	128.7	22	225. 7 226. 5	164.6	
Dist. Lat. Dop. Dist.	37 38	29.9 30.7	22. 3	97 98	78.5	57.0	57 58	127. 0	92.9	17	176.4	127. 5 128. 1	77	224. I 224. 0	163.4	
Dist. Lat. Dop. Dist.	35 36	29. I		95	76.9	55.8	55	125. 4 126. 2	91.7	15	173.9 174.7	127.0	75 76	223. 3	162. 2	
Diet. Lat. Dop. Diet. Diet. Diet. Dop. Diet. Diet. Dop. Diet. Lat. Dop. Diet. Lat. Dop. Diet. Diet. Dop. Diet. Diet. Dop. Diet. Diet. Dop. Diet. Diet. Dop. Diet. Diet. Dop. Diet. Diet. D	33 34	26. 7 27. 5	20.0	04	75.2	54- 7 55- 3	53 54	124.6	90.5	14	173.1	125. 2	73	221. 7	161.1	
Dist. Lat. Dep. Dist. Dist	32	25. I 25. 9	18.8	92	74.4	53- 5 54- 1	52	122.0	88.8	12	171.5	124.6	72	220. 1		
Dist. Lat. Dep. Dist. Dep. Dist. Dis	30	24.3	17.6	90	72.8	52. 9	50	131. 4		10	169.9	123.4	70		158.7	
Dist. Lat. Dop. Dist.		22. 7	16.5		71.2	51.7		119.7	87.0		168. 3	122. 3	68	216.8	157.5	
Dist. Lat. Dep. Dist. Di	20	24 19, 4 14, 1 84 68, 0 49, 4 44 116, 5 84, 6 04 165, 0 119, 9 64 1313, 6 155, 2 85 28, 2 14, 7 85, 6 8, 8 50, 0 45 119, 3 85, 2 05 165, 8 120, 5 65 1814, 4 155, 8 20 21, 0 15, 3 85 69, 6 50, 5 45 118, 1 85, 8 05 165, 7 121, 1 65 1812, 2 155, 4 27 21, 8 15, 0 8 150, 8 7 121, 1 65 1812, 2 155, 4 127 21, 8 15, 0 8 5, 2 7 18, 1 5, 0 8 7 18, 1 15, 0 8 7 18, 2 155, 4 18, 2 1														
Dist. Lat. Dep. Dist. Di	24	23 18.6 13.5 83 67.1 48.8 43 115.7 84.1 03 164.2 119.3 63 212.8 154.6 24 19.4 14.1 84 68.0 49.4 4 116.5 84.6 04 165.0 119.9 64 213.6 155.2 25 20.2 14.7 85 68.8 50.0 45 117.3 85.2 05 165.8 120.5 65 214.4 155.8														
Dist. Lat. Dop. Dist. Dop. Dist. Lat. Dop. Dist. Lat. Dop. Dist. Lat. Dop. Dist. Dis	£2	21 17.0 12.3 81 65.5 47.6 141 114.1 82.9 201 162.6 118.1 261 211.2 153.4 22 17.8 12.9 82 65.3 48.2 42 114.9 85.5 02 165.4 118.7 62 212.0 154.0 12.0 154.0 12.0 154.0 12.0 154.0 12.0 154.0 12.0 154.0 12.0 154.0 12.0 154.0 12.0 154.0 12.0 154.0 12.0 154.0 12.0 154.0 12.0 154.0 154.0 154.0 155.0 1														
Dist. Lat. Dep. Dist. Dist. Dist. Dist. Dist. Dep. Dist. Dis	20	20 16.2 11.8 80 64.7 47.0 40 113.3 82.3 200 161.8 117.6 60 210.3 152.8 21 17.0 12.3 81 65.5 47.6 141 114.1 82.9 20 162.6 118.1 261 211.2 153.4 22 17.8 12.9 82 66.3 48.2 42 114.9 83.5 02 163.4 118.7 62 212.0 154.0														
Dist. Lat. Dop. Dist. Dist. Dist. Dist. Dist. Dop. Dist. Dis		19 15.4 11.2 79 03.9 40.4 39 112.5 81.7 99 101.0 117.0 59 209.5 152.2 20 10.2 11.8 80 64.7 47.0 40 113.3 82.3 200 101.8 117.0 60 210.3 152.8 21 17.0 12.2 81 65.5 47.6 141 14.1 82.0 201 102.6 118.1 201 211.2 152.4														
Dist. Lat. Dop. Dist. Dist		12. 9 13. 8	10.0	76 77	62.3	44.7	36 37	110.8	79.9 80.5	96 97	158.6	115.2	56 57	207.9	151.1	
Dist. Lat. Dep. Dist. Dist. Dist. Dist. Dist. Dep. Dist. Dep. Dist. Dist. Dep. Dist. Dist. Dep. Dist. Dist. Dep. Dist. Dep. Dist. Dist. Dep. Dist. Dist. Dep. Dist. Dist. Dep. Dist. Dep. Dist. Dist. Dep. Dist. D	14 15	II. 3 I2. I	8.8	74 75	59.9 60.7	44 1	34 35	109. 2	79-4	94 95	150. 9	112.6	54 5Ş	205. 5	149.9	
Dist. Lat. Dep. Dist. Dist. Dist. Dist. Dist. Dep. Dist. Dep. Dist. Dist. Dep. Dist. Dist. Dep. Dist. Dist. Dep. Dist. Dep. Dist. Dist. Dep. Dist. Dist. Dep. Dist. Dist. Dep. Dist. Dep. Dist. Dist. Dep. Dist. D	13	9. 7 10. 5	7.6	73	59.1	42.9	33	107.6	77.0	93	155. 3 156. 1	113.4	52 53	204.7	145.7	
Dist. Lat. Dop. Dist. Dist. Dist. Dist. Dist. Dop. Dist. Dop. Dist. Dist	11	8.0	6.5	71	57.4	41. 7	131	100.0	77. 0	191	154.5	112. 3	25I	203. I		
Dist. Lat. Dop. Dist. Dist. Dist. Dist. Dist. Dop. Dist. Dop. Dist. Dist	او	7.3	5.3	69	55.8	40.6	29	104.4	75.8	89	152.9	111.1	49	201.4	146.4	
Dist. Lat. Dop. Dist. Lat. Dep. Dist. Dist. Dep. Dist. Dep. Dist. Dep. Dist. Lat. Dep. Dist. Dep. Dist. Dep. Dist. Dep. Dist. Dep. Dist. Dist. Dep. Dist. Dist. Dist. Dist. Dist. Dep. Dist. Dist. Dist. Dist. Dist. Dist. Dist. Dist. Dist. Dist		5.7	4.7	67 68	C4.2	39-4	27 28		74-0	87 88	151. 3	109.9	47	199. 8	145.2	
Dist. Lat. Dop. 2 a. 6. 6. 6. 49. 4. 35. 9. 121 97. 9. 71. 1 81 165. 4. 165. 4. 165. 195. 9. 147. 2 1.6. 1.2 63 50.2 35. 4. 22 56. 7. 71. 7 82 147. 2 10.7. 0. 42 195. 8 142. 2 3. 4. 1.8 63 50. 2 35. 4. 22 56. 57. 23. 3. 8. 16. 1 197. 6 44 195. 6 142. 2 3. 2 3. 4 64 15. 8 17. 6 24 195. 7 22. 8 8 145. 2 197. 6 145. 4 14			. 29 35	1 2	53-4	38. 2 38. 8		101.1	73-5 74-1	85 86	150.5	108. 7	45 46	199.0	144.0	
Dist. Lat. Dop. 1 0.8 0.6 61 49.4 35.9 121 97.9 71.1 181 146.4 106.4 241 195.0 141.7 2 1.6 1.2 63 50.2 30.4 22 98.7 71.7 82 147.2 107.0 42 195.8 143.2	3 4	3.2	24	64	51.8	37. O	24	99- 5 100- 3	72.0	84	148. Q	107. 6	44	196.6	143.4	
Dist. Lat. Dop.	2	1.6	1. 2	62	50.2	35. 9 36. 4	22	97.9 98.7	71. 1 71. 7	82	146.4	107. 0	43	195. 8	142. 2	
	-		<u> </u>	-	-	⊢∸	—		-				-		 -	
DISTRIBUTION OF A MINISTER AND DEPARTMENT OF THE PROPERTY OF T																
				171773	7077 0					200						

	D	FFE	REN	CE C	F L	ATIT	UDE	AND	DE	PART	URE	FOR	. 37°.		
Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat	Dep.	Dist.	Lat.	Dep.	
1	0.8	0.6	·61	48.7	36. 7	121	96.6	72.8	181	144.6	108.9	241	192. 5	145.0	
3	1.6 2.4	1.2	62 63	49. 5 50. 3 51. 1	37. 3 37. 9 38. 5	22	97.4 98.2	73·4 74·0	83	145.4 146.2	109. 5 110. I	42 43	193. 3 194. 1	145.6	
4	3.3	2.4	64		38. 5	24	00.0	74.6	84	146. q	110.7	44	194.9	146.8	
ş	48 46	3.0 3.6	65	51.9 52.7	39. I 39. 7	25 26	99.8 100.6	75.2 75.8 76.4	85 86	147.7	111.9	45 46	195. 7 196. 5	147.4 148.0	
3		42	67 68	53-5	40.3	27 28	101.4	76.4 77.0	87 88	149. 3 150. I	112. 5 113. 1	47	197. 3 198. 1	148.6	
	7.2	\$.4 6.0	69	53- 5 54- 3 55- 1	41.5	29	102.0	77.6 78.2	89	150. 9	113.7	49	198.9	149.9	
10		6.6	70	55.9	42.1	30	103.8	78. 2 78. 8	90	151. 7 152. 5	114.3	50 251	199. 7 200. 5	150. 5 151. 1	
11	8.8 9.6	7.2	71 72	56. 7 57. 5 58. 3 59. 1	42. 7 43. 3	131 32	104.0 105.4 106.2	79-4 80-0	191 92	153.3	115.5	52	201, 3	151.7	
13	10.4	7. 2 7. 8 8. 4	73 74	57. 5 58. 3	43.9	33	106.2	80.0	93	154. I	115.5 116.2 116.8	53	202. 1	152.3	
1 14	15 12.0 9.0 75 59.9 45.1 35 107.8 81.2 95 155.7 117.4 55 203.7 153.5 16 12.8 9.6 76 60.7 45.7 36 108.6 81.8 95 136.5 118.0 56 204.5 134.1 17 12.6 10.0 17 17 17 17 18 18 18 18 18 18 18 18 18 18 18 18 18														
	15 12.0 9.6 75 59.9 45.1 35 107.8 81.2 95 155.7 117.4 55 203.7 153.5 16 12.8 9.6 76 60.7 45.7 36 108.6 81.8 96 156.5 118.0 56 204.5 154.1 17 13.6 10.2 77 61.5 46.3 37 109.4 82.4 97 157.3 18.8 6 57 205.2 154.7														
18	10 12.8 9.6 70 00.7 45.7 30 108.0 31.8 90 150.5 118.0 50 204.5 154.1 17 13.6 10.2 77 61.5 40.3 37 109.4 82.4 118.6 57 205.2 154.7 18 14.4 10.8 48 62.3 46.0 138 110.2 82.1 08 158 1 119.2 58 200.0 155.3														
19	18 14.4 10.8 16 62.3 46.9 38 110.2 83.1 98 158.1 110.2 58 206.0 155.3 19 15.2 11.4 79 63.1 47.5 39 111.0 83.7 99 158.9 119.8 59 206.8 155.9 10.1 10.2 10.4 60 207.6 156.5														
21	19 15.2 11.4 79 63.1 47.5 39 111.0 83.7 99 158.9 119.8 59 200.8 155.9 20 16.0 12.0 80 63.9 48.1 40 111.8 84.3 200 159.7 120.4 60 207.6 156.5														
22	17.6	13.8	82	64. 7 65. 5 66. 3	49.3 50.0	42	113.4	84. 9 85. 5 86. 1	02	161.3 162.1	121.6	62	209. 2	157. 7 158. 3	
23 24	19.2	14.4	84	07. 1	50.6	43	116.0	86.7	O.	162.0	122.8	64	210.8	158.0	
25	20.0	15.0	83 84 85 86	67.9 68.7	51. 2 51. 8	45	115.8 116.6	87. 3 87. 0	9 9	163. 7 164. 5	123.4 124.0	63 64 65 66	211.6	159. 5 160. 1	
27 28	21.6	15. 6 16. 2	87 88	69.5	52.4 53.0	43	117.4	87. 9 88. 5	37	165. 3 166. I	124.6	67 68	213.2	160.7	
28 20	22.4 23.2	16.9	88 80	70.3 71.1	53. 0 53. 6	48 49	118.2	89. î 89. 7	08	166.1	125. 2	68	214.0 214.8	161. 3 161. 9	
3	24.0	17. 5 18. 1	2	71.9	14.2	50	119.8	90.3	IÓ	167. 7	125. 8 126. 4	70	215.6	162.5	
31	24.8	18. 7	91 92	72. 7	54.8 55.4 56.0 56.6	151 52	120.6	90. 9 91. 5	211	168. 5 169. 3	127.0	271	216.4 217.2	163. I 163. 7	
32 33	25.6 26.4	19.3 19.9 20.5		73-5 74-3 75-9 77-5 78-3	33.4	53	122. 2	92.1	13	170. I	127. 6 128. 2	73	218.0	164.3	
33 34 35 36	27. 2 28. 0	20.5	93 94 95 96	75. 1	56.6	54	123.0 123.8	92.7	14	170.9	128. 8 129. 4	74	218.8	164. 9 165. 5	
33	28. 8	21.7	3	75-9 76-7 77-5	57. 2 57. 8 58. 4	33.55	124.6	93-3 93-9 94-5	15 16	172.5	130.0	78	220.4	166. 1	
37 38	89. 5 20. 2	22.3	3	77:5	58.4	57	125. 4 120. 2	94-5 95.1	17 18	173. 3 174. 1	130.6	77	221. 2	166. 7 167. 3	
39	30. 3 31. 1	23.5	99	79.1	59.6 60.2	122	127. 0	95. 7 96. 3	19	174.9	131.8	72 73 74 75 77 78 79 80	222. 8	167. 9	
40	31.9	24.1	100	79.9 80.7	60, 2	161	127. 8	96.3	20	175.7 176.5	132.4	80 281	223. 6 224. 4	160	
41 42	32. 7 33. 5	25.3	02	81.5	61.4	62	120.4	97.5 98.1	22	176. 5 177. 3 178. 1	133.6	82	225. 2	169.7	
43	34-3 35-1	25.9 26.5	3	82. 3 83. 1	62.0	63	130.2	98.1 98.7	23 24	178.0	134-2 134-8	83 84	226. 0 226. 8	170.3 170.9	
\$444	35.9 36.7	27. 1	3	83.9	62. 2	8	121.X	99-3	25 26	179.7	135.4	85	227. 6	171.5	
40	35-9 36-7 37-5 38-3	27.7 28.3 28.9		84-7 85-5 86-3	63.8	67	132.6 133.4	99.9 100.5	20	180.5	135. 4 136. 0 136. 6	86 87	228. 4 239. 2	172. I 172. 7	
47 48	37. 5 38. 3 39. 1	28.9	3	85. 5 86. 3	63.0	67 68	134.2	101, 1	27 28	182. ī	137. 2	84 85 86 87 88 89	230.0	173.3	
49 50	39. I 39. 9	29.5 30.1	10	87. I 87. 8	65. 6 66. 2	69 70	135.0	101.7	39 30	182. 9 183. 7	137. 2 137. 8 138. 4	90	230. 8 231. 6	173. 9 174. 5	
51	40.7	30. 7	111	88.6	66.8	171	136.6	102, 0	231	184. 5	139.0	291	232.4	175. 1	
52 53	41.5 42.3	31.3	13	89.4 90.2	67. 4 68. 0	72 73	137.4 138.2	103. 5	32	185. 3 186. 1	139.6	92	233. 2 234. 0	175. 7 176. 3	
53 54 55	43. I	32.5	14	91.0	168.6	74	130.0	104.7	33 34 35 36	1 186. o	140.8	93 94 95 96 97 98	2 ta . 8	176.0	
38	43.9	33. I 33. 7	15 16	91.8 92.6	69. 2 69. 8	75	139.8 140.6	105. 3	35 36	187. 7 188. 5	141. 4 142. 0	95 96	235. 6 236. 4	177. \$ 178. 1	
57 58	44.7 45.5 46.3	34.3	17	93.4	70.4	77	141. 4 142. 3	105. 9 106. 5 107. 1	37 38	189. 3 190. I	142. 6 143. 2	97	237. 2 238. 0	178.7	
50 59	47. 1	34-9 35-5 36-1	19	§5.0	71.6	70	143.0	107. 1	38 39	190.9	143. 2	98	238.8	179. 3 179. 9 180. 5	
60	47.9	36. í	20	95. 8	72. 2	86	143.8	108. 3	40	191. 7	144-4	300	239.6	180. 5	
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dop.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	
												[For	53 Deg	rees.	

DIFFERENCE OF LATITUDE AND DEPARTURE FOR 88°.

Dist.	Let	Dep.	Dist.		-	-			-	· ·				
		<u> </u>		Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dop.	Dist.	Lat.	Dep.
1 2	a. 8	0.6	61 62	48.1 48.9	37.6 38.2	121	95. 3 96. 1	74- 5 75- 1	181 82	143. 6 143. 4	111.4 112.1	241 43	189. 9 190. 7	148.4 149.0
3	2.4	1.8	63	49.6	38.8	23	96.9	75. 7 76. 3	83	144. 3	112. 7	43	191.5	149.6
1 1	3. 2 3. 9	2. 5 3. 1	64	50.4 51.2	39. 4 40. 0	24	97. 7 98. 5	76.3	84	145. 0 145. 8	113. 3 113. 9	44	192. 3	150. 2 150. 8
ş	4.7	3.7	65 66	52.0	40.6	25 26	99-3	77.6	85 86	146.6	114 E	45	193. 1	151.5
7	5.5	43	67 68	52. 8 53. 6	41.2	27 28	100. 1	78. 2 78. 8	87 88	147. 4 148. I	115. 1	47	194.6	152.1
9	5. 5 6. 3 7. 1	5. 5 6. 2	69	54-4 55-2	42.5	29	101. 7	79-4	89	1481.9	115. 1 115. 7 116. 4	49	195. 4 196. 2	152. 7 153. 3
10	7.9	6. 2	70	55. 2	43. I	30	102. 4	80.0	96	149.7	117.0	50	197. 0	153.9
12		7:4 8:0	71 72	55.9 56.7 57.5 58.3	43-7 44-3	131	103. 2 104. 0	80. 7 81. 3	191 92	150. 5 151. 3	117.6	251 52	197. 8	154. 5 155. I
13	9. 5 10. 2	8.6 8.6	73	57· 5	44. 9 45. 6	33	104.8	81.9	93	152. I	118.2	53	199.4	155. 8 156. 4
14 15 16	11.0	9.3	74	59.1	46. 2	34 25	105.6	82. 5 83. 1	94	152. 9 153. 7	119. 4 120. 1	54	200. 2	156.4
16	12. 6	9.9	75 76	50.0	46.8	35 36	107. 2	83.7	95 96	154.5	120.7	55 56	201. 7	157.6 158.2
17	13. 4 14. 2	10.5	77 78	60. 7 61. 5	47.4 48.0	37 38	108.0	84. 3 85. 0	97 98	155. 2 156. 0	121.3	57 58	202. 5 203. 3	158.2 158.8
19	15.0	11.7	79 80	62.3	48.6	39	109.5	85.6	99	156.8	122.5	59 60	204. 1	159.5
20	15.8	12. 3	80 81	63. o 63. 8	49-3	40	110.3	86. 2 86, 8	200	157.6	123. 1		204.9	159. 5 160. I
22	17. 3 18. 1	13.5	82	64.6	49-9 50-5	141	111.1	87.4	201	158.4	123. 7 124. 4	261 62	205. 7	160. 7 161. 3
23	18. 1	14.2	83 84	65.4 66.2	50. 5 51. I	43	112.7	88.o	03	160.0	125. 0	61	207. 2	161. 9 162. 5
24 25	18. 9 19. 7	14.8	85 86	67.0	51. 7 52. 3	44	113.5	88. 7 89. 3	94	160. 8 161. 5	125.6	64	208. 0	162. 5 163. 2
25 26	20. 5	15.4	86	67. o 67. 8 68. 6	52. 9 53. 6	45 46	115.0	89.g	05 06	162. 3	126. 8	65 66	209.6	163.8
27 28	21. 3 22, 1	16.6 17.2	87 88	69.3	53. 6 54. 2	47 48	115.8 116.6	90. 5 91. I	°7	163. 1 163. 9	127. 4 128. 1	67 68	210.4	164.4
29	22. 9 23. 6	17.9 18.5	89	70.1	54.8	49	117.4	91.7	ى س	164. 7	128. 7	69	212.0	165. o 165. 6
30		18.5	90	70.9	55.4	50		92. 3	10	165. 5	129. 3	70	212.8	160.2
32	24. 4 25. 2	10.7	92	71. 7 72. 5	56. o 56. 6	151 52	119.0	93. 0 93. 6	211 12	166. 3 167. I	129. 9 130. 5	271 72	213.6	166. 8 167. 5
33	25. 2 26. 0 26. 8	20.3	93	73-3	57· 3 57· 9 58. 5	53	120.6	94-2	13	167. 8	131. 1	73	215. I	168. 1
34 35	27.6	21.5	94	74.1	57.9	54	121. 4 122. I	94. 8 95. 4	14	168. 6 169. 4	131. 8 132. 4	74	215.9	168. 7 169. 3
35 36	28. 4	22. 2	95 96	74-9 75-6 76-4	59. I	55 56	122. 9	06.0	15	170.2	133.0	75 76	217.5	169.9
37 38	29. 2 29. 9	22. 8 23. 4	97 98	70.4	59. 7 60. 3	57 58	123. 7 124. 5	96. 7 97. 3	17	171.0	133. 6 134. 2	77 78	218. 3 219. 1	170.5
39	30. 7	24.0	99	77. 2 78. 0	61.0	59	125. 3 120. i	97-9	19	172.6	134.8	79	219. 9	171.8
40 41	31.5	24.6	100	78. 8	61.6	161	120. 1		20	173.4	135.4 136.1	28 I		172.4
42	33. 1	25. 9 26. 5	02	79.6 80.4	62. 8	62	127.7	99. I 99. 7	22	174.9	136. 7	82	221.4	173. 0 173. 6
43 44	33. 9 34. 7	26. 5 27. 1	03 04	81. 2 82. o	63. 4 64. 0	63 64	128.4	100.4	23	175.7	137.3 137.9	83 84	223.0	174.2
45 46	35. 5 36. 2	27.7	3,2	82. 7	64.6	65	130.0	101.6	24 25	176.5	1379	85 86	223.8	174.8
46	36. 2 37. 0		06	So E	65. 3	66	130.8	102. 2	25 26	177.3 178.1	139. 1	86	225.4	175. 5 176. 1
47	37. 8 38. 6	28. 9 29. 6	°7	85. 1	65.9	67 68	131.6 132.4	102.8	27 28	178.9	139. 8 140. 4	87 88	226. g	176.7
49	38.6	30. 2	9	84. 3 85. 1 85. 9 86. 7	67. 1	69	133. 2	104.0	29	179. 7 180. 5	141.0	89	227. 7 228. 5	177.9
50 51	39. 4 40. 2	30. 8 31. 4	10	87. f	68.3	70 171	134.0	104. 7	30 231	181. 2	141.6	90 291		
52	41.0	32.0	12	87. 5 88. 3	69.0	72	135. 5 136. 3	105. 9	32	182. 8	142. 8	92	229. 3 230. I	179. 2
53 54	41.8 42.6	32. 6 33. 2	13	89. 0 89. 8	69.6	73	136. 3 137. I	106. 5	33	183. 6	143. 4	93	230. 9	180.4
55 56	43-3	22.0	15	90.6	70.8	74 75 70	137. 9 138. 7	107. 7	34 35	184. 4 185. 2 186. 0	144. I 144. 7	94 95	231. 7	181. 0 181. 6
50	44. I	34- 5	16	91.4 92.2	71.4	76	138.7	108.4	35 36	186. o 186. 8	145. 3	95 96	233. 3	182. 2
57 58	44-9 45-7 40-5	34· 5 35· 1 35· 7 36· 3	17	93.0	72.6	77	139. 5 140. 3	109.0	37 38	187. 5	145. 9 146. 5	97 98	234-0 234-8	183. 9 183. 5
\$9 60	45. 7 46. 5	36. 3 36. 9	19	93.8	73-3	79	141. 1	110. 2	39	188. 3	147. I	99	235. 6 236. 4	184.1
	47.3			94.6	73.9	-	141.8	110.8	40	189. 1	147. 8	300	236. 4	184. 7
Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dop.	Lat	Dist.	Dep.	Lat
												[For	52 Deg	rees.

DIFFERENCE OF LATITUDE AND DEPARTURE FOR 89°.

Dist.	Lat.	Dep.	Dist.	Lat	Dep.	Dist.	Lat	Dep.	Dist.	Lat.	Dep	Dist.	Lat	Dep
		-			_	Disc.			_		Deb			Deb
2	0.8	0.6	61	47: 4 48: 2	38.4	121	94.9	76.1	181	140.7	113.9	241	187. 3 188. 1	151. 7
*	1.6	I. 3 I. 9	62 63	48.2 49.0	39.0 39.6	23	94.8	76.8	82 83	141. 4 142. 2	114.5	42 43	188. B	152.3
3 4	2. 3 3. I	2.5	1 62	49.7	40.3	24	95.6 96.4	77.4	84	143.0	115.2	44	189. 6	152.9
š	2.0	3. š 3. 8	64 65 66	49-7 50-5	40.9	25 26	97:1 97:9 98:7	78.7	85	143.8	116.4	45 46	190.4	154.2
	4.7 5.4 6.2	3.8	66	51.3	41.5	26	97.9	79-3	86	144.5	117. 1	46	191. 2	154.8
7	ş. 4	4-4 5-0	67 68	52. 1	42.2	27 28	99.5	80.6	87 88	145. 3 146. I	117. 7 118. 3	47 48	192. 0	155.4 156.1
او	7.0	5.7	69	32.6	43-4	29	100.3	81.2	89	146.9	118.9	49	193 5	156.7
1ó	7. 0 7. 8	5.7 6.3	70	52.8 53.6 54.4	44.1	30	101.0	81.8	9ó	147. 7	119. 6	50.	194.3	157.3
11	8.5	6.0	71	55. 2 56. 0	44-7	131	101.8	82.4	191	148.4	120. 2 120. 8	25I	195. 1	158.0 158.6
12	9. 3 10. I	7. 6 8. 2 8. 8	72	56. 7	45.3 45.9 46.6	32	102. 6 103. 4	83. I 83. 7	92	149. 2 150. 0	120. 8	58 53	195. 8 196. 6	150.0
13 14	10.1	8.8	73 74	50.7	126.6	33 34	104.1	84.3	93 94	150.8	121. 5 122. 1	ᆲ	197.4	150.8
15 16	IO. 9 II. 7 I2. 4	9.4 10.1	75 78	57. 5 58. 3	47. 2	35 36	104.9	1 8c.o	95 96	151.5	122. 7	54 55 56	197. 4 198. 2	160.5
16	12.4	10.1	75	59. I 59. 8 60. 6	47.8 48.5	36	105. 7	85.6 86.2	96	152. 3	123. 3	56	198.9	161. 1
17	13.2	10. 7 11. 8	77 78	59-8	48. 5 49. I	37 38	100.5	86.8	97 98	153. 1 153. 9	124. 0 124. 6	57 58	199. 7	161. 7 162. 4
19	14.8	12.0	70	61.4	49.7	39	107. 2	87. 5	99	154-7	125.2	1 %	201.3	163.0
20	15. 5	12.6	79 80	61. 4 62. 2	50. 3	40	108. 8	87. 5 88. 1	200	155.4	125. 9	59 60	202. 1	163.6
21	16. 3	13.2	18	62.9	51.0	141	109.6	88.7	201	156. 2	126. 5	261	202. 8	164. 3
22	17. 1	13.8	82	63.7 64.5 65.3 66.1	51.6	42	110.4	89.4	02	157.0	127. 1	62	203.6	164.9
23 24	18.7	14.5 15.1	83 84	65.2	52. 2	43	111.1	90.0	03 04	157.0	127. 8 128. 4	23	204. 4.	165. 5 166. 1
25 26	19.4	15.7 16.4	84 85 86	66. i	52. 9 53. 5 54. I	45	112.7	91.3	05	157. 8 158. 5 159. 3 160. 1	129. 0	63 64 65 66	205.9 206.7	165.8
26	20. 2	16.4	86	63.8	54.1	45 46	113.5	91.9	90	160. 1	129.6	66	206. 7	167. 4 168. 0
27 28	21.0	17.0 17.6	87 88	67. 6 68. 4		47	114, 2	92. 5	°7	160. 9 161. 6	130. 3 130. 9	67 68	207. 5 208. 3	168.7
29	22.5	18.2	89	69.2	55.4 56.0	49	115.0	93. 1 93. 8	9	162.4	131.5	69	200. I	169.3
30	23. 3	18. 9	90	69.9	56.6	56	115.8 116.6	94.4	10	163. 2	132. 2	70	200.8	169.9
31	24. I	19. 5 20. 1	91	70.7	57-3	151	117.3 118.1	95.0	211	164.0	132.8	271 72	210.6	170.5
32	24. 9 25. 6 26. 4	20. 1	92	71.5	57.9 58.5 59.2	52	118.1	95.7 96.3 96.9	12	164. 8. 165. 5	133.4	72	211.4	171. 2
33 34	25.0	21.4	93 94	72.3	50.5	53 54	118.9	90.3	13 14	166. 3	134.0 134.7	73 74	212.2	172.4
35	27. 2 28. 0	22.0	55 96	72.8	59.8	55 56	120.5	97·5 98·2	15	167. 1	135.3	75	213.7	173.4
35 36	28.0	22. 7	96	74.0	60.4	56	121. 2	98.2	16	167. 9 168. 6	135. 3 135. 9 136. 6	76	214.5	173-7
37 38	28.8	83.3	97 98	75.4 76.2	61,0	57 58	122. 0 122. 8	98.8	17 18	169.4	130.0	75 76 77 78	215.3 216.0	174-3 175.0
39	10.3	23.9 24.5	99	76.9	62.3	. 50	123.6	99-4 100-1	10	170.2	137.8	79	216.8	175.6
40	29. 5 30. 3 31. 1	25.2	100	77.7	62.9	59	124.3	100.7	20	171.0	137.8		217.6	175.6 176.2
41	31. 9 32. 6	25.8	101	78. 5	63.6	161	125. I	101.3	221	171. 7	139. 1	281	218.4	176.8
48	32.6	26.4	02 03	79.3 80.0	64.2	62 63	125. 9 126. 7	101.9	22	172.5	139. 7 140. 3 141. 0	82	219.2	177.5 178.1
43 44	33- 4 34- 2	27. I 27. 7	04	80.8	65.4	64	127. 5	103. 2	,23 24	173-3	141.0	83 84	220.7	178.7
45	35. O	27. 7 28. 3	05 06	81.6	65.4 66.1	65 66	127. 5 128. 2	103.8	25 26	174.9	141.6	85 86	221.5	179.4 180.0
46	35. 7 36. 5	28.9	06	82. 4	166.7	66	129.0	104.5	26	175.6 176.4	142. 2	86	222. 3	180.0 180.6
47	30. 5.	29.6 30.2	97 08	83.2	62.3	67 68	129. 8 130. 6	105. 1	27 28	170.4	142.9	87 88	223. 0 223. 8	184. 3
49	37· 3 38. 1	30.8	9	83. 9 84. 7	68.6	69	131.3	105.7	29	177. 2 178. 0	143. 5 144. I	89	224.6	181. q
50	38.9	31.5	IÓ	85.5	69. 2	70	132. 1	107.0	30	178. 7	144-7	90	225.4	I 182. € I
51	39.6	32. I	111	86. 3	69.9	171	132.9	107.6	231 32	179. 5 180. 3	145.4	291	226. 1	183. I
52	40. 4 41. 2	32. 7 33. 4	13	87. 0 87. 8	70. 5 71. 1	72 73	133.7 134.4	108.2	32 33	180. 3 181. 1	146.0 146.6	92 93	226.9	183. 8 184. 4
53 54 55 66 57 58	42.0	34-0	14	88.6	71.7	73	135. 2	109.5	33	181.9	147. 2	94	227. 7 228. 5	185.0
55	42.7	34.6	15	89.4	72.4	75	135. 2 136. 0	110.1	35 36	182, 6	147.9	95	229. 3	184.6
46	42.5	35. 2	16	90. I	73.0	76	136.8	110.8	36	183.4	148.5	96	230.0	186. 3 186. 9
57	44- 3 45. I	35. 9 36. 5	17	90.9	73.6 74.3	77 78	137.6 138.3	111.4	37 38	184. ź 185. o	149. I 149. 8	97 98	230. 8 231. 6	187. 5
59 60	45. 9	1 .7. 1	19	92.5	74.9	72	139.1	112.6	39	185. 7 186. 5	159.4	99	232.4	187. 5 188. 2
66	45. 9 40. 6	37.8	aó	93.3	75. 5	8ó	139.9	113.3	40	186. 5	151.0	300	233. i	188.8
Dist.	Dep.	Lat.	Dist	Dep.	Lef	Dist	B==	Lat.	Dist.	Dep.	Lat	Dist	Dep.	Int
D-86.	neb.	Last.		Dep.		- DIE.	Dep.							
l												[Fo	r 51 Deg	rees.

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DIFFERENCE OF LATITUDE AND DEPARTURE FOR 40°.

Dist.	Let.	Dep.	Dist.	Let.	Dep.	Dist.	Let.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.
1	0.8	0.6	61	46.7	39. 2	121	92. 7	77.8 78.4	181	138. 7	116. 3	241	184. 6	154. 9 155. 6
:	1.5 2.3 3.1	1.3	6a 63	47.5 48.3	39.9 40.5	23 23	93- 5 94- 2	75.4	82 83	139. 4 140. 2	117.0	42 43	185. 4 186. 1	156.2
3 4	3.1	1. 9 2. 6	64	40.0	41. 1	24	65.0	79-7	84	141.0	118.3	44	186. o	156.8
8	3.8	3-8	65	49.8	41.8	25 26	95.8		85 86	141.7	118.9	45	187. 7 188. 4	157. 5 158. 1
	4.6 5.4 6.1	3.9	67	50.6 51.3	42. 4 43. 1		96.5	81.0 81.6	87	142. 5	119. 6 120. 2	40	188.4	158.8
8	5. 4 6. i	4 S 5. I	67 68	52. 1	43-7	27 28	97. 3 98. 1	82.3	87 88	144.0	120. 8	47 48	190.0	159. 4 160. I
9	6.9 7.7	5. 8 6. 4	69	52. 9 53. 6	44· 4 45· 0	29	98. 8 99. 6	82. 9 83. 6	89 90	144.8	121. 5 122. I	49 50	190. 7 191. 5	160. I 160. 7
10	7. 7 8. 4	7. 1	70 71	54-4	45.6	30 131	100.4	84.2	191	146. 3	122. 8	251	192. 3	161.3
12	9. 2	7.7	73	55.2	45.6 46.3	32	101. 1	84.8	92	147. 1	123.4	52	102.0	161. 3 168. 0 162. 6
13 14	10.0	8.4	73	55. 9 56. 7	46. 9	33 34	101. 9 102. 6	85. 5 86. 1	93 94	147. 8	124.1	53 54	193. 8 194. 6	162.2
15	11.5	9.0 9.6	74 75	57.5	46. 9 47. 6 48. 2	35	103. 4	86.8	35	149.4	185. 3 120. 0	55 56	195. 3 196. I	163. 9 164. 6
16	12. 3	10. 1	75 76	58.2	48.0	35 36	104. 2	87. 4 88. i	96	150.1	126. 6	56	196. 1	164.6
17	13.0	10.9	77	59. 0 59. 8	49. 5 50. I	37 38	104. 9	88.7	97	150.9	127.3	57 58	196. 9 197. 6 198. 4	165. 2 165. 8 166. 5
19	10. 7 11. 5 12. 3 13. 0 13. 8 14. 6	12. 2	79	86.5	50.8	39	105. 7 106. 5	89.3	99	152.4	127. 9	59	198.4	166.5
20	15-3 16. I	12.9	80 81	61.3	51.4	40	107. 2	90.0	200	153.2		961	199. 2	167. i 167. 8
21 22	16. 0	13. 5 14. 1	82	62.8	52. 1	141	108.8	01. 1	201 02	154-0 154-7	129. 2	62	199.9	168.4
23	16. 9 17. 6 18. 4	14.8	83	63.6	52. 7 53. 4	43	109. 5	91.9 92.6	03	155. 5 150. 3 157. 0	130.5	63	201.5	169. 7 170. 3 171. 0
24	18. 4 19. 2	15.4 16.1	84	64.3	CL O	44	110. 3 111. I	92.6	3,4	150.3	131.1	64	203. 2	170.7
25 26	19.2	16. 7	85 86	65. I 65. 9 66. 6	54. 6 55. 3	45 46	111.8	93. 2 93. 8	95 86	157. 8 158. 6	132.4	65 66	203.8	171.0
27	19.9 20.7 21.4	17.4	87 88	66.6	55. 9 56. 6	47	112.6	94- 5 95- 1	°7	158.6	133.1	67 68	204. 5	171.6
20	21. 4	18.6	80	67. 4 68. 2	57. 2	49	113.4 114.1	95.1	09	159. 3 160. I	133. 7 134. 3	69	205. 3 200. I	172.9 173.6
30	23.0	19.3	90	68.9	57. 2 57. 9	50	114.9	95. 8 96. 4	10	160. g	135.0	70	206.8	
31	23. 7 24. 5	19. 9 20. 6	91	69. 7 70. 5 71. 2	58. 5	151	115.7	97. 1 97. 7	211	161. 6 162. 4	135.6	271 72	207.6	174. 2 174. 8
32 33	25. 3	21. 2	92 93	70.5	59. 1 59. 8	52 53	117. 2	98.3	13	162.2	136. 3 136. 9 137. 6 138. 2	73	209. I	175.5
34 17 36	25. 3 26. 0 26. 8	21.9	انمة	72.0 72.8	60.4	54	118.0	99.0	14	163.9	137.6	74	209.9	176.8
3	26. 8	22. 5 23. 1	95 96	72.8	61. 1 61. 7	54 55 56	118.7	99.6 100.3	15	164. 7	138.8	75 76	210. 7 211. 4	177.4
37 38	27. 6 28. 3	23.8	97 98	73- 5 74- 3 75- 1	62.4	57 58	120. 3	100. 9	17	163. 5 166. 2	139.5	77	212. 2	178.1
38	29. I	24. 4 25. 1	98	75. 1	63.6	58	121.0	101.6	18	167. 0	140.1	75	213.0 213.7	178.7
39 40	29. 9 30. 6	25. 7	100	75. 1 75. 8 76. 6	64.3	59 60	122.6	102. 8	20	167. 8 168. 5	140. 8 141. 4	79 80	214.5	180.0
41	31.4	26.4	101	77·4 78. 1	64.0	161	123. 3	103. 5	221	169. 3	142. 1	281	215. 3	180. 6
42 43	32. 2 32. 9	27. 0	02 03	78. I 78. 9	65.6	6a 63	124. 1	104 I 104 8	22 23	170.1	142. 7 143. 3	82 83	216.0	181. 3 181. 9 182. 6
44	33. 7	28. 3	04	79.7	66.8	64	124. 9 125. 6 126. 4	105. 4 106. 1	24	171.6	144.0	84	217.6 218.3	182.6
45	34 5	28.9	05 06	80. 4 81. 2	67. 5 68. 1	65	120.4	106.1	25 26	172.4 173.1	144. 6 145. 3	85 86	218. 3 219. I	183. 2 183. 8
4 ⁰	35. 2 36. 0	29.6 30.2	00	81. 2	68.8	67		107.3	27	173.9	145. 9	87 88	219. 9 220. 6	184.5
47	36.8	30.0	37	82. 7 83. 5	60.4	67 68	127. 9 128. 7	108.0	27 28	174.7	145. 9 146. 6	88	220. č	185. 1
49 50	37· 5 38. 3	31. 5 32. 1	10	83. 5 84. 3	70. I 70. 7	69 70	129. 5 130. 2	108. 6 109. 3	29 30	175.4 176.2	147. 2 147. 8	89 90	221.4	184. 5 185. 1 185. 8 186. 4
51	20. I	32. 8	111	8c. o	71.3	171	131.0		231	177.0	148.5	291	222. 9	187. 1
52	30. 8	33-4	12	85. 8 86. 6	72. 0	72	131.8	109. 9 110. 6	32 33	177.7	149. I	92	223. 7	187. 7 188. 3
53 54	40. 6 41. 4	34 I 34 7	13	80.6	72.6	73 74	132. 5 133. 3	111.2	24	170.5	149. 8 150. 4	93 94	224. 5 225. 2	180.0
55 56	42. 1	35.4	15 16	87. 3 88. t	73-9 74-6	75	134.1	112.5	35 36	179. 3 180. 0	151.1	95 96	82Ô. O	189.6
56	42. 9 43. 7	.35· 4 36· 6 36· 6	16	88. g 89. 6	74.6	76	134.8	113. 1	36	180. 8 181. 6	151.7	90	226. 7 227. 5	190. 3 190. 9
57 58	44.4	37. 3	17	90.4	75. 2 75. 8 76. 5	77	135. 6 136. 4	114.4	37 38	182. 3	153.0	97 98	228. 3	191.6
59	45. 2	37· 3 37· 9 38· 6	19	91.2	76.5	Z	137. I	115. 1	39	183. 1	153.6	99	229. 0 229. 8	192. \$ 192. 8
60	46.0	38. 6	20	91.9	77. i	L <u></u>	137.9	115. 7	40	183. 9	154-3	300	#2y. 0	
Dist	Dep.	Lat	Dist.	Dop.	Lat	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.
												[For	50 Deg	rees.

DIFFERENCE OF LATITUDE AND DEPARTURE FOR 41°. Dist Lat. Dep. Dist Lat. Dep. Dist. Lat Dep. Dist. Lat. Dop. Dist. Lat. Dop. 118.7 158. 1 158. 8 61 46, o 46, 8 136. a. 8 91. 3 92. 1 92. 8 181 181. 9 182. 6 183. 4 184. 1 184. 9 185. 7 186. 4 187. 2 187. 9 188. 7 1 40.0 121 79-4 0 7 80-7 80-7 83-3 84-6 3 85-6 85-6 241 137. 4 138. 1 138. 9 139. 6 140. 4 141. 1 141. 9 L 3 2.0 119.4 2 1.53085308 62 **40.** 7 22 82 42 41.3 42.0 42.6 159. 4 160. 1 160. 7 161. 4 47. 5 48. 3 49. 8 50. 6 51. 3 52. 8 53. 6 23 63 64 65 66 83 84 85 86 87 88 89 434454 34 24 25 26 93. 6 94. 3 95. 8 95. 8 2334550 120. 7 121.4 ş 43-3 43-4-6 45-3 45-9 45-6 122. o 122. 7 123. 3 124. 0 67 27 28 162. 0 7 47 48 49 50 162. 7 30 30 97. 4 98. 1 98. 9 69777737475777798 163. 4 164. b 9 10 7.5 8.3 9.1 9.8 10.6 143.4 124.7 90 191 92 93 94 95 96 97 98 189. 4 190. 2 190. 9 191. 7 125. 3 126. 0 126. 6 127. 3 127. 9 128. 6 164. 7 11 7. 2 144- 1 144- 9 145- 7 140- 4 147- 9 148- 7 149- 4 150- 9 7.95 9.8 10.2 11.8 54 55 8 55 55 6 165. 3 160. 0 47. 2 12 37 33 34 35 35 37 38 39 40 47.9 47.9 49.9 50.5 87.3 87.9 88.6 89.4 90.5 91.8 13 14 15 16 100. 4 101. 1 166. 6 11.3 12.1 12.8 13.6 14.3 15.1 191. 7 192. 5 193. 2 194. 0 194. 7 195. 5 167. 3 168. 0 101. 9 102. 6 57.41 9 6 4 57.55.55.55.64 129. 2 129. 2 129. 9 130. 6 103. 4 104. 1 104. 9 105. 7 168.6 17 18 51. 8 51. 8 52. 5 169. 3 169. 9 170. 6 19 12.5 13. 200 131. 2 13.8 14.4 15.7 16.4 17.1 171. 2 171. 9 172. 5 15.8 16.6 81 82 61. i 106.4 62 63 65 65 65 69 70 197. 0 31 53. 8 53. 8 54. 5 55. 8 55. 4 57. 7 53. 4 59. 0 141 92. 5 93. 8 93. 8 94. 5 95. 8 96. 4 97. 8 98. 4 201 151. 7 152. 5 153. 2 154. 7 154. 7 155. 5 157. 0 157. 7 158. 5 131.9 107. 8 107. 9 108. 7 61.96 63.4 9 64.9 66.7 66.7 66.7 9 66.4 9 70.9 71.7 132. 5 133. 2 133. 8 134. 5 135. 1 135. 8 136. 5 137. 1 197. 7 198. 5 199. 2 22 44444444 03 17.4 18.1 18.9 19.6 20.4 21.1 171.9 172.5 173.2 173.9 174.5 175.8 175.8 834588889953345997899 32428 23 24 100. 7 109. 4 110. 8 110. 9 111. 7 112. 5 113. 2 200. 8 201. 5 202. 3 203. 0 203. 8 37 17.7 18. 4 19. 0 19. 7 29 30 \$1.9 22.6 49 50 9 23. 4 24. 2 24. 9 25. 7 20. 4 27. 2 177.8 178.4 179.1 179.8 180.4 181.1 114 0 114 7 115 5 116 2 99. 1 99. 7 100. 4 101. 0 20. 3 21. 0 59. 7 60. 4 61. 0 151 53 53 54 55 55 55 57 58 59 60 159. 2 160. 0 160. 8 161. 5 162. 3 163. 6 164. 5 165. 3 166. 0 138. 4 139. 1 139. 7 140. 4 141. 1 141. 7 142. 4 143. 0 143. 7 144. 3 271 72 73 74 75 77 77 78 79 80 204.5 31 211 12 205. 3 200. 0 206. 8 32 21. 6 33 34 35 36 37 38 39 49 13 14 15 16 22.30623.43925.8 61. 7 117.0 117.7 118.5 101. 0 101. 7 102. 3 103. 0 103. 7 104. 3 105. 0 62.3 63.6 64.3 64.3 65.6 66.3 66.3 66.2 907. 908. 71. 7 72. 5 73. 2 74. 7 75. 5 70. 2 31 27.9 28.7 29.4 33.2 209. 8 209. 1 181. 7 17 18 19 20 182. 4 183. 0 119. s 120. 0 183. 7 184. 4 185. 0 185. 7 186. 3 120. 8 211. 3 26. 9 27. 6 28. 2 166. 8 167. 5 168. 3 169. 1 169. 8 170. 6 171. 3 172. 1 172. 8 173. 6 161 62 63 64 65 66 121. 5 122. 3 123. 0 123. 8 281 83 84 85 87 88 89 41 42 101 105. 6 106. 3 106. 9 107. 6 108. 2 108. 9 110. 9 111. 5 145.0 145.6 140.3 147.0 148.3 148.9 150.9 150.9 152.8 152.9 153.5 154.8 155.5 154.8 212. I 30.9 221 212.8 213.6 214.3 215.1 215.8 210.6 31. 7 32. 5 33. 0 34. 7 35. 2 37. 0 02 77. 0 77. 5 80. 8 81. 5 83. 8 84. 5 86. 8 23 03450 43 44 45 40 23 24 25 20 27 28 29 30 68. 2 68. 9 69. 5 70. 2 71. 5 72. 2 186. 3 187. 0 187. 6 124.5 125.3 126.0 126.8 29.5 30. 2 30. 8 31. 5 32. 8 188. 3 188. 9 189. 6 ã 47 48 97 08 217.4 218. I 69 70 127.5 49 09 10 218. 9 219. 6 śó 37.7 <u>90</u> 190. 3 33-5 34-1 34-8 112.2 112.8 113.5 114.2 114.8 115.5 116.8 38. 5 72.8 129. I 129. 8 130. 6 174-3 175-1 175-8 176-6 190. 9 191. 6 51 171 72 73 74 75 70 77 78 231 33 34 35 37 38 39 40 29 I 30, 5 39, 2 40, 0 40, 8 73-5 74-1 74-8 220. 4 221. I 52 53 54 55 56 12 93 94 95 97 98 99 13 14 102. 2 192. 8 192. 9 193. 5 194. 8 194. 6 195. 5 131. 3 132. 1 132. 8 132. 6 134. 3 135. 1 35. 4 36. 1 36. 7 221.9 222.6 41. 5 42. 3 177. 4 178. 1 178. 9 179. 6 180. 4 181. 1 15 16 87. 5 88. 3 89. 1 89. 8 90. 6 224. I 224. I 224. 9 225. 7 43. 8 43. 8 44. 5 45. 3 57 58 59 37. 4 38. 7 38. 7 39. 4 17 18 156.8 19 117.4 Z 225. 7 226. 4 190. ž 196. Š

Dust.

Dep. Let Die. Dep. Lat.

366 157-5

[For 49 Degrees.

Dist. Dep. Let Dist Dep. Lat Dist. Dep. Let

	D	IFFE	REN	ICE O	F L	TIT	UDE	AND	DEI	ART	URE I	FOR	42°.		
Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	
1	۵.7	0.7	61 62	45. 3 46. I	40. 8 41. 5	121	89.9	81. o 81. 6	181 82	134. 5	121. I 121. 8	241	179. 1	161. 3	
3	1.5	1.3	61	46.8	42.2	22	90.7 91.4	82. 3	83	135. 3 136. 0	121. 6	42 43	179.8	161. 9 162. 6	
4	3.0	2. 7	64	47.6	42. 8	24	92. I	83.0	84	116.7	123. 1	44	181. 3	163.3	
ş	3-7 4-5	3.3	538	40.0	43- 5 44- 2	25 26	92.9 93.6	83.6 84.3	85 86	137. 5 138. 2	123. 8 124. 5	45	182. I 182. 8	163. 9 164. 6	
7	6.8	4.7	67 68	49.8	44.8	27	94-4	85.0	87 88	139.0	125. 1	47	183.6	165. 3	
8	5.9 6.7	5.4	66	50. 5 51. 3	45. 5 40. 2	28 29	95. I	85. 6 86. 3	88 89	139. 7	125. 8- 126. 5	48 49	184. 3 185. 0	165. 9 166. 6	
10	7.4	6.7	70	52.0	46.8	30	95. 9 96. 6	87.0	90	141.2	127. 1	50	185. 8	167. 3	
11	8.2	7:4	71	52. 8	47· 5 48. 2	131	97·4 98. I	87. 7	191	141. 9	127.8	251	186. 5	168. o 168. 6	
12	8.9 9.7	8.7	72 73	53. 5 54. 2	48. 2 48. 8	32 33	98. t 98. 8	88. 3 80. 0	92 93	142. 7 143. 4	128. 5 129. 1	52 53	187. 3 188. 0	169.3	
14	10.4	9.4	74	55. o	49.5	34	99.6	89.0 89.7	94	144. 2	129.8	54	188.8	170.0	
15 16	11.1	10.0	75 76	55. 7 56. 5	50. 2 50. 9	35 36	100. 3 101. 1	90. 3 91. 0	95 96	144-9	130. 5 131. I	55 56	189. 5 190. 2	170.6	
17	17 12.6 11.4 77 57.2 51.5 37 101.8 91.7 97 140.4 131.8 57 191.0 172.0 18 13.4 12.0 78 58.0 52.2 38 102.6 92.3 98 147.1 132.5 58 191.7 172.6														
18	18 13.4 12.0 78 58.0 52.2 38 102.6 92.3 98 147. i 132.5 58 191. 7 172.6														
20	19 14.1 12.7 79 58.7 52.9 39 103.3 93.0 99 147.9 133.2 59 192.5 173.3 20 14.9 13.4 80 59.5 53.5 40 104.0 93.7 200 148.6 133.8 60 193.2 174.0														
21		14.1	81	60. 2	54. 2	141	104. 8	94-3	201	149.4	134.5	261	194.0	174.6	
	16. 3	14.7		60.9	54-9	42	105. 5	95.0		150. 1	135.2			175.3	
24	22 16. 3 14. 7 82 60. 9 54. 9 42 105. 5 95. 0 02 150. 1 135. 2 62 194. 7 175. 3 23 17. 1 15. 4 83 61. 7 55. 5 43 106. 3 95. 7 03 150. 9 135. 8 63 195. 4 176. 0 24 17. 8 151. 84 62. 4 64. 2 44 107. 0 06. 4 151. 6 136. 5 62 176. 7 176. 0														
25 26		16. 7	85 86	63. 2 63. 9	56. o	45 46	107. 8	97.0	05 06	152. 3 153. 1	137. 2	65	196.9	177.3 178.0	
27 28	19. 3 20. I	17.4 18.1	87	64. 7	57. 5 58. 2	47	100.5	97. 7 98. 4	07	153. 8	137. 8 138. 5	67 68	197. 7	178.7	
	20. 8 21. 6	18. 7	88 89	65. 4 66. I	58. 9	47 48	110.0	99.0	% 8	154.6	110.2		199.2	179. 3 180. 0	
29 30	22. 3	19. 4 20. 1	3	66. 9	58. 9 59. 6 60. 2	49 50	110. 7	99- 7 100- 4	10	155. 3 156. 1	139. 8 140. 5	69 70	199. 9 200. 6	180.7	
31	23.0	20. 7	91	67. 6 68. 4	60. 9 61. 6	151	112. 2	101.0	211	156.8	141.2	271	201.4	181. 3	
32 33	23. 8 24. 5	21.4 22. I	92 93	68.4 69.1	61.6	52 53	113.0	101. 7	12	157. 5 158. 3	141.9 142.5	72 73	202. I 202. 9	182. 0 182. 7	
34	25. 3	22. 8	94	69.9	62. 9 63. 6	54	1144	103. 0	14	159.0	143. 2	74	203.6	183. 3	
35 36	26. 0 26. 8	23. 4 24. I	95 96	70.6 71.3	63. 6 64. 2	55 56	115. 2	103. 7 104. 4	15	159. 8 160. 5	143.9	75 76	204. 4 205. I	184. 0 184. 7	
37	27. 5	24.8	97 98	72. I	64.0	57 58	116. 7	105. 1	17 18	161.3	145. 2	77	205. 9	185. 3	
37 38	28. 2	25.4 26.1		72.8	65. 6 66. 2	58	117.4 118.2	105. 7		162. 0	145. 9	77 78	206.6	186. o 186. 7	
39 40	29. 0 29. 7	26.8	99 100	73.6 74.3	66.9	59 60	118.9	106. 4 107. I	19 20	162. 7 163. 5	146. 5 147. 2	72	207. 3 208. I	187.4	
41	30. 5	27.4 28.1	IOI	75. 1	67. 6 68. 3	161	119.6	107. 7	221	164. 2	147. 9 148. 5	281	208.8	188.0	
42 43	31. 2 32. 0	28. I 28. 8	02	75. 8 76. 5	68. g	62 63	120. 4 121. I	108.4 109. I	22 23	165. o 165. 7	140.2	82 83	209.6	188. 7 189. 4	
44	32. 7	29.4	04	77.3 78.0	63. 9 69. 6	64	121. 9	109. 7	24	166.5	149. 9 150. 6	8ă	21 I. I	190.0	
45 46	33- 4 34- 2	30. I 30. 8	1 25 1	78. o 78. 8	70. 2	65 66	122. Č 123. 4	110. 4 111. 1	25 26	167. 2	150.6	85 86	211.8	190. 7	
47	34-9	31.4	37	79-5	70. 9 71. 6	67 63	124. I	111.7	27 28	168.7	151. 9 152. 6	ž	213.3	192.0	
47	35- 7	32. I 32. 8	.08 .00	80. 3 81. 0	72. 3	63 69	124.8	112.4		169. 4 170. 2	152.6	88 89	214.0	192.7	
49 50	36. 4 37. 2	33. 5	10	81.7	72. 9 73. 6	70	125. 6 126. 3	113.1	29 30	170.9	153. 2 153. 9	90	215.5	193.4 194.0	
51	37. 0 38. 6	24 7	111	82. 5	74. 3	171	127. 1	114.4	231	171.7	154.6	29I	216. 3	194-7	
52 53	38.6	34.8	12	84.0	74.9	72 73	127. 8 128. 6	115. 1	32 33	172. 4 173. 2	155. 2	92 93	217.0	195.4 196.1	
4	40.1	35. 5 36. I	14	83. 2 84. 0 84. 7 85. 5	74.9 75.6 76.3	74	229. 3	115.8 116.4	34	173. 9 174. 6	155. 9 156. 6	94	217.7 218.5	196.7	
\$\$ \$6	40. 9 41. 6	36.8	15	85. 5	77.0	75 76	130. I 130. 8	117. 1	34 35 36	174.6	157. 2	95 96	219. 2	197.4 198.1	
57 58	42.4	-8 -	17	86. o.∣	78.3	77	131. 5	118.4	37 38	175.4	157. 9 158. 6	97 98	220. 7	198.7	
58	43. I 43. 8	38. 8 39. 5	18	87.7 88.4	70.0	75	132. 3 133. 0	119. I 119. 8	38 39	176.9	140. 3	98	221. 5	199- 4	
59 60	44.6	39. 3 40. I	80	89. 2	79.6 80.3	79 80	133. 8	120.4	40	178.4	150. 6	300	222. 9	200.7	
Dıst.	Dep.	Let.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat.	
												[For	48 Deg	rees.	

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DIFFERENCE OF LATITUDE AND DEPARTURE FOR Dist Dep. Dep. Dep. Dep. Ļat Dist. Let Dist. Lat 88. 5 89. 2 90. 0 164. 165. 165. 166. a. 7 1. 5 a. 7 6 121 82. 5 83. 9 84. 6 85. 9 86. 6 87. 3 88. 0 181 123. 4 176. 3 132. 4 24 Í 42. 3 43. 0 43. 6 133. 1 133. 8 134. 6 135. 3 136. 0 136. 8 1. 4 62 4546.8 5 3 4 4 4 4 4 5 5 1 . 2 82 83 84 85 86 124. I 124. 8 177. 0 177. 7 178. 5 179. 2 179. 9 180. 6 181. 4 182. 1 182. 8 22 43 44 45 46 47 48 49 50 2.4 2. 0 63 64 65 66 23 74 274196 2734 125. 5 126. 2 24 ġa. 7 44 45 45 46 91 4 92 2 92 9 93 6 94 3 95 1 25 3 126. 2 126. 9 127. 5 128. 2 167. 8 168. 5 169. 1 169. 8 170. 5 4 8 5 5 6 8 67 68 69 4 27 28 87 88 89 5 2 47. 128. 29 9 6 7.3 70 47- 7 30 88. 7 90 139. 0 89. 3 90. 0 90. 7 7·5 8·2 8·9 48. 4 49. 1 49. 8 50. 5 51 1 51 8 171. 2 171. 9 g o 7177374757778798 51. 9 52. 7 53. 4 54. 1 54. 9 55. 6 57. 8 57. 8 58. 5 131 32 95. 8 90. 5 97. 3 98. 0 98. 7 99. 5 100. 2 100. 9 101. 7 102. 4 191 251 52 53 54 55 55 57 58 59 60 183. 6 184. 3. 185. 0 185. 8 186. 5 187. 2 188. 7 188. 7 189. 4 139. 7 140. 4 141. 2 141. 9 142. 6 143. 3 144. 1 144. 8 145. 5 140. 3 130. 3 130. 9 131. 6 132. 3 133. 0 133. 7 134. 4 135. 0 135. 7 136. 4 8. 8 171. 9 172. 5 173. 2 173. 9 174. 6 175. 3 176. 6 177. 3 9. 5 10. 2 93 94 95 97 98 99 200 33 34 35 36 37 38 39 40 9 5 10 2 91. 4 92. 8 93. 4 94. 8 95. 5 50. 51 52 53 54 11.0 11. 7 12. 4 13. 2 13. 9 14. 6 10. 9 11. 6 5 2 93-4 94-1 91-8 95-5 96-2 96-8 97-5 98-2 12. 3 13. 0 13. 6 13. 13. 9 190. 9 191. 6 192. 3 193. 1 193. 8 194. 5 195. 3 81 82 83 84 85 86 87 88 89 90 59. 2 60. 0 60. 7 61. 4 62. 2 55. 2 55. 9 56. 6 103. I 103. 9 104. 6 105. 3 106. 0 261 178. 0 178. 7 179. 4 180. 0 180. 7 14.3 15.0 15.7 16.4 17.0 17.7 18.4 19.1 19.8 20.5 201 147 137. 1 137. 8 138. 4 139. 1 139. 8 140. 5 141. 2 141. 9 142. 5 143. 2 15. 4 16. 1 16. 8 17. 6 18. 3 19. 0 19. 7 141 0 147. 7 148. 5 149. 2 149. 9 150. 7 151. 4 02 63 64 65 66 67 68 69 70 42 43 44 45 40 90. a 97. 5 98. 2 98. 9 99. 6 100. 3 100. 9 03 57.3 53.0 58.7 59.3 04 17. 6 18. 3 19. 0 19. 7 20. 5 21. 4 21. 9 ું 62. 2 63. 6 64. 4 65. 1 65. 8 181, 4 182: I 106. 8 107. 5 27 47 48 49 50 182. 8 60. 7 61. 4 183. 5 184. 1 184. 8 185. 5 186. 2 109. 0 109. 7 09 196. L97. 7 96,308 52 0 7 42 9 102. 3 110. 4 111. 2 111. 9 112. 6 154. 155. 155. 156. 198. 2 198. 9 199. 7 200. 4 201. I 62. I 22. 7 23. 4 24. 1 24. 9 25. 3 27. 8 27. 8 28. 5 21. 1 91 92 93 94 95 96 97 98 51 52 53 54 55 57 58 59 103. 0 21 [143. 9 144. 6 145. 3 145. 9 140. 6 147. 3 148. 7 148. 7 149. 4 150. 0 271 72 103. 7 104. 3 105. 0 67. 3 68. 9 68. 7 69. 5 70. 2 70. 9 71. 7 72. 4 73. I 62. 7 63. 4 64. 1 64. 8 65. 5 66. 8 12 22. 5 23. 2 23. 9 24. 6 25. 2 13 7374757777898 186. 187. 188. 14 15 16 96 318 53 5 2 113. 4 114. 1 11 . 8 115. 6 116. 3 105. 7 106. 4 107. 1 107. 8 108. 4 157. 158. 158. 159. 201. 9 202. 6 203. 3 204. 0 204. 8 188. 189. 17 8 25. 26. 9 67. 68. 116. 3 117. 0 4 19 20 190. 3 191. 0 5 2 160 29. 109. 68. 9 69. 6 70. 2 70. 9 71. 6 117. 7 118. 5 119. 2 109. 8 110. 5 111. 2 111. 8 161. 6 281 205. 22 I 5 191.6 162. 4 163. 1 163. 8 164. 6 165. 3 02 192. 3 193. 0 22 23 24 207. 0 193.

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[For 47 Degrees.

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DIFFERENCE OF LATITUDE AND DEPARTURE FOR 44°.															
	υ 	IFFE	REN	ICE C)F. L	ATTI	ODE	AND	DE	PART	URE	FOR	44°.		
Dist.	Let.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat.	Dep.	Dist.	Lat	Dep.	Dist.	Lat.	Dep.	
1 2	0.7 1.4	0.7	61 62	43. 9 44. 6	42.4	121 22	87.0	84. I 84. 7	181 82	130. 2	125. 7 126. 4	241 42	173-4 174-1	167.4	
3	1. 4 2. 2	1.4 2.1	63	45.3 40.0	43. I 43. 8	23	87. 8 88. 5	85. 4 86. 1	82	130. 9 131. 6	127. 1	43	174.8	168, 8	
4	2.9 3.6	2.8	64	46.8	44-5	24	89.2	86. 1 86. 8		132. 4	127. 8 128. 5	44	175. 5 176. 2	169. 5 170. 2	
ş	4.3	3.5 4.8	65 66	47.5	45. 2 45. 8	25 26	89.9 90.6	87. 5 88. 2	85 86	133. I 133. 8	129, 2	45	177.0	170.9	
3	€.0	4.9	67 68	47.5 48.2	45. 8 46. 5	27 28	91.4	88.2	87 88	134.5	129.9 130.6	47	177.7 178.4	171.6 172.3	
اۋا	6.5	6.1	69	48.9 49.6	47. 2 47. 0	29	92. 1	88. 9 89. 6	89	135. 2 136. 0	131.3	49	179.1	173.0	
10	7. 2	6.9	70	50.4	47. 9 48. 6	30	93-5	90, 3	90	136. 7	132.0	50	179.8	173-7	
11	7.9	7. 6 8. 3	71 72	51. I 51. 8	49. 3 50. 0	131 32	94. 2 95. 0	91.0 91.7	191 92	137.4 138.1	132. 7 133. 4	251	180. 6 181. 3	174-4 175-1	
13	0.4	9.0	73	52. 5	50.7	33	95. 7 96. 4	92.4	93	138,8	134. I	53	182. 0	175 7	
14	10. I 10. 8	9. 7 10. 4	74 1	53. 2 54. 0	51.4 52.1	34	96. 4 97. I	93. I 93. 8	94	139.6	134.8	54	182. 7 183. 4	175.4	
15 16	11.5	11. 1	75 76	54-7	52.8	35 36	97.8	94.5	95 96	141.0	135. 5	52 53 54 55 56 57 58	184.2	177.8	
17	12. 2 12. 9	11.8	77 78	55.4	53- 5 54- 2	37 38	98. 5 99. 3	95.2	97 98	141.7	1 1 16, 8	57	184. 9 185. 6	178.5	
19	10 12.7 12.2 70 66.8 64.0 20 100.0 06.6 00 142.1 123.2 60 186.2 170														
20	20 14.4 13.9 80 57.5 55.0 40 100.7 97.3 200 143.9 138.9 60 137.0 180.														
21	15.1	15.3	82	59.0	57. 0	42	102, 1	97. 9 98. 6	201	144.0	140. 3	62	187. 7 188. 5	182.0	
23	15. 8 16. 5	15. 3 16. 0	81	59. 7 60. 4	57. 7 58. 4	43	102, 9 103, 6	99-3	03	145. 3 146. 0	141.0	63	180.2	182. 7	
24	17. 3 18. 0	16.7	84 8c	61.1	59.0	44	103. 0	100, 0	04	146. 7	141.7	64	189. 9 190. 6	183. 4 184. I	
25 26	18. 7	17. 4 18. I	85 86	61.9	59. 7 60. 4	45 46	105. 0	101.4	05	147. 5 148. 2	143. I	65 66	191.3	184.8	
27 28	19. 4 20. 1	18, 8 19, 5	87 88	62. 6 63. 3	60. 4 61. 1	47 48	105. 7 100. 5	102, I 102, 8	97 98	148. 9 149. 6	143. 8 144. 5	67 63	192. I 192. S	185. 5 186. 2	
29	20.9	20, 1	89	64.0	61.8	49	107. 2	103. 5	09	150.3	145. 2	69	193. 5	186.9	
30	21.6	20. 8	90	64. 7	62. 5	50	107.9	104. 2	10	151.1	145.9	70	194. 2	187.6	
31 32	22, 3 23, 0	21. 5 22. 2	91 92	65. 5 66. 2	63. 2 61. 9	151 52	108, 6	104. 9 105. 6	211	151.8	146.6	271 72	194. 9	188. 3 188. 9	
33	23.7	22. 9 23. 6	93	66. 9 67. 6 68. 3	63. 9 64. 6	53	110, 1	106. 3	13	153.2	147.3 148.0	73	195. 7 196. 4	189.6	
34 35 36	24. 5 25. 2	23.6 24.3	94	68. 2	66.0	54	110.8	107. 0	14	153.9 154.7	148.7	74 75 76	197. 1	190, 3	
36	25. 9 26. 6	25.0	95 96	69. 1 69. 8	66. 7	55 56	112.2	107. 7 163. 4	15 16	155. 4 156. I	150.0	76	197. 8 198. 5	191. 7	
37 38	20, 0	25. 7 26. 4	97 98	70.5	67. 4 68. 1	57 58	112.9	109. 1	17	156. I 156. 8	150.7	77 78	199. 3	192, 4 193, I	
39	27. 3 28. 1	27. 1	99	71.8	68, 8	59 60	114.4	110.5	19	157. 5 158. 3	152. 1	79	200. 7	193.8	
40	28, 8	27. 8 28. 5	100	71.9	69.5		115.1	111. 1	20		152. 8	80 28t	201.4	194. 5	
41 42	29. 5 30. 2	29. 2	101	72. 7 73. 4	70. 2 70. 9	161 62	115.8	112.5	22 I 22	159. 0 159. 7	153. 5 154. 2	82	202. 1	195. 2 195. 9	
43	30.9	29. 9 30. 6	03	74-1 74-8	71.5	63	117.3	113.2	23	159. 7 160. 4	154.9 155.6 150.3	83	202. 9 203. 6	195. 9 196. 6	
45	31. 7 32. 4	31. 3	04	74. 8	72. 2 72. 9	8	118. 7	113.9 114.6	24 25	161. Í 161. o	155.0	83 84 85 86	204. 3.	197. 3 158. 0	
45	33-1	32.0	05 06	75. 5 76. 3	72. 9 73. 6	65	119.4	115.3	25 26	162.6	1 57. 0	86	205. 7 200. 5	198. 7	
47	24.5	32. 6 33. 3	07 08	77. 0 77. 7	74- 3 75. 0	67 68	120. 1	116.0	27 28	163. 3 164. 0	157. 7 158. 4	87 83	200. 5	199. 4 200. I	
49	35. 2 36. 0	34.0	09	77. 7 78. 4	75. 7	69	121, 6	317.4 118.1	29	164. 7	150.1	89	207. 9	200, 8	
50 51	36, o 36, 7	34-7	111	79. F 79. 8	76. 4 77. I	70 171	122. 3 123. 0	118.1	30 231	165. 4 166. 2	159. 8 160. 5	90 291	208.6	201. 5 202. I	
52	37-4	35. 4 36. 1	12	80.6	77.8	72	123. 7	119.5	32	166. 9 167. 6	161. 2	92	210, 0	202, 8	
53	37·4 38. 1 38. 8	36, 8	13 14	81. 3 82. 0	78. 5 79. 2	73	124. 4 125. 2	120, 2 120, 9		167. 6 168. 3	161. 9 162. 6	93 94	210.8 211.5	203. 5 204. 2	
53 54 55 56	39.6	37. 5 38. 2	14 15 16	82. 7	79. 9 80. 6	74 75 76	125. 2 125. 9 126. 6	121,6	33 34 35 36	169.0	162.3	94 95 96	212.2	204. 9 205. 6	
56	40.3	38. 9 39. 6		82.4	80.6	76	126, 6	122, 3	36	169.8	163. 9 164. 6	96	212. 9 213. 6	205.6	
57 58	41. 0 41. 7	40.3	17	84. 2 84. 9	81. 3 82, 0	77 78	127. 3 128. 0	123.0	37 38	170.5	165. 1	97 98	213. 0 214. 4	200, 3	
8	42.4	41.0	19	85.0	82, 7	72	128, 8	124.3	39	171.9	165. 3	99	215. 1	207.7	
\vdash	43. 2	41.7	20	86. 3	83. 4		129. 5	125. 0	40	172.6	166. 7	300	215.8	208. 4	
Dist.	Dep.	Lat.	Dist.	Dep.	Lat	Dist.	Dep.	Lat.	Dist.	Dep.	Let	Dist.	Dep.	Lat.	
												[For	46 Deg	1008.	
							157	,							
								-	1						

DIFFERENCE OF LATITUDE AND DEPARTURE FOR 45°.

Dist	Let.	Dep.	Dist.	Let.	Dep.	Dist.	Let.	Dep.	Dist.	Lat.	Dep.	Dist.	Let.	Dep.			
1	0.7	9.7	61	43-1	43. I 43. 8	121	85. 6 83. 3	85.6 86.3	181	128.0	128.0	241	170.4	170.4			
2	1.4	1.4	6a 63	43.8 44.5 45.3	43.8	23	83.3	86. 3 87. 0	82	128. 7	128.7	42 43	171.1	171.1			
3 4	2. I 2. 8	2.8	23	46.3	44-5 45-3 46-0	24	87.0 87.7 88.4	87. 7 88. 4	84	129.4 130.1	130.1	44	172. 5	172.5			
š	3-5	3.5 4.2	45.8		46.0	15	88.4	88.4	ಪ್ರತ್ಯಕ್ಷಣ	130.8	130.8	45 46	173. 2	173.2			
	4.3	4.2	66	46.7	46. 7		89. i 89. 8	89. i 89. 8	80	131.5	131.5 132.2	40	173. 9 174. 7	173-9 174-7			
3	35 42 49 57	42	67 68	47.4 48.8 48.8	12:1	7	90.5	90.5	97 88	132.0	132.9 133.6	47 48	175.4	175.4			
9	6.4	\$.7 6.4	69	48.8	48.8	29	91.2	91.2	89	133.6	133.6	49	175.4 176.1 176.8	175. 4 176. 1 176. 8			
11	7. 1	7.1	70	49.5	49. 5 50. 2	30	91.9	91.9	90 191	134.4	134.4	50					
1 11	7.8	7.8	71 72	50, 2 50, 0	50.0	131 32	92.0	92.6	92	135. 1	135. 1 135. 8 136. 5	251	177.5 178.2	177. 5 178. 2			
13	9.9 9.9 10.6 11.3	9.2	73	50.9 51.6	50. 9 51. 6	33	93-3 94-0 94-8	93-3 94-0 94-8 95-5 96-2	93	135.8 136.5	136. 5	53	178.9 179.6 180.3	178. 9 179. 6 180. 3			
4	9.9	10.8	74 75 70 77 78 79	52. 3 53. 0 53. 7	52. 3	34	94.8	94.8	94	137. 2	137.2	54	180.3	179.0			
15 16	11. 1	11.3	75	53.7	53.0 53-7	35 36	95.5 96.2	22.3	95 96	137.9 138.6	137.9 138.6	꿇	181.0	181.0			
17	12. 0	12.0	77	54-4 55-2	54-4	37 38	96.9 97.6 93.3	00.0	97 98	139. 3	139.3	57	181.7	181.7			
18	13.7	12. 7	78	55.2	55. 2	38	97.6	97.6 98.3	98	140.0 140.7	140.0	58	182. 4 183. I	182. 4 183. i			
30	13. 4 14. Î	13.4	1 K	54-4 55-2 55-9 56-6	54-4 55-2 55-9 56-6	39 40	99.0	99.0	200	141.4	141.4	88 82 82 82 8 8 8 8 8 8 8 8 8 8 8 8 8 8	183.8	183.8			
1	14.8	14.8	81	57·3 58.0 58.7	57.3 58.0 58.7	141	99. 7 100. 4	99-7 100-4	201	142. 1	142. I 142. 8	261	184.6	184 6			
22	15.6	15. 6 16. 3	82	58.0	58.0	42	100.4	100.4	02	142.8	142.8	62	185. 3 186. 0	185.3			
73	15. 6 16. 3 17. 0	17.0	83 84 85 85	50.7	50.4	43	101. 1	101. 1	93 94	143. 5	143. 5	88.85	186.7	185. 3 186. 0 186. 7			
25 26	17. 7 18. 4	17. 7	85	59.4 60.1	59. 4 60. 1	45	102.5	102. 5 103. 2	8	144. 2 145. 0	144. 2 145. 0	65	187. 4 188. i	187. 4 188. i			
20	18.4	18. 4 19. 1	85	60. 8 61. 5	60. 8 61. 5	46	103. 2	103. 2	80	145. 7 146. 4	145.7 140.4	60	188. 1	183.8			
27	19. I 19. 8	19. I 19. 8	87 88	62.2	62.2	47	103.9	103.9	97 98	147. 1	147. I	67 68	189. 5	180.5			
29	20. 5 21. 2	20.5	89	62.0	62. 9 63. 6	49	105. 4 106. I	105. 4 106. I	09 10	147.8 148.5	147. 8	69	190, 2	100.2			
30	21.2	21.3	90	63.6	64. 3	50	100, 1	106.8	211			70	190. 9 191. 6	190.9			
31	21. 9 22. 6	21.0	91 92	64. 3 65. 1 65. 8 66. 5	64, 3 65, I	151 53	107. 5	107. 5	12	149. 2	149. 2	271 72	192. 3	102. 3			
33	22.2	23.3	93	65.8	65. 1 65. 8 66. 5	53	107. 5 108. 2	107. 5 108. 2 108. 9 109. 6	13	149. 9 150. 6 151. 3	149. 9 150. 6	73	193.0	193.0			
33 34 35 36	24.0	24.0	94 95 96	66.5	67. 2	54	108.9	108.9	14	151.3	151.3 152.0	74	193. 7 194. 5	193. 7			
38	24.7 25.5 20.2	24.7 25.5	23	67. 2 67. 9	67. 9 68. 6	33	210.3	110. 2	15 16	152.7	152. 7	13	195. 2	194. 5 195. 2			
37 38	20.2	26. 3	97 98	68.6	68.6	53 54 55 56 57 58	111.0	111.0	17 18	153.4	153.4	7374 7576 7778	195. 9 196. 6	195. 9 196. 6			
35 39	20.0	26.9 27.6	98 99	69.3 70.0	69. 3 70. 0		111.7	111.7	18	154. 1	154. 1	.78	190.0	190.0			
40	20. 9 27. 6 28. 3	27. 6 28. 3	100	70.7	70.7	8	112.4 113.1	113. i	19 20	154. 9 155. 6	154. 9 155. 6	79	197.3 198.0	197. 3 198. 0			
41	20.0	29.0	101	71.4	71.4	161	11128	113.8	221	156. g	156. 3	281	198. 7	198.7			
42	27.7 30.4 31.1	29.7	œ	72. F	72.1	62	114.6	114.6	23 23	157.0	157.0	8a 83	199. 4 200. I	199. 4 200, I			
43 44	31.1	30. 4 31. I	93 94	72.5	73.5	1 &	115.3	115. 3 116. 0	24	157. 7 158. 4	157. 7 158. 4	84	200. 8	200,8			
45	31.5	31.8	8.8	72. 8 72. 8 73- 5 74- 2 75- 0	73- 5 74- 2	17455 6455	116.7	1116.7	25 26	150.1	159. I 159. 8 160. 5	8 8 8 8 8	201.5	201.5			
1 42	32. 5	32. 5 33. 8	, e	75.0	75.0	67	117.4 118.1 118.8	117.4 118.1 113.8	20	159. 8 160. 5	159.8	87	202. 2				
43	33. 8 33. 9 34. 6	33.9	3	78.4	16.4	67 68	118.8	113.8	27 28	161.2	101.2	88	202. 9 203. 6	202. 9 203. 6			
49	34.6	34.6	99	75. 7 76. 4 77. 1 77. 8	75. 0 75. 7 70. 4 77. 1 77. 8	69	119.5	119. 5 120. 2	29 30	161.9 162.6	161.9 162.6	89	204. 4 205. I	204. 4 205. I			
50	35. A 36. I 36. 8	35.4 36.1 36.8	111	77. 6	78.5	171	120, 2	120. 2	221	163. 3	163. 3	90 29 1	205. 8	205.8			
51 52 53	36.8	36.8	12	78.5 79.2	79.2	72	120.9 121.6	120. 9 121. 6	231 32 33 34 35 36 37 38	164.0	164.0	03	205. 8 206. 5	205. 8 200. 5			
53	37.5	37. 5 38. 2	13	20.8	79.2 79.9 80.6	73	122. 3	122. 3	33	164.8	164.8	93	207. 2	207.2			
54	35.5	35.3	14	81.3	81.3	1 74	123.0 123.7	123. 0 123. 7	34	165. 5 166. 2	165. 5 166. 2	94	207. 9	207. 9 208. 6			
54 55 50 57 58	37:5 38.9 39.6	30.6	15 16	89.6	82.0	73 74 75 77 78	124.5	124.5	36	166. a	166.0	95 96	209.3	209.3			
57	40.3 41.0	40.3 41.0	73	82.7	82.7 83.4	77	125.2	125. 2	37	167. 6 168. 3	167.6	97 98	210.0 210.7	210.0			
39 58	41.7	41.7	19	82. 7 83. 4 84. 1	I84⊾ II	72	125. 9 126. 6	125. 9 126, 6	39	169.0	169.0 169.7	99	211.4	211.4			
60	42.4.	42.4	20	84.9	84.9	86	127. 3	127. 3	40	169.7	169. 7	300	212. 1	212. i			
Dist.	Dep.	Lat.	Dist.	Dep.	Let.	Dist.	Dep.	Lat.	Dist.	Dep.	Lat. Dist Dep. Lat.						
				-							[For 45 Degrees.						

TABLE II. REFRACTION, DIP, AND PARALLAX

REFRACTION, DIP, AND PARALLAX.

pparent titude.	ac-	pparent Utitude. efrac- tion.	pparent Altitude. Refrac- tion.	pparent Altitude. efrac- tion.	pparent Altitude. efrac- tion.		THE SEA
App	Refrac	Appare Altituc	Appare Altituc Refraction.	Appare Altituc	Appare Altitud	Height	Dip of
	1	9 30 5 35	15 0 3 34	25 0 2 4	42 0 1 5	of the Eye.	the Ho- rizon.
0 0 0 1 0 0 2 0 0 2 0 0 1 0 0 2 0 0 0 0	36 293 24 53 31 14 25 4 53 31 14 25 14 25 14 25 26 11 11 14 14 19 9 86 88 9 9 14 19 9 9 86 8 34 16 8 8 28 28 8 10 10 8 5 7 7 5 44 9 7 7 48 7 7 88	35 5 32 40 5 29 45 5 27 50 5 24 55 5 5 17 10 5 5 17 10 5 5 17 10 30 5 5 17 10 4 44 11 30 4 45 11 0 4 47 15 4 49 10 4 43 11 30 4 39 4 33 40 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	10 8 32 20 3 29 30 3 27 40 3 25 50 3 22 16 0 3 20 10 3 18 20 3 14 40 3 12 50 3 10 17 0 3 8 10 3 6 20 3 5 30 3 3 1 10 3 6 20 3 5 30 3 2 20 3 5 30 3 3 5 30 3 2 20 3 5 30 3 2 30 3 2 30 3 3 5 30 3 3 5 30 3 3 5 30 3 2 5 30 3 3 5 30 3 2 5 30 3 2 3 5 30 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	10 2 8 20 2 2 2 30 2 1 40 2 1 1 50 2 0 26 0 1 59 30 1 56 40 1 55 50 1 54 10 1 53 20 1 54 10 1 53 20 1 54 10 1 53 20 1 54 10 1 55 30 1 51 40 1 51 50 1 50 28 0 1 49 40 1 46 29 0 1 48 40 1 46 20 1 30 40 1 46 40	20 1 1 3 40 1 1 3 40 1 1 2 20 1 1 2 40 1 1 0 20 0 59 45 0 0 58 20 0 55 40 0 0 54 40 0 53 48 0 0 52 49 0 9 50 50 0 0 0 49 55 0 0 0 49 55 0 0 0 49 55 0 0 0 45 55 0 0 0 49 55 0 0 0 45 55 0 0 0 45	Ft. 1 2 3 4 4 5 6 7 7 8 9 9 10 11 12 13 14 14 15 16 17 18 19 20 21 22 22 4 25	0 59 1 28 1 58 1 58 2 24 2 36 2 56 3 15 3 24 2 36 3 15 3 24 3 40 3 55 4 09 4 16 3 4 29 4 34 4 44 4 44 4 44
50 55 7 0 5 10 15 20 25	7 53 7 28 7 24 7 19 7 14 7 10 7 6 7 1	50 4 31 55 4 29 12 0 4 27 5 4 26 10 4 24 15 4 22 20 4 20 25 4 19	40 2 42 50 2 40 20 0 2 39 10 2 37 20 2 36 30 2 35 40 2 33 50 2 32	20 1 85 40 1 84 32 0 1 83 20 1 82 40 1 31 33 0 1 29 20 1 28 40 1 27	58 0 0 36 59 0 0 35 60 0 0 33 61 0 0 32 62 0 0 31 63 0 0 30 64 0 0 28 65 0 0 27	26 27 28 29 30	5 00 5 06 5 11 5 17 5 22 N'S PAR-
7 30 35 40 45	6 57 6 53 6 49 6 45	12 30 4 17 35 4 15 40 4 13 45 4 12	21 0 2 31 10 2 29 20 2 28 30 2 27 40 2 26 50 2 24	34 0 1 26 20 1 25 40 1 24 35 0 1 23	66 0 0 26 67 0 0 25 68 0 0 23 69 0 0 22	ALLAX	IN ALTI-
50 55 8 0	6 41 6 37	50 4 10 55 4 9 18 0 4 7		20 1 22 40 1 21 36 0 1 20	70 0 0 21 71 0 0 20 72 0 0 19	Sun's Alt.	Sun's Parallax.
5 10 15	6 29 6 25 6 22	5 4 5 10 4 4 15 4 2	10 2 22 20 2 21 30 2 20	20 1 19 40 1 18 37 0 1 17	73 0 0 18 74 0 0 17 75 0 0 15	D .	S.
20 25 8 30 35 40 45 50 55 9 0 15 20 25 9 80	6 19 6 15 6 12 6 8 6 5 6 2 5 59 5 56 5 52 5 49 5 44 5 44 5 48 5 48 5 58	20 4 1 13 30 3 58 25 3 56 40 3 55 45 3 54 50 3 52 50 3 47 20 3 44 40 3 39 50 3 34 41 40 3 39 50 3 34 15 0 3 34	40 2 19 23 0 2 16 10 2 15 20 2 14 30 2 13 40 2 12 50 2 11 24 0 2 10 20 2 8 30 2 7 40 2 6 50 2 5	20 1 16 40 1 15 38 0 1 14 20 1 13 40 1 12 39 0 1 11 40 1 10 40 0 1 9 20 1 8 40 1 8 41 0 1 7 20 1 6 40 1 5	76 0 0 14 77 0 0 13 78 0 0 12 79 0 0 11 80 0 0 10 81 0 0 9 82 0 0 8 83 0 0 8 84 0 0 6 85 0 0 5 86 0 0 4 87 0 0 3 88 0 0 2 89 0 0 1 90 0 0	0 10 20 30 40 55 60 65 75 80 85 60	9988876544882210

TABLE III. DECLINATION OF THE SUN, 1886-1901.

DECLINATION OF THE SUN FOR THE YEARS 1886, 1890, 1894, 1898.

	South.	<u> </u>	FEE	3.	MAE	•	A DD						
-	uth.	9			l		APR	IL.	MA	¥.	Ju		
	88	Diff. on hour.	Dec. South.	Diff. one hour.	Dec. South North.	Diff. one hour.	Dec. North.	Diff. one hour.	Dec. North.	Diff. one hour.	Dec. North.	Diff. one hour.	و.
Days.	,		• /	"	. ,	<u>"</u>	。 <i>'</i>	<u>"</u>	• /	"	。,		Days.
2 22 8 22 4 22	2.59 2.54 2.48 2.42 2.85	+18 14 15 16 +17	17.02 16.44 16.27 16.09 15 51	+48 44 44 45 +46	7.80 7.07 6.44 6.21 5.58	+57 57 57 58 +58	4.87 5.00 5.23 5.46 6.09	58 57 57	15.08 15.26 15.44 16.01 16.18	+45 45 44 43 +48	22.05 22.13 22.20 22.28 22.34	19 18 17	1 2 8 4 5
7 22 8 23 9 22	2.28 2.21 2.18 2.04 1.55	18 19 20 22 +23	15.82 15.14 14.55 14.85 14.16	46 47 48 48 49	5.84 5.11 4.48 4.24 4.01	58 58 58 59 +59	6.82 6.54 7.17 7.89 8.01	56 56 56	16.35 16.52 17.08 17.25 17.40	42 41 41 40 +89	22.41 22.47 22.52 22.57 23.02	12	6 7 8 9 10
18 21 14 21	1.46 1.86 1.26 1.16 1.05	24 25 26 27 +28	18.56 18.86 18.16 12.55 12.55	49 50 51 51 +52	8.87 8.14 2.50 2.26 2.08	59 59 59 59 +59	8 28 8.45 9.07 9.29 9.50	54 54	17.56 18.11 18.26 18.40 18.55	38 38 37 36 +35	23.10 23.14 23.17 23.20	9	11 12 18 14 15
17 20 18 20 19 20	0.58 0.42 0.80 0.17 0.04	29 80 81 82 +83	19.15 11.54 11.33 11.11 10.50	58 53 53 +54	1.89 1.15 0.53 0.28 0.04	59 59 59 59 +59	10.12 10.32 10.54 11.15 11.85	58 53 52 52 +51	19.09 19.22 19.86 19.49 20.01	84 84 83 82 +81	28,22 28 24 23,25 28,26 28,27	5 4 8 2 +1	16 17 18 19 20
22 19 23 19 24 19	9.51 9.87 9.28 9.09 8.54	84 85 35 86 +87	10.28 10.06 9.44 9.22 9.00	54 55 55 55 +56	0.19 0.43 1.07 1.80 1.54	59 59 59 59 +59	11.56 12.16 12.36 12.56 13.15	51 50 50 49 +49	20.18 20.25 20.87 20.48 20.59	80 89 88 88 +27	23.27 23.27 28.26 23.25 23.24	0 -1 2 8 -4	21 22 28 24 25
27 18 28 18 29 17	3.89 3.24 3.08 7.52 7.85	88 89 40 41 +41	8.38 8.15 7.52 7.30	56 56 57 57	2.17 2.41 8.04 8.28 8.51	59 59 58 58 +58	18.85 18.54 14.18 14.81 14.50	48 48 47 46 +46	21.10 21.20 21.80 21.39 21.48	26 25 24 23 +22	28.22 28.20 23.17 28.14 28.10	5 6 7 8 -9	26 27 28 9 80
31 17 32 17	7.19 7.02	42 48		į	4.14 4.87	58 58	15.08	45	21.57 22.05	21 20	23.07	10	81 82

	JUL	Y.	Avet	7 8T.	SEP	т.	Oc	т.	No	▼.	Dr	o.	
	Dec. North.	Diff. one hour.	Dec. North.	Diff. one hour.	Dec. North South.	Diff. one hour.	Dec. South.	Diff. one hour.	Dec. South.	Diff. one hour.	Dec. South.	Diff. one hour.	
Days.	• /	<u>"</u>	• /	"	۰,	"	۰,	"	。 /	"	• ,	<u>"</u>	Days.
1 2 8 4 5	28.07 28.02 22.58 22.52 22.47	-10 11 12 18 -14	17.59 17.44 17.28 17.12 16.56	-38 89 89 40 -41	8.18 7.52 7.80 7.07 6.45	-54 55 55 55 -56	3.16 3.89 4.02 4.25 4.48	-58 58 58 58 -58	14.80 14.49 15.08 15.27 15.45	-48 47 47 46 -45	21.51 22.00 22.09 22.17 22.25	-23 22 21 20 -19	1 2 3 4 5
6 7 8 9 10	22.41 22.85 22.28 22.21 22.14	15 16 17 18 -19	16 40 16.23 16.06 15.49 15.82	41 42 43 48 - 44	6.23 6.00 5.38 5.15 4.52	56 56 56 57 57	5.12 5.85 5.57 6.20 6.48	58 57 57 57 -57	16.03 16.21 16.39 16.56 17.13	45 44 48 43 -42	22.89 22.45 22.51 22.57	18 17 15 14 -18	6 7 8 9 10
11 12 18 14 15	22.06 21.58 21.49 21.40 21.81	20 21 22 23 -24	15.14 14.56 14.38 14.19 14.01	45 45 46 46 —47	4.80 4.07 3.44 3.21 2.58	57 57 57 58 -58	7.06 7.28 7.51 8.18 8.36	57 56 56 56 -55	17.29 17.46 18.02 18.18 18.88	41 40 40 39 -88	28.02 23.06 23.10 28.14 23.17	12 11 10 9 -7	11 12 18 14 15
16 17 18 19 20	21.21 21.11 21.01 20.59 20.89	25 26 26 27 -28	18.42 13.23 13.08 12.44 12.24	47 48 48 49 -50	2.85 2.11 1.48 1.25 1.01	58 58 58 58 -58	8.58 9.20 9.42 10.03 10.25	55 55 54 54 54	18.48 19.08 19.17 19.81 19.45	37 36 36 85 -84	28.90 28.92 23.94 28.96 28.97	6 5 4 8 -2	16 17 18 19 20
21 22 23 24 25	20.27 20.15 20.08 19.51 19.38	29 30 81 82 -32	12.04 11.44 11.24 11.08 10.42	50 50 51 51 -58	0 80 0.15 0.08 0 82 0.55	58 58 58 58 -58	10.46 11.08 11.29 11.50 12.10	53 58 52 52 -52	19.58 20.11 20.24 20.36 20.48	38 32 31 30 -29	23.27 22.27 23.26 23.25 23.25	0 +1 2 8 +4	21 22 28 24 25
26 27 28 29 30	19.25 19.11 18.57 18.43 18.29	83 84 85 86 —36	10.22 10.01 9.40 9.18 8.57	58 58 58 58 -54	1.19 1.42 2.06 2.28 2.52	58 58 58 58 -58	12.81 12.51 13.12 13.32 13.51	51 50 50 -49	21.00 21.11 21.21 21.82 21.42	28 27 26 25 -24	28.22 23.20 28.17 23.18 23.10	5 7 8 9 + 10	26 27 28 29 80
81 83	18.14 17.59	37 38	8.35 8.18	54 54	8.16	58	14.11 14.80	49 48	21.51	. 23	28.05 28.01	11 12	81 82

DECLINATION OF THE SUN FOR THE YEARS 1887, 1891, 1895, 1899.

	Jan.		Fei	в.	Mai	R.	APR	ш	MA	Y.	Jun	E.	
	Dec. South.	hour.	Dec. South.	Diff. one hour.	Dec. South North	Diff. one hour.	Dec. North.	Diff. one hour.	Dec. North.	Diff. one hour.	Dec. North.	Diff. one hour.	و
Days.	۰,	"	• /	"	。,	"	。,	"	。 /	"	• /	"	Days.
1 2 3 4 5	22.55 22.50 22.44	+12 18 15 16 +17	17.06 16.49 16.81 16 13 15.55	+48 43 44 45 +46	7.85 7.12 6.49 6.26 6.08	+57 57 57 58 +58	4.82 4.55 5.18 5.40 6.04	+58 58 57 57 +57	15.04 15.22 15.40 15.57 16.14	+45 45 44 48 +43	22.08 22.11 22.19 22.26 22.33	+20 19 18 17 +17	1 2 3 4 5
6 7 8 9 10	22.80 22.23 22.15 22.06 21.58	18 19 20 21 +22	15.87 15.18 14.59 14.40 14.21	46 47 47 48 +49	5.40 5.17 4.58 4.80 4.06	58 58 58 59 +59	6.26 6.49 7.11 7.84 7.56	57 56 56 56 +55	16.81 16.48 17.04 17.21 17.86	42 41 41 40 +89	22.89 22.45 22.51 22.56 23.01	16 15 14 18 +12	6 7 8 9 10
11 12 13 14 15	21.48 21.39 21.29 21.18 21.08	23 24 26 27 +28	14.01 18.41 18.21 13.01 12.40	49 50 50 51 +51	3.48 3.19 2.56 2.89 2.06	59 59 59 59 +59	8.18 8.40 9 02 9.24 9 45	55 55 54 54 +54	17.52 18.07 18.22 18.87 18.51	39 38 37 36 +85	23.05 23.09 23.13 23.16 23.19	10 10 8 7 +6	11 12 18 14 15
16 17 18 19 20	20.56 20.45 20.83 20.20 20.07	29 30 31 82 +32	12.20 11.59 11.38 11.16 10.55	52 52 53 53 +54	1.45 1.21 0.57 0.84 0.10	59 59 59 59 +59	10.06 10.28 10.49 11.09 11.80	58 53 52 52 +51	19.05 19.19 19.89 19.45 19.58	85 34 83 32 +81	23.21 23.23 23.25 23.26 23.27	5 4 8 2 +1	16 17 18 19 20
21 22 28 24 25	19.54 19.41 19.27 19.12 18.58	33 34 85 36 +37	10.33 10.12 9.50 9.28 9.05	54 55 55 55 +56	0.14 0.87 1.01 1.24 1.48	59 59 59 59 +59	11.51 12.11 12.81 12.51 13.10	51 50 50 49 +49	20.10 20.28 20.84 20.46 20.57	30 30 29 28 +27	23.27 23.27 23.26 23.25 23.24	0 -1 2 8 -4	21 22 28 24 25
26 27 28 29 30	18.48 18.27 18.12 17.56 17.89	38 39 89 40 +41	8.48 8.20 7.58 7.85	56 56 57 57	2.12 2.85 2.59 3.22 3.45	59 59 59 59 +58	13.30 13.49 14.08 14.27 14.45	48 48 47 47 +46	21.07 21.17 21.27 21.87 21.46	26 25 24 28 22	23, 22 23, 20 23, 18 23, 15 28, 11	5 6 7 8 -9	26 27 28 29 39
81 82	17.28 17.06	42 48			4.09 4.82	58 58	15.04	45	21.55 22.08	21 20	23.08	10	81 82

	Ju	L¥.	Αυ	G.	SEP	T.	Oc	T.	No	v.	Dr	c.	
	Dec. North.	Diff. one hour.	Dec. North.	Diff. one hour.	Dec. North South.	Diff. one hour.	Dec. South.	Diff. one hour.	Dec. South.	Diff. one hour.	Dec. South.	Diff. one hour.	
Days.	。,	"	• /	<i>"</i>	• /	"	۰,	"	• /	"	۰,	"	Days.
1 2 3 4 5	23.08 23.08 22.59 22.54 22.48	-10 11 12 18 -14	18.03 17.48 17.82 17.16 17.00	-88 88 89 40 -41	8.19 7.57 7.85 7.18 6.51	-54 55 55 55 -56	3.10 8.38 3.56 4.20 4.48	-58 58 58 58 -58	14.26 14.45 15.04 15.22 15.41	-48 47 47 46 -46	21.49 21.58 22.07 22.15 22.28	-23 22 21 20 -19	1 2 8 4 5
6 7 8 9 10	22.43 22.36 22.80 22.23 22.15	15 16 17 18 19	16.44 16.27 16.10 15.53 15.86	41 42 42 43 43 –44	6.28 6.06 5.43 5.21 4.58	56 56 56 57 -57	5.06 5.29 5.52 6.15 6.87	58 57 57 57 57 -57	15.59 16.17 16.84 16.52 17.09	45 44 44 48 -42	22.80 22.87 22.44 22.50 22.55	18 17 16 15 -18	6 7 8 9 10
11 12 18 14 14	22.08 22.00 21.51 21.42 21.88	20 21 22 23 23	15.18 15.00 14.42 14.24 14.05	44 45 46 46 —47	4.85 4.12 3.49 3.26 8.08	57 57 57 58 -58	7.00 7.28 7.45 8.08 8.80	57 56 56 56 -55	17.25 17.42 17.58 18.14 18.29	41 41 40 89 -38	23.01 23.05 28.10 23.18 23.17	12 11 10 9 -8	11 12 18 14 15
16 17 18 19 20	21.28 21.13 21.08 20.52 20.41	24 25 26 27 -28	18.46 18.27 13.08 12.48 12.29	47 48 48 49 - 49	2.40 2.17 1.54 1.80 1.07	58 58 58 58 -58	8.52 9.14 9.86 9.58 10.20	55 55 55 54 -54	18.44 18.59 19.14 19.28 19.42	87 87 36 85 -84	28.20 28.22 28 24 28.25 23.26	7 5 4 8 -2	16 17 18 19 20
21 22 23 24 25	20.80 20.18 20.06 19.54 19.41	29 30 81 81 -82	12.09 11.49 11.28 11.08 10.48	50 50 51 51 -52	0.44 0.20 0.08 0.26 0.50	58 58 58 58 58	10,41 11,02 11,24 11,45 12,05	58 58 52 52 - 52	19.55 20.08 20.21 20.83 20.45	38 32 31 80 -29	28.27 23.27 28.27 23.26 23.26	1 +0 2 8 +4	21 22 23 24 25
26 27 28 29 80	19.28 19.14 19.01 18.47 18.88	88 84 85 35 -86	10.27 10.06 9.45 9.23 9.02	58 58 58 58 -54	1.18 1.85 2.00 2.28 2.47	58 58 58 58 58 -58	12.26 12.46 18.07 13.27 18.47	52 51 50 50 -49	20.57 21.08 21.19 21.29 21.39	28 27 26 25 -24	28.28 28.20 28.18 23.14 28.10	5 6 7 9 +10	26 27 28 29 80
31 82	18.18 18.08	87 38	8.40 8.19	54 54	8.10	58	14.06 14.25	49 48	21.49	28	23.06 23.09	11 12	81 82

DECLINATION OF THE SUN FOR THE YEARS 1888, 1892, 1896, 1900.

	JAI	N.	FE	R.	MAR	CH	APE	RIT.	MA	v.	Ju	æ.	
	Dec. South.	Diff. one hour.	Dec. South.	Diff. one hour.	Dec. South. North	Diff. one hour.	Dec. North.	Diff. one hour.	Dec. North.	Diff. one hour.	Dec. North.	Diff. one hour.	
Days.	• /	"	• ,	<u>"</u>	. ,	"	. ,	"	• ,	"	• ,	<u>"</u>	Days.
1 2 3 4 5	28.02 22.57 22.51 22.45 22.39	+12 18 14 15 +17	17.10 16.53 16.85 16 18 16.00	+42 48 44 45 +45	7.17 6.55 6.82 6.09 5.46	+57 57 58 58 +58	4.49 5.12 5.85 5.58 6.21	57 57 57	15.17 15.35 15.53 16.10 16.27	+45 44 44 48 +42	22.09 22.17 22.24 22.31 22.38	+90 19 18 17 +16	1 2 3 4 5
6 7 8 9	22.32 22.24 22.17 22.08 22.00	18 19 20 21 +22	15.41 15.28 15.04 14.45 14.25	46 47 47 48 +49	5.22 4.59 4.85 4.18 8.49	58 58 59 59 +59	6.44 7.06 7.28 7.51 8.18	56 56 55	16.44 17.01 17.17 17.88 17.48	42 41 40 39 +89	22.44 22.49 22.55 28.00 28.04		6 7 8 9 10
11 12 13 14 15	21.51 21.41 21.81 21.81 21.10	28 24 25 26 +27	14.06 18.46 13.26 18.06 12.45	49 50 50 51 +51	3.25 3.01 2.38 2.14 1.50	59 59 59 59 +59	8.85 8.57 9.18 9.40 10.01	54 54	18.04 18.19 18.28 18.48 19.02	38 37 36 86 +35	23.08 23.12 23.15 23.18 23.21	10 9 8 7 +6	11 12 18 14 14
16 17 18 19 20	20.59 20.47 20.85 20.28 20.10	28 29 80 81 +32	12.25 12.04 11.48 11.21 11.00	52 52 53 53 +54	1.27 1.08 0.89 0.16 0.08	59 59 59 59 +59	10.28 10.44 11.05 11.25 11.46	52 52 51	19.16 19.29 19.42 19.55 20.08	34 33 32 81 +81	28.25 28.25 28.25 23.27 28.27	5 4 8 2 +0	16 17 18 19
21 23 23 24 24 23	19.57 19.44 19.80 19.16 19.01	88 34 85 35 +37	10.98 10.17 9.55 9.88 9.11	54 54 54 55 +56	0.82 0.55 1.19 1.48 2.06	59 59 59 59 +59	12.06 12.26 12.46 13.06 13.25	50	20.80 20.82 20.48 20.54 21.05	30 29 28 27 +26	28.27 28.27 23.26 23.25 23.25	-0 1 2 4 -5	21 22 28 24 25
23 27 28 29 80	18.46 18.81 18.15 18.00 17.48	88 88 89 40 +41	8.48 8.26 8.08 7.41 7.18	57 57 57 57 +57	2.80 2.58 8.16 8.40 4.08	59 59 58 58 +58	18.45 14.04 14.22 14.41 14.59	48 47 47 46 +45	21.15 21.25 21.85 21.44 21.58	25 24 23 23 +22	28.21 28.18 23.15 23.12 23.09	6 7 8 9 -10	26 27 28 29 30
\$1 \$ 2	17.27 17.10	41 42			4.96 4.49	57 57	15.17	45	22.01 22.09	21 20	28.04	11	81 82

	Jui	_	Αυ	a	SEP	,	Oo	,	No		DE	n.	
										_			
	Dec.l North.	Diff. one hour.	Dec. North.	Diff. one hour.	Dec. North South.	Diff. one hour.	Dec. South.	Duff. one hour.	Dec. South.	Diff. one hour.	Dec. South.	Diff. one hour.	
Days.	۰,	"	• /	"	• /	"	۰,	<u>"</u>	٠,		。,	"	Days.
1 2 8 4 5	23.04 23.00 22.55 22.50 22.44	-11 12 13 14 -15	17.51 17.86 17.20 17.04 16.48	-86 39 40 40 -41	8.02 7.40 7.18 6.56 6.84	-55 55 56 -56 -56	8.27 8.51 4.14 4.87 5.00	-58 58 58 58 -58	14.49 14.59 15.18 15.86 15.54	47	21.56 22.04 22.18 22.21 22.21	20	1 2 3 4 5
6 7 8 9 10	22.88 22.81 22.25 22.17 22.10	16 17 18 19 —20	16.81 16 15 15.57 15.40 15.23	42 48 44 -44	6.11 5.49 5.26 5.04 4.41	56 56 67 57 -57	5.28 5.46 6.09 6.82 6.55	58 57 57 57 -57	16.18 16.80 16.47 17.04 17.21		22 85 22 42 22 48 22 54 22 54	16 15 14	6 7 8 9 10
11 12 18 14 15	22.02 21.53 21.44 21.85 21.86	20 21 22 23 24	15.05 14.47 14.28 14.10 18.51	45 46 46 47 -47	4.18 3.55 8.32 8.09 2.46	57 58 58 -58	7.17 7.40 8.02 8.95 8.47		17.88 17.54 18.10 18.25 18.41	40	23.04 23.00 23.18 23.16 23.16	9	11 12 18 14 15
16 17 18 19 20	21.16 21.06 20.55 20.44 20.88	25 26 27 28 -29	18.82 18.18 19.58 12.84 12.14	- 42 - 42 - 42 - 43 - 43 - 43 - 43 - 43 - 43 - 43 - 43	2.28 1.59 1.86 1.18 0.50	58 58 58 -58	9.09 9.10 9.58 10.14 10.86	55 54 54	18.56 19.10 19.24 19.36 19.58	86 85 84	23.24 23.24 23.25 23.26 23.26	-1	16 17 18 19 90
21 22 23 24 25	20.21 20.09 19.57 19.44 19.81	29 30 31 32 83	11.54 11.84 11.18 10.58 10.82	50 51 51 59 -59	0.26 0.03 0.20 0.44 1.07	58 58 58 58 -58	10.57 11.48 11.89 12.66 12.81	58 52	20.05 20.18 20.86 20.42 20.64	81 31 80	23.27 23.27 23.26 23.26 23.25	+5	91 98 98 94 95
26 27 28 29 30	19.18 19.04 18.50 18.86 18.21	34 35 36	10.11 9.50 9.29 9.07 8.46	58 54	1.81 1.54 2.17 8.41 8.04	58 58 58 -58	12.41 18.69 13.22 13.49 14.01	50	21.05 21.16 21.27 21.87 21.46	27 26 25	23.18 23.18 23.16 23.19 28.07	8	96 97 98 99 80
81 83	18.07 17.51	87 88	8.94 8.02	54 55	8.27	58	14.91 14.40		21.56	23	23.06 22.56		81 82

Г	 I												
	Jan.	.	FEE	3.	MARC	H.	APR	IL.	MA	¥.	JUN	B.	
	Dec. South.	bour.	Dec. South.	Diff. one hour.	Dec. South. North	Diff. one hour.	Dec. North.	Diff. one hour.	Dec. North.	Diff. one hour.	Dec. North.	Diff. one hour.	
Days.	• /	″	• /	<u>"</u>	• /	"	• /	<u>"</u>	• /	″	•. <i>'</i>	·"	Days.
1 2 8 4 5	22.58 22.47 22.40	+18 14 15 16 +17	16.57 16.40 16.22 16.04 15.46	+43 44 44 45 +46	7.28 7.00 6.87 6.14 5.51	+57 57 58 58 +58	4.44 5.07 5.30 5.53 6.15	+58 57 57 57 +57	15.13 15.31 15.49 16.06 16.28	+45 44 44 48 +42	22.07 22.15 22.22 22.80 22.86	+20 19 18 17 +16	1 2 8 4 5
6 7 8 9 10	22.26 22.19 22.11 22.02 21.58	19 20 21 22 +23	15.27 15.08 14.49 14.80 14.11	47 47 48 48 +49	5.28 5.05 4.41 4.18 8.54	58 58 58 59 +59	6.38 7.01 7.23 7.45 8.08	56 56 56 56 +55	16.40 16.57 17.13 17.29 17.45	42 41 40 40 +39	22.42 22.48 22.54 22.59 23.08	18 12	6 · 7 8 9 10
11 12 18 14 14	21.44 21.84 21.24 21.13 21.02	24 25 26 27 +28	13.51 13.81 13.11 12.50 12.30	50 50 51 51 +52	8.31 8.07 2.43 2.20 1.56	59 59 59 59 +59	8.80 8.51 9.13 9.35 9.56	55 54 54 54 +58	18.00 18.15 18.80 18.44 18.59	38 37 37 36 +35	28.07 28.11 28.15 28.18 28.20	7	11 12 13 14 15
16 17 18 19 20	20.50 20.38 20.26 20.14 20.01	29 30 31 82 +33	12.09 11.48 11.27 11.05 10.44	52 53 53 54 +54	1.82 1.09 0.45 0.21 0.02	59 59 59 59 +59	10.17 10.89 10.59 11.20 11.41	58 52 52 52 +51	19.12 19.26 19.89 19.52 20.05	34 33 38 32 +81	23.22 23.24 23.26 23.26 23.27		16 17 18 19 20
21 22 23 24 25	19.47 19.88 19.19 19.05 18.50	34 35 86 37 +37	10.22 10.00 9.38 9.16 8.54	54 55 55 56 +56	0.26 0.49 1.18 1.37 2.00	59 59 59 +59	12.01 12.21 12.41 18.01 18.21	51 50 50 49 +49	20.17 20.29 20.40 20.51 21.02	30 29 28 27 +26	23.27 23.27 23.26 23.25 23.25	8	21 22 22 24 25 24 25 25 25 25 25 25 25 25 25 25 25 25 25
26 27 28 29 30	18.85 18.19 18.08 17.47 17.81	88 89 40 41 +42	8.31 8.09 7.46 7.23	56 57 57 57	2.24 2.47 8.11 3.34 8.57	59 59 58 58 +58	13.40 18.59 14.18 14.86 14.55	47 47	21.12 21.28 21.82 21.42 21.51	26 25 24 23 +22	28.21 23.19 23.16 23.18 23.09	6 7 8	26 27 28 29 30
81 82	17.14 16.57	42 48			4.21 4.44	58 58	15.18	45	21.59 22.07	21 20	23.05	10	31 32

		1		<u> </u>	1		
	JULY.	AUG.	SEPT.	Ост.	Nov.	DEC.	
	Dec. North. Diff. one	Dec. North. Diff. one	Dec. North South. Diff. one	Dec. South. Diff. one	Dec. South. Diff. one	Dec. South. Diff. one	
Days.	。/ "	• / //	• / "	• / //	• / "	。/ //	Days.
1 2 8 4 5	28.06 -11 28.01 12 22.56 18 22.51 16 22.45 -15	17.08 40	8.07 - 55 7.46 55 7.24 55 7.01 55 6.39 - 56	8.22 -58 3.45 58 4.08 58 4.81 58 4.55 -58	14.35 - 48 14.54 47 15.13 47 15.32 46 15.50 - 45	21.54 -28 22.02 22 22.11 21 22.19 20 22.27 -18	1 2 3 4 5
6 7 8 9 10	22.39 16 22.83 17 22.26 18 22.19 19 22.12 -20	16.19 42 16.01 43 15.44 43	6.17 56 5.54 56 5.32 56 5.09 57 4.46 -57	5.18 57 5.41 57 6.04 57 6.26 57 6.49 —57	16.08 45 16.26 44 16.43 43 17.00 43 17.17 -42	22.34 17 22.41 16 22.47 15 22.58 14 22.58 -18	6 7 8 9 10
11 12 18 14 15	22.04 20 21.55 21 21.47 22 21.38 23 21.28 -24	15.09 45 14.51 45 14.33 46 14.14 46 18.54 -47	4.23 57 4.01 57 3.38 57 3.15 58 2.51 -58	7.12 56 7.84 56 7.57 56 8.19 56 8.41 -55	17.34 41 17.50 40 • 18.06 89 18.22 89 18.37 —38	28.08 12 23.07 11 23.12 10 23.15 8 23.18 -7	11 12 18 14 15
16 17 18 19 20	21.18 25 21.08 26 20.58 27 20.47 28 20.36 —28	13.37 48 13.17 48 12.58 49 12.38 49 12.19 -50	2.28 58 2.05 58 1.42 58 1.19 58 0.55 —58	9.04 55 9.26 55 9.47 54 10.09 54 10.31 -54	18.52 87 19.07 36 19.21 35 19.35 84 19.49 - 84	23.21 6 23.28 5 23.25 4 23.26 2 23.27 -1	16 17 18 19 20
21 22 23 24 24 25	20.24 20.12 20.00 31 19.47 19.34 -33	11.59 50 11.89 51 11.18 51 10.58 51 10.87 -52	0.32 58 0.08 58 0.15 58 0.38 58 1.02 -58	10.52 58 11.13 58 11.34 52 11.55 52 12.16 -51	20.02 33 20.15 32 20.27 31 20.40 30 20.51 -29	28.27 +1 28.26 2 23.25 3 28.24 +5	21 22 23 24 25
26 27 28 29 30	19.21 88 19.08 34 18.54 85 18.39 86 18.25 —87	10.16 52 9.55 53 9.34 53 9.12 53 8.51 -54	1.25 58 1.48 58 2.12 58 2.35 58 2.58 -58	12.37 51 12.57 51 13.17 50 13.87 49 18.57 -49	21.03 28 21.14 27 21.24 26 21.84 25 21.44 -24	23.22 6 23.19 7 23.16 8 23.12 9 28.09 +10	26 27 28 29 30
81 82	18.10 87 17.55 88	8.29 54 8.08 55	3.27 58	14.16 48 14.85 48	21.53 28	23.04 12 22.59 13	31 32

TABLE IV. EQUATION OF TIME, 1886-1901.

EQUATION OF TIME FOR THE YEARS 1886, 1890, 1894, 1898.

	JAN.	FEB.	MAR.	APR.	MAY.	JUNE.	T	470	SEPT.	Ост.	Nov.	DEC.
			MAR.	APR.		JUNE.	JULY	AUG.	SEPT.	OCT.	NOV.	DEC.
ri e	Add to app. time.	Add to app. time.	Add to app. time.	Sub. from app. time.	Sub. from app. time.	Sub. from Add to app. time.	Add to app. time.	Add to app. time.	Sub. from app. time.	Sub. from app. time.	Sub. from app. time.	Sub. from Add to app. time.
Days.	M. 8	м. s.	M. S.	M. S.	M. S.	M. S.	M. S.	M. S.	M. S.	M. S.	M. S.	M. S.
1 2 3 4 5	8 58 4 21 4 49 5 16 5 48	18 51 18 58 14 05 14 10 14 15	12 30 12 18 12 05 11 52 11 88	3 54 8 36 3 18 3 00 2 48	8 02 8 10 8 16 8 22 8 27	2 27 2 18 2 08 1 58 1 47	8 83 8 44 8 55 4 06 4 17	6 05 6 01 5 57 5 52 5 46	0 08 0 27 0 48 1 05 1 25	10 21 10 40 10 58 11 17 11 85	16 18 16 18 16 18 16 18 16 16	10 44 10 21 9 58 9 83 9 09
6 7 8 9 10	6 10 6 86 7 02 7 27 7 51	14 20 14 28 14 25 14 27 14 28	11 24 11 10 10 55 10 40 10 25	2 25 2 08 1 51 1 84 1 18	8 32 8 87 8 41 8 44 8 46	1 87 1 26 1 14 1 08 0 51	4 27 4 37 4 47 4 56 5 04	5 40 5 88 5 25 5 17 5 09	1 45 2 05 2 26 2 46 8 07	11 52 12 09 12 26 12 42 12 58	16 14 16 10 16 06 16 02 15 56	8 48 8 18 7 51 7 25 6 57
11 12 13 14 14	8 15 8 88 9 01 9 28 9 44	14 28 14 27 14 26 14 24 14 21	10 09 9 53 9 86 9 19 9 02	1 02 0 46 0 30 0 15 0 00	8 49 8 50 8 51 8 51 8 51	0 89 0 27 0 15 0 02 0 10	5 18 5 20 5 28 5 84 5 41	4 59 4 49 4 89 4 28 4 17	8 28 8 49 4 10 4 31 4 52	18 14 18 29 18 48 18 57 14 11	15 49 15 42 15 34 15 25 15 15	6 30 6 02 5 34 5 05 4 36
16 17 18 19 20	10 05 10 24 10 44 11 02 11 20	14 17 14 13 14 07 14 02 13 55	8 45 8 27 8 10 7 52 7 84	0 15 0 29 0 48 0 57 1 10	8 49 8 48 8 45 8 42	0 23 0 36 0 49 1 02 1 14	5 46 5 52 5 57 6 01 6 04	4 05 3 52 8 39 8 26 8 12	3 14 5 35 5 56 6 17 6 38	14 24 14 36 14 47 14 58 15 09	15 04 14 52 14 40 14 26 14 12	4 07 3 38 3 06 2 38 2 09
21 22 23 24 25	11 37 11 53 12 08 12 23 12 36	18 48 18 40 13 32 13 23 18 18	7 15 6 57 6 89 6 20 6 02	1 22 1 85 1 47 1 58 2 09	8 89 8 85 8 80 8 25 8 20	1 27 1 40 1 53 2 06 2 19	6 08 6 10 6 12 6 14 6 15	2 57 2 42 2 27 2 11 1 55	6 59 7 20 7 41 8 02 8 22	15 18 15 27 15 86 15 48 15 50	18 57 18 41 18 24 13 07 12 49	1 39 1 09 0 38 0 08 0 22
26 27 28 29 30	12 49 13 02 13 13 13 24 13 83	18 03 12 53 12 42 12 30	5 43 5 25 5 07 4 48 4 80	2 19 2 29 2 38 2 47 2 55	8 14 8 07 8 00 2 52 2 44	2 32 2 44 2 57 3 09 3 21	6 15 6 15 6 14 6 13 6 11	1 39 1 22 1 04 0 47 0 29	8 43 9 03 9 23 9 42 10 02	15 56 16 02 16 07 16 10 16 14	12 30 12 10 11 50 11 29 11 07	0 51 1 21 1 51 2 20 2 49
81	18 42		4 12	8 02	2 86	8 88	6 08	0 11	10 21	16 16	10 44	8 18

EQUATION OF TIME FOR THE YEARS 1887, 1891, 1895, 1899.

	J	AN.	F	В.	M	LB.	A	R.	MA	Y.	Ju	JN	E.	Jυ	LY.	A	σ G.	SE	PT.	Oc	T.	No	v.	Dı	EC.
	Add to	app. time.	Add to	app. time.	Add to	app. time.	Add to	app. time.	Sub. from	app. time.	Sub. from	Add to	app. time.	Add to	app. time.	Add to	app. time.	Sub. from	app. time.	Sub. from	app. time.	Sub. from	app. time.	Sub. from	app. time
Days.	M.	8.	M.	8.	M.	8.	M.	s.	м.	8.	M	. 8	3.	M	. 8.	M	. s .	М	. s.	M	. 8.	M.	8.	М.	8.
1 2 8 4 5	4	47 15 43 10 87	18 18 14 14 14	57 04 09	12 12 12 12 11	21 09 56	8 8	59 41 23 05 47	8 8	00 07 14 20 26	200	26 11 10 10 50		8 4	80 42 58 04 14	5 5	06 02 58 52 47	0 0 1	04 23 42 02 21	10 11	17 86 55 18 82	16 16 16 16 16	20 20 19	10 10 9	51 28 04 40 16
8 9 10	6 7	04 30 55 20 45	14 14 14 14 14	22 24 26	11 11 10 10 10	14 59 44	2 1 1	29 12 55 88 21	8 8 8	81 86 40 43 46	1 1	81 21 11 01 54	P 7 8	444	25 84 44 58 02	5 5 5	41 84 26 18 10	2 2 2	41 02 22 42 03	12 12 12	49 07 28 40 56	16 16 16 16 16	18 09 04	8	51 25 59 32 05
11 12 18 14 15	8 8 9	09 32 55 17 38	14 14 14 14 14	27 25 28	9	12 56 89 28 06	0 0	05 49 33 18 08	8 8 3	48 50 51 52 52	0	0 41 0 18 0 0 0	0 8 6	5 5 5	10 18 25 82 89	444	01 51 41 80 19	8 4 4	24 45 06 27 48	18 18 18	11 26 41 55 08	15 15 15 15 15	45 86 27	5 5	87 09 41 12 48
18 19	9 10 10 10 11	38 57	14	17 18 08 08 57	8 8 7	48 81 13 56 38	0 0	12 26 40 53 07	8 8 8	51 50 48 46 43		9 20 9 40 9 50 1 1:	8 6 9	5 6	45 50 56 00 04	3 3 8	07 55 42 29 15	5 6	09 30 51 12 33	14 14 14	22 38 45 56 06	14	55 43	8 3	14 44 14 45 15
22 23 24	11 12 12 12 12	49 04 19	13 13 18	50 42 34 26 16	7 6 6	20 02 43 25 07	1 1 1	19 81 43 54 05	8 8	89 85 81 26 20	1	1 2 1 5 2 0 2 1	1	6 6 6	07 10 13 14 15	2 2	01 46 31 15 00	777	54 15 86 57 17	15 15 15	16 25 84 42 49	13 18 18	00 45 28 11 53	0	45 45 45 15
28 29	12 12 18 13 13	11 22	12 12	06 56 45 88	5 5 4	49 80 12 58 85	2 2 2	16 25 35 44 52	8 2	14 08 01 53 45	1	2 8 2 4 2 5 3 0 3 1	2 5 7	6	16 16 15 14 12	1 1 0	48 26 09 51 83	99	88 58 18 88 58	16 16 16	55 01 06 10 14	12 11 11	34 15 55 34 13	1 1 2	45 14 44 18 42
81	13	41			4	17	2	60	2	87	1	3 3	0	6	09	0	15	10	17	16	16	10	51	8	11

EQUATION OF TIME FOR THE YEARS 1888, 1892, 1896, 1900.

	JAN	FEB.	MAR.	APR.	May.	JUNE.	JULY.	AUG.	SEPT.	Ост.	Nov.	DEC.
	Add to	Add to app. time.	Add to app. time.	Add to Sub. from app. time.	Sub. from app. time.	Sub. from Add to app. time.	Add to app. time.	Sub. from app. time.	Sub. from app. time.	Sub. from app. time.	Sub. from app. time.	Sub. from Add to app. time.
Days.	M.S	M.S.	M. 8.	M. S.	M. S.	M. 8.	M. 8.	M. S.	M. 8.	M. 8.	M. 8.	M. S.
1 2 8 4 5	4 06 4 96 5 08	13 48 3 13 55 3 14 02 3 14 08 14 14	12 25 12 12 11 59 11 46 11 82	8 45 8 27 8 10 2 52 2 84	3 05 3 12 3 18 3 24 3 29	2 22 2 12 2 02 1 52 1 42	3 38 3 50 4 01 4 12 4 22	6 02 5 58 5 58 5 48 5 42	0 19 0 38 0 58 1 17 1 87	10 88 10 52 11 10 11 28 11 46	16 90 16 21 16 20 16 19 16 17	10 84 10 11 9 47 9 22 8 57
6 7 8 9	6 25 6 45 7 14	14 25	11 18 11 08 10 48 10 83 10 17	2 17 2 00 1 43 1 27 1 10	3 84 3 89 8 42 8 45 8 47	1 81 1 20 1 08 0 56 0 45	4 32 4 42 4 51 5 00 5 09	5 85 5 28 5 20 5 12 5 05	1 57 2 17 2 37 2 58 8 19	12 08 12 20 12 36 12 52 18 08	16 14 16 10 16 06 16 00 15 54	8 81 8 05 7 38 7 11 6 44
11 12 13 14 15	8 27 8 50 9 18	14 28	10 01 9 45 9 28 9 12 8 55	0 54 0 89 0 23 0 08 0 06	3 49 3 50 3 50 8 50 8 50	0 32 0 20 0 07 0 05 0 18	5 17 5 24 5 81 5 38 5 44	4 54 4 44 4 88 4 92 4 10	8 40 4 01 4 22 4 23 5 04	13 28 13 88 18 52 14 05 14 19	15 47 15 39 15 30 15 21 15 10	6 16 5 48 5 19 4 50 4 21
18 19	10 16 10 8 10 5	14 20 14 16 14 12 14 06 14 00	8 37 8 20 8 02 7 44 7 26	0 91 0 85 0 48 1 02 1 15	8 49 8 47 8 45 8 42 8 39	0 81 0 44 0 57 1 10 1 22	5 50 5 55 5 59 6 08 6 07	8 58 8 45 8 83 3 18 8 04	5 25 5 47 6 08 6 29 6 50	14 81 14 48 14 54 15 05 15 15	14 59 14 47 14 84 14 20 14 06	8 58 3 28 2 53 2 28 1 54
22 23 24	11 40 12 0 12 1	18 58 18 46 2 13 38 7 13 29 1 18 20	7 08 6 50 6 31 6 18 5 54	1 27 1 39 1 50 2 02 2 12	8 85 8 81 8 26 8 21 8 15	1 85 1 48 2 01 2 14 2 26	6 10 6 12 6 18 6 14 6 15	2 49 2 84 2 18 2 02 1 46	7 11 7 82 7 58 8 14 8 84	15 25 15 88 15 42 15 49 15 56	18 50 18 84 18 17 12 59 12 41	1 24 0 54 0 24 0 06 0 36
27 28 29	12 57 18 09 13 20	18 10 18 00 12 49 12 87 12 25	5 86 5 17 4 59 4 40 4 22	2 22 2 32 2 41 2 50 2 58	8 09 8 02 2 55 2 47 2 39	2 39 2 51 3 03 3 15 8 27	6 15 6 14 6 13 6 11 6 09	1 29 1 12 0 54 0 36 0 18	8 55 9 15 9 35 9 54 10 14	16 01 16 07 16 11 16 15 16 17	12 22 12 02 11 41 11 19 10 57	1 06 1 35 2 05 2 84 3 03
81	18 3		4 04	8 05	2 81	3 3 8	6 96	0 00	10 88	16 19	10 84	8 832

EQUATION OF TIME FOR THE YEARS 1889, 1893, 1897, 1901.

	Jar.	FEB.	MAR.	AFR.	May.	JUNE.	JULY.	Δυg.	SEPT.	Ост.	Nov.	DEC.
	Add to app. time.	Add to app. time.	Add to app. time.	Add to Sub. from app. time.	Sub. from app. time.	Sub. from Add to app. time.	Add to app. time.	Add to app. time.	Sub. from app. time.	Sub. from app. vione.	Sub. from app. time.	Sub. from Add to app. time.
Days.	M. S.	M.S.	M. S.	M.S.	M. S.	M. S.						
1	4 01	18 54	12 28	8 50	8 08	2 24	3 36	6 04	0 18	10 27	16 19	10 39
2	4 29	14 01	12 16	8 32	8 10	2 14	3 48	6 00	0 82	10 46	16 20	10 16
3	4 56	14 07	12 08	8 14	8 17	2 04	3 59	5 55	0 53	11 04	16 20	9 52
4	5 24	14 13	11 50	2 57	3 28	1 54	4 10	5 50	1 11	11 22	16 19	9 28
5	5 51	14 18	11 36	2 39	8 28	1 44	4 20	5 44	1 81	11 40	16 17	9 08
6	6 17	14 22	11 22	2 22	3 83	1 88	4 30	5 88	1 51	11 58	16 14	8 38
7	6 48	14 25	11 08	2 05	8 87	1 22	4 40	5 81	2 12	12 15	16 11	8 12
8	7 09	14 27	10 58	1 48	8 41	1 11	4 49	5 28	2 32	12 82	16 07	7 45
9	7 38	14 28	10 87	1 31	8 44	0 59	4 58	5 15	2 53	12 48	16 02	7 19
10	7 58	14 29	10 22	1 15	8 46	0 48	5 07	5 06	3 14	18 04	15 56	6 51
11	8 21	14 29	10 06	0 58	8 48	0 36	5 15	4 56	8 84	13 19	15 49	6 24
12	8 45	14 28	9 49	0 42	9 50	0 24	5 22	4 46	8 56	13 84	15 41	5 55
18	9 07	14 26	9 38	0 27	8 51	0 11	5 29	4 86	4 17	13 48	15 83	5 27
14	9 29	14 24	9 16	0 12	3 51	0 01	5 86	4 25	4 38	14 02	15 23	4 58
15	9 50	14 21	8 59	0 08	8 51	0 14	5 42	4 18	4 59	14 15	15 18	4 29
16	10 10	14 17	8 41	0 18	3 50	0 27	5 48	4 01		14 28	15 02	4 00
17	10 80	14 12	8 28	0 82	3 49	0 39	5 58	3 48		14 40	14 50	8 30
18	10 49	14 07	8 06	0 46	8 47	0 58	5 58	8 35		14 52	14 87	8 01
19	11 07	14 01	7 48	1 00	8 44	1 05	6 02	3 22		15 02	14 23	2 31
20	11 24	18 54	7 30	1 12	8 41	1 18	6 05	8 07		15 12	14 09	2 01
21	11 41	13 47	7 12	1 25	8 37	1 31	6 08	2 58	7 06	15 22	18 54	1 81
22	11 57	18 39	6 53	1 37	8 33	1 44	6 11	2 88	7 27	15 31	18 88	1 01
23	12 12	13 31	6 35	1 49	3 29	1 57	6 13	2 28	7 47	15 89	18 21	0 81
24	12 27	13 22	6 17	2 00	3 23	2 10	6 14	2 07	8 08	15 46	13 03	0 01
25	12 40	18 12	5 58	2 10	8 17	2 23	6 15	1 51	8 26	15 53	12 45	0 29
26 27 28 29 80	12 58 13 05 13 17 13 27 13 37	18 02 12 51 12 40 12 28	5 40 5 21 5 06 4 45 4 26	2 21 2 30 2 89 2 48 2 56	8 11 8 04 2 57 2 49 2 41	2 86 2 48 8 00 8 13 3 25	6 15 6 15 6 14 6 12 6 10	1 34 1 17 1 00 0 42 0 24	8 49 9 09 9 29 9 48 10 08	15 59 16 04 16 09 16 12 16 15	12 25 12 05 11 45 11 24 11 02	0 59 1 29 1 58 2 28 2 57
81	18 46		4 08		2 33		6 07	0 05		16 18	10 89	8 25

TABLE IVa. CORRECTION TO BE APPLIED TO EQUATION OF TIME.

` &	~∞4°	6895	2225	5558	2828	2222
* &	-840	20040	=525	5526	2882	£888
` &	65.4 ₹0	02-00	5554	5586	ខ្លួនន	8828
\$ °		er-80	5252	8728	2828	2882
· 8	-0004	600-301	2222	4585	28 2 2 2	8288
` 8	-000 4	10 to 00	8 518	4585	8582	ន្តនន្ត
, 48		∞~4œn	6513	82459	8587	2382
` %		00-100	8212	55 5 7 5	57.86	8288
÷ 81	-01004	-100a	802I	55545	127.7.8	2823
21,	∺ 0500.4	41006		=352	51 18 18	. <u>&</u> &&
` &	-000 00	4000	စာစာ ဇာ ဝ	5555	120	8858
19		4000	7-80G	2222	82459	138
18		4000	1-0000	2222	8445	127718
"		4400	60046	9211	5552	11665
16	00	8247070	9~~œ	96011	1388	4555
15		24470	84366	စာတစ င်	1122	8448
14		80 4 4 7O	7665	ထထထထ	2223	35 55 4
13	H-000	20244	-3@00	t-ထဲထမ	©22I	2828
12 ,		20244	ကက္ခ	C-0000	00 22	2223
* =	0	01 to 20 4	4550	9922	တတ္ထာတ	2222
101	08	64 to to to	4400	70 to 51-	\$~00000	8600
` 6	08	04040000	0244°C	2229	œ-1-1œ	80000
` ∞	0	0,0,0,0	80044	4000	&&&:-	r-r-0000
: 1-	0	-0000	∞∞∞4	4440	ကလေလသ	9944
, 9	0===	-2000	0,000	2244	4000	ဃဇာဇာ
2 10	00	0	6,0,0,0	00000	4444	4101010
. 4	0077		અજજ	0,0,00	ಯಬಬಲ	4444
≥ ∞	0007			80000	0,0,0,0	တက္ကေဘး
2 00	0000	0				અ ભ ભ અ
1	0000	0000	000=			
.moH	⊣%∞4	တက္တေ	∞ 2∺%	8248	8222	2882

Table V. SINES, TANGENTS, AND SECANTS.

0°											1790
М.	Hour a. M.	Hour r. n.	Sine.	Diff. 1'.	Conecant.	Tangent.	Dift. 1 .	Cotangent.	Secant.	Cosine.	ж.
٥	12 0 0	0 0 0	Inf. neg.		Infinite.	Inf. neg.		Infinite.	10,00000	10, 00000	60
1 1	11 59 52	08	6. 46373	30103	1,3. 53627	6. 46373	30103	13. 53627	00000	00000	59 58
3	59 44 59 36	0 24	76476 94085	17609	23524	76476 94085	17609	23524 05915	00000	00000	58
1 4	59 28	0 32	7.06579	969 i	12. 93421	7. 06579	9691	12, 93421	00000	00000	57 56
5	11 59 20	0 0 40	7. 16270	7918	12.83730	7. 16270	7918	12. 83730	10, 00000	10,00000	55
	59 12	0 48 0 56	24188 30882	6694 5800	75812 69118	24188 30882	6694	75812	00000	00000	54
7	59 4 58 56	1 4	36682	5115	63318	36682	5800	69118	00000	00000	53 52
9	58 48	I 12	41797	4576	58203	41797	4576	63318 58203	00000	00000	51
10	11 58 40	0 1 20	7-46373	4139	12. 53627	7. 46373	4139	12, 53627	10,00000	10.00000	50
11	58 32 58 24	1 28 1 36	50512 54291	3779 3476	49488 45799	50512 54291	3779-	49488	00000	00000	49 48
13	58 16	1 44	57767	3218	42233	57767	3476	45709 42233	00000	00000	47
14	58 8	1 52	60985	2997	39015	60986	2996	39014	00000	00000	46
15	11 58 0	0 2 0	7. 63982	2802	12. 36018	7. 63982	2803	12. 36018	10,00000	10,00000	45
17	57 52 57 44	2 8	66784 69417	2633 2483	33216 30583	66785 69418	2633 2482	33215 30582	00000	00000	44
18	57 36	2 24	71900	2348	28100	71900	2348	28100	00001	9-99999	43 42
19	57 28	2 32	74248	2227	25752	74248	2228	25752	10000	99999	7
20	11 57 20 57 12	0 2 40 2 48	7. 76475	2021	12, 23525	7. 76476	2119	12, 23524	10,00001	9- 99999	40
22		2 56	78594 80615	1930	21406 19385	78595 80615	2020 1931	21405 19385	10000	99999	39 38
23	56 56	3 4	82545	1848	17455	82546	1848	17454	10000	99999 99999	30
24	56 48	3 12	84393	1773	15607	84394	1773	15606	10000	99999	37 36
25 26	11 56 40 56 32	0 3 20	7. 86166 87870	1704	12, 13834	7. 86167	1704	12. 13833	10,00001	9- 99999	35
27	56 24	3 28 3 36	89509	1639	12130	87871 89510	1639 1579	12129	10000	99999	34
28	56 16	3 44	91088	1524	08912	91089	1524	08911	00001	99999	33 32
29	56 8	3 52	Ç2612	1472	07388	92613	1473	07387	00002	99998	31
30 31	11 56 o 55 52	0 4 0	7. 94084	1424	12. 05916	7. 94086	1424	12. 05914	10. 00002	9. 99998	30
32	55 44	4 16	95508 96887	1379 1336	04492	95510 96889	1379 1336	04490	00002	99998	29 28
33	55 36	4 24	98223	1297	01777	98225	1297	01775	00002	99998	27 26
34	55 28	4 32	99520	1259	00480	99522	1259	00478	00002	99998	
35 36	11 55 20 55 12	0 4 40 4 48	8.00779	1223	97998	8,00781	1223	97996	10, 09002	9. 99998	25
37 38	55 4 54 56	4 56	03192	1158	96808	03194	1159	96806	00003	99998	24 23
		5 4	04350	1128	95650	04353	1128	95647	00003	99997	22
39 40	54 48 11 54 40	0 5 20	05478	1100	94522	05481	1100	94519	00003	99997	21
41	54 32	0 5 20 5 28	8. 06578	1072	92350	8. 06581 07653	1072	92347	10, 00003	9- 99997	20
42	54 24	5 36	07650 08696	1022	91304	08700	1022	91300	00003	99997 99997	19 18
43	54 16 54 8	5 44 5 52	09718 10717	999	90282	09722	998	90278	00003	99997	17 16
44	11 54 0	0 6 0	8. 11693	976	11.88307	10720 8, 11606	976	89280 11.88304	00004	99996	
46	53 52	6 8	12647	954 934	87353	12651	955 934	87349	10.00004 00004	9. 99996 99996	15 14
47	53 44	6 16	13581	914 896	86419	13585	015	86415	00004	99996	13
48 49	53 36 53 28	6 24	14495 15391	896	85505 84609	14500	895 878	85500 84605	00004	99996	12
50	11 53 20	0 6 40	8. 16268	860	11.83732	15395 8, 16273	860	11.83727	10,00005	99996	11
51	53 12	6 48	17128	843	11. 83732 82872	17133		82867	00005	99995	
52	53 4	6 56	17971	827	82029	17133	843 828	82024	00005	99995	8
53 54	52 56 52 48	7 4	18798 19610	797	81202 80390	18804 19616	812	81196 80384	00005	99995	7
	11 52 40	0 7 20	8, 20407	782		8, 20413	797		19,00006	99995	5
55 56	52 32	7 28	21189	769	78811	21195	769	78805	00006	99994	1 4
57 58	52 24 52 16	7 36	21958	755	78042	21964	756	78036	00006	99994	3
50 59	52 16 52 8		22713 23456	743 730	77287	22720 23462	742 730	77280 76538	00006	99994	:
66	52 0	7 52 8 0	24186	717	76544 75814	24192	718	75808	00007	99994 99993	6
M.	Umr	Hame .	Cardini	210			<u> </u>		<u> </u>		-
	Hour P. M.	Hour A. M.	Cosine.	Diff. r'.	Secant.	Cotangent.	Diff. t'.	Tangent.	Concent.	Sine.	M.
30° °									0	ī	89°

our a. M.	1									
	Hour P. M.	Sine.	Diff. 1'.	Conecant.	Tangent.	Diff. x'.	Cotangent	Senist.	Cosine	1
52 0	080	8, 24186	717	11. 75814	8, 24192	718	11. 75808	10.00007	9. 99993	6
51 52	8 8	24903	700	75007	24910	706	75090	80007	99993	1 5
51 44	8 16	25000	695	74391	25016	696	74384	00007	99993	1.5
51 36	8 24	26304	684	73006	26312	684	73688	00007	99993	13
51 28	8 32	26988	673	73012	26996	673	73004	80000	99992	L
51 20	0 8 40	8, 27661	663	11, 72339	8, 27669	663	11, 72331	10,00008	9.99992	1
51 12	8 48	28324	653	71676	28332	654	71068	80000	99992	L
51 4	8 56	28977	644	71023	28986	643	71014	80000	99992	Ŀ
50 56	9 4	29621	634	70379	29629	634	79371	80000	99992	L
50 48	9 12	30255	624	69745	30263	625	69737	000009	99991	L
50 40	0 9 20	8, 30879	616	11,69121	8, 30888	617	11,69112	10,00009	9. 99991	8
50 32	9 28	31495	608	68505	31505	607	68495	000009	99991	и
50 24	9 36	32103	599	67897	32112	599	67888	01000	99990	ŀ
50 16	9 44	32702	590	67298	32711	591	67289	01000	99990	Ŀ
50 8	9 52	33292	583	66708	33302	584	66698	01000	99990	Ŀ
50 0	0 10 0	8. 33875	575 568	11.66125	8, 33886	575 568	11.66114	10,00010	99990	ŀ
49 52	10 8	34450	568	65550	34461	568	65539	00011	99989	и
49 44	10 16	35018	560	64982	35029	561	64971	11000	99989	1
49 36	10 24	35578	553	64422	35590	553	64410	11000	99989	Ŀ
49 28	10 32	36131	.547	63869	36143	546	63857	11000	99989	L
49 20	0 10 40	8, 36678	539	11.63322	8, 36689	540	11, 63311	10,00012	9. 99988	1
49 12	10 48	37217	533	62783	37229	533	62771	21000	99988	
49 4	10 56	37750 38276	526	62250	37762 38289	537	62238	00012	99988	L
48 56	11 4	38276	520	61724	38289	520	61711	00013	99987	ы
48 48	11 12	38796	514	61204	38809	514	61191	00013	99957	L
48 40	0 11 20	8. 39310	508	11.60690	8, 39323	509	11,60677	10,00013	9. 99987	П
48 32	11 28	39818	502	60182	39832	502	60168	41000	99986	L
48 24	11 36	40320	196	59680	40334	496	59666	41000	99986	13
48 16	11 44	40816	191	59184	40830	491	59170	00014	99986	L
48 8	11 52	41307	485	58693	41321	486	58679	00015	99985	Ŀ
48 o	0 12 0	8, 41792	480	11.58208	8, 41807	480	11, 58193	10,00015	9.99985	I.
47 52	12 8	42272	474	57728	42287	475	57713	00015	99985	ŀ
47 44	12 16	42746	470	57254	42762	470	57238	91009	99984	ŀ
47 36	12 24	43216	454	56784	43232	464	56768	00016	99984	ŀ
47 28	12 32	43680	459	56320	43696	460	56304	00016	99984	L
47 20	0 12 40	8, 44139	455	11.55861	8, 44150	455	11. 55844	10,00017	9. 99983	ŀ
47 12	12 48	44594	450	55406	446114	450	55389	00017	99983	н
47 4 46 56	12 56	45044	445	54956	45061	446	54939	00017	99983	ŀ
46 56	13 4	45489	441	54511	45507	441	54493	00018	99982	Ŀ
46 48	13 12	45930	436	54070	45948	437	54052	00018	99982	Ŀ
46 40	0 13 20	8, 46366	433	11.53634	8, 46385	432	11, 53615	10,00018	0.99982	ŀ
46 32	13 28	46799	427	53201	46817	428	55183	00019	99951	г
46 24	13 36	47226	424	52774	47245	424	52755	90019	99051	1
	13 44	47650 48069	410	52350	47669	420	52331	00019	99951	н
4	13 52		416	51931	48089	416	51911	00020	99980	L
46 0	0 14 0	8. 48485	411	11.51515	8. 48505	412	11.51495	10,00020	9, 99980	Г
45 52	14 8	48896	408	51104	48917	408	51083	00021	99979	E
45 44	14 16	49304	404	50090	49325	404	50675	00021	99979	Н
45 36	14 24	49708	400	50292 40892	49729	401	50271	00021	99979	И
-	14 32		396		50130	397	49870	00022	99978	L
45 20	0 14 40	8. 50504	393	11. 49496	8, 50527	393	11.49473	10,00022	9,99978	Г
45 12	14 48	50897	390 386	49103	50920	390	49080	00023	99977	1
45 4	14 56	51287	380	48713	51310	386	48690	00023	99977	1
44 56 44 48	15 4	51673	382	48327	51696	383	48304	00023	99977	Ĺ
	-	52055	370	47945	52079	380	47921	00024	99976	L
44 40	0 15 20	8, 52434	376	11.47566	8, 52459	376	11.47541	10,00024	9, 99976	
				47190		373				П
44 24	15 30		309		53208	370				1
				40448						1
	15 52	53919	303							
	10 0	54202	300	45/10	34,300	301	45092	00020	99974	ĺ
44 0						min i		4	71.7	1
44 44 44	32 24 16 8	32 15 28 24 15 36 16 15 44 8 15 52 0 16 0	32 15 28 52810 24 15 36 53183 16 15 44 53552 8 15 52 53919 0 16 0 54282	32 15 28 528 6 373 24 15 36 53183 369 16 15 44 53552 367 8 15 52 53919 363 0 16 0 54282 360	32 15 28 528 0 373 47190 24 15 36 53183 369 46817 16 15 44 53552 367 46448 8 15 52 53919 363 46081 0 16 0 54282 360 45718	32 15 28 5 2810 373 47190 5255 24 15 36 53183 369 46817 53208 16 15 44 53552 307 4648 53578 8 15 52 53919 363 46081 53945 0 10 0 54282 360 45718 54308	32 15 28 52876 373 47190 52835 373 24 15 36 53183 369 46817 5120 370 16 15 44 53352 367 46448 53578 367 8 15 52 53919 363 46681 53944 363 0 16 0 54282 360 45718 54308 361	32 15 28 52850 373 47169 3285 373 47165 24 15 36 46817 3308 370 46717 3308 370 4672 370 4642 367 367 4642 3577 367 4642 367 367 4642 367 4642 367 367 4642 367 4642 367 367 4642 367 4642 367 367 4642 367 4642 367 367 4642 367 367 367 <td>32 15 28 52810 373 47190 52835 373 47165 00025 24 15 36 53183 369 46817 53208 370 46792 00025 16 15 44 53552 367 46445 53578 367 46422 00026 68 15 52 53919 363 46681 53944 305 46755 00026 0 16 0 54282 360 45718 54308 361 45692 00026</td> <td>32 15 28 52870 373 47190 52835 373 47165 00025 99973 24 15 36 53183 369 46817 53208 370 46792 00025 99975 16 15 44 53552 367 46448 53578 367 46422 00026 99974 8 15 52 53919 363 46681 53945 309 46925 00026 99974</td>	32 15 28 52810 373 47190 52835 373 47165 00025 24 15 36 53183 369 46817 53208 370 46792 00025 16 15 44 53552 367 46445 53578 367 46422 00026 68 15 52 53919 363 46681 53944 305 46755 00026 0 16 0 54282 360 45718 54308 361 45692 00026	32 15 28 52870 373 47190 52835 373 47165 00025 99973 24 15 36 53183 369 46817 53208 370 46792 00025 99975 16 15 44 53552 367 46448 53578 367 46422 00026 99974 8 15 52 53919 363 46681 53945 309 46925 00026 99974

go.				_						-	177
M.	Houra. M.	Hour r.ac.	Sine.	Diff. r'.	Cosecant.	Tangent,	Diff. r'.	Cotangent.	Secant	Cosine	N
0	11 44 0	0 10 0	8, 54282	360	11. 45718	8, 54308	36r	11.45692	10,00026	9 99974	6
Ĭ.	43 52	16 8	54642	357	45353	54669	358	45331	00027	99973	5
2	43 44	16 16	54999	355	45001	55027	355	44973 4461S	00007	99973	5
3	43 36	16 24	55354	351	44646	55382	352	44018	00028	99972	5
4	43 28	16 32	55705	349	44295	55734	349	4,266		99972	
5	11 43 20	0 10 40	8, 56054	346	11, 43946	8, 56083 56429	346	11. 43917	10,00029	9-99971	1 5
	43 12	16 48 16 56	56400	343	43000	56773	344	43571	00010	99971	3
7	43 4 43 50	16 56	56743 57084	341	43257 42916	57114	341	43886	00030	99970	3
ŏ	42 48	17 12	57421	336	42579	57452	336	42548	15000	99969	Ŀš
0	11 42 40	D 17 20 4	8. 57757	332	EL. 42243	8, 57788	333	11, 42212	10,00031	9. 99969	T:
ī	42 32	17 28	8. 57757 58089	330	41911	53121	330	41879	00032	99968	H
2	42 24	17.36	58419	328	41581	58451	328	41549	00032	99968	
3	42 15	17 44	58747	325	41253	58779	326	41221	00033	99967	н
4	42 8	17 52	59072	323	40928	59105	323	40895	доозз	99967	18
5	II 42 0	0 18 0	8, 59395	320	11.40605	8, 59428	.321	11.40572	10,00033	9. 99967	Þ
6	41 52	18 8	59715	318	40285	59749	319	40251	00034	99966	14
7 8	41 44	13 15	60033	316	39967	60068	316	39932	00034	99966	В
	41 36	18 24	60349	313.	39651	60384	314	39016	00035	99965	ŀ
9	41 28	18 32	60662	311	39338	60698	311	39302	00036	99964	Ŀ
0	11 41 20	0 18 40	8. 60973	309	11. 39027	8, 61009	310	11. 38091	10,00036	9-99964	ŀ
ı	41 12	18 48	61282	397	38718	61319	307	38681	00037	99963	
2	41 4	18 56	61589	305	33411	61626	395	38374	00037 00038	99963 9996a	L
3	40 56	19 4	61894	302	35106 37804	62234	303	37766	00038	99962	Ŀ
4	40 48	19 12					_				
5	11 40 40	0 19 20	8, 62497	298	11. 37503	8, 62535	299	37166	10, 00039	9, 99961	l
	40 32	13 23	62795	294	37205 36909	63131	295	36869	00040	99960	L
7	40 24 40 16	19 36	63385	293	36615	63426	293	3657A	00040	99960	L
9	40 8	19 44	63678	200	36322	63718	201	36574 36283	00041	99959	L
	II 40 0	0 20 0	8, 63968	288	11, 35032	8, 64000	280	11. 35991	10,00041	9- 99959	t
I	39 52	20 8	64256	287	35744	64208	287	35702	00042	99958	в
2	39 44	20 16	64543	284	35457	64585 64870	285	35415	00042	99958	в
3	39 36	20 24	64827	287	35173	64870	284	35130	00043	99957	ı
4	39 28	20 33	65110	281	34890	65154	281	34846	00044	99956	Ŀ
5	11 39 20	0 20 40	8, 65391	279	11. 34609	8. 65435	280	11. 34505	10, 00044	9. 99956	В
5	39 12	20 43	65670	277	34330	65715	278	34285	00045	99955	I.
7	39 4	20 56	65947	276	34053	65993	276	34007	00045	99955	ı
3	39 4 38 56	21 4	66223	274	33777	66269	274	33731	00046	99954	Ŀ
9	38 48	21 12	66497	272	33503	66543	273	33457	00046	99954	1
0	11 38 40	0 21 20	8.66769	270	11. 33231	8, 66816	271	11. 33184	10,00047	9. 90953	ı
t.	38 32	21 28	67039	269	32961	67087	269	32913	00048	99952	ı
2	38 24	21 36	67308	267 266	32692	67356	266	32644	00049	99952	ı
3	38 15	21 44	67575 67841	261	32425	67624	264	32376	00049	99951	F
4	38 8	21 52			32159		-		10,00050	9-99959	t
5	11 38 0	0 22 0	8, 68104	263	11. 31896	8, 68154 68417	263	31583	12,00050	999949	ı
ě	37 52	22 8	68367 68627		31633	68678	260	31303	12000	99949	ŀ
78	37 44	22 24	68886	259 258	31373	68938	258	31062	00052	99948	L
9	37 36 37 28	22 33	69144	256	30856	69196	257	30804	00052	99948	L
0	11 37 20	0 22 40	8, 69400	254	11, 30600	8, 69453	255	11. 30547	10,00053	0. 99947	Ť
1	37 12	22 48	69054	253	30346	69708	254	30292	00054	99946	ı
2	37 4	22 56	69907	252	5,000,7	69962	252	30038	00054	99946	1
3	40 56	23 4	70150	250	29841	70214	251	29786	00055	99945	1
4	36 48	23 12	70409	249	29591	70465	249	29535	00056	99944	L
9	11 36 40	D 23 20	8, 70658	247	11. 29342	8, 70714	248	11.29286	10,00056	9.99944	
ő	36 32	23 28	70905	245	20095	70962	246	29038	00057	99943	1
7	30 24	23 36	71.151	244	28849	71208	245	28792	00058	99942	П
8	36 16	23 44	71395 71638	243	28605	71453	244	28547	00058	99942	1
59	36 8	23 52	71638	242	28362	71697	243	28303 28060	00059	99941	П
90	35 0	24 0	71880	240	28120	71940	241	20000	00000	99940	L
_	Hour p. at.	Hour A. M.	Cosine.	Diff. r	Secant.	Cotangent.	Diff. c'.	Tangent.	Cosecant	5ine.	1
ME.											

SINES.	TANGENTS,	AND	SECANTS.
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30											176°
¥.	Hour A. M.	Houry. M.	Sine.	Diff. 1'.	Coscent.	Tangent.	Diff. r'.	Cotangent.	Secant,	Couine.	M.
	11 36 0	0 24 0	8, 7i88o	240	11. 28120	8. 71940	241	11. 28060	10. 00060	9. 99940	60
1	35 52	24 8	72120	239	27880	72181	259	27819	00060	99940	59 58
3	35 44 35 36	24 I6 24 24	72359 72597	238	27641 27403	72420 72659	239 237	27580 27341	00062	99939 99938	50 57
4	35 28	24	72834	235	27166	72896	236	27104	00062	99938	36
	11 35 20	0 24 47	8, 73069	234	11. 26931	8. 73132	234	11. 26868	10. 00063	9-99937	55
5	35 12	24 48	73303	232	26697	73366	234	26634	00064	99936	54
7	35 4	24 56	73535	232	26465	73600	232	26400 26168	00064	99936	53
	34 56 34 48	25 4 25 12	737 ⁶ 7 73997	230	26233 26003	73832 74063	23I 229	25937	00066	99935 99934	52 51
10	11 34 40	0 25 20	8. 74226	228	11. 25774	8. 74292	229	11. 25708	10. 00066	9- 99934	50
11	34 32	25 28	74454 74680	226	25546	74521	227	25479	00067	99933	امدا
12	34 24	25 36		226	25320	74748	226	25252	00068	99932	48
13 14	34 I6 34 8	25 44 25 52	74906 75130	224	25094 24870	74974 75199	225	25026 24801	00068 00069	99932 99931	47 46
15	11 34 0	0 26 0	8. 75353	222	11, 24647	8. 75423	222	11. 24577	10,00070	9. 99930	45
16	33 52	26 8	75575	220	24425	75645	222	24355	00071	99929	44
17	33 - 44	26 16	75795	220	24205	75867	220	24133	00071	99929	43
18	33 36 33 28	26 44 26 12	76015	219	23985 23766	76087	219	23913	00072	99928	42
19 20	33 28	26 32 0 26 40	76234 8. 76451	217	11. 23549	76306 8. 76525	219	23694	10, 00074	99927	4I 40
21	33 12	26 48	76667	216	23333	76742	217	23258	00074	99926	39
22	33 4	26 56	76883	214	23117	76958	215	23042	00075	99925	39 38
23	32 56	27 4	77097	213	22903	77173 77387	214	22827	00076	99924	37
24	32 48	27 I2 0 27 20	77310 8, 77522	212	22690		213	22613	00077	99923	36
25 26	11 32 40 32 32	0 27 20 27 28	8. 77522 77733	211	11. 22478 22267	8. 77600 77811	211	11. 22400 22180	10.00077	9. 99923	35 34
27	32 24	27 36		209	22057	78022	210	21978	00070	99921	33
28	32 16	27 44	77943 78152	208	21848	78232	209	21768	00080	99920	32
29	32 8	27 52	78360	208	21640	78441	208	21559	00080	99920	31
30 31	11 32 0 31 52	0 28 0 28 8	8. 78568 78774	206	21226	8, 78649 78855	206	21145	10. 00081	9. 99919 99918	30 20
32		28 16	78979	204	21021	79061	205	20939	00081	99917	28
33	31 36	28 24	70182	203	20817	79266	204	20734	00083	99917	27 26
34	31 28	28 32	79386	202	20614	79470	203	20530	00084	99916	
35 36	11 31 20 31 12	0 28 40 28 48	8. 79588 79789	20I	11, 20412	8. 79673 79875	202	20125	10, 00085	9. 99915	25 24
30		28 56	79999	199	20010	80076	201	19924	20087	99914 99913	23
37 38	30 56	29 4	80189	199	19811	80277	199	19723	00087	99913	22
39	30 48	29 12	80388	197	19612	80476	198	19524	00088	99912	21
40	11 30 40	20 28	8. 80585 80782	197	11. 19415	8. 80674 80872	198	11. 19326	10.00089	9. 99911	20
41 42	30 32 30 24	29 28 29 36	80978	196	19022	81068	196	19128	00090	99910	19 18
43	30 16	29 44	81173	194	18827	81264	195	18736	10000	99909	17 16
44	30 8	29 52	81367	193	18633	81459	194	18541	00092	99908	
45	11 30 0	20 8	8, 81560	192	11. 18440	8. 81653 81846	193	11. 18347	10. 00093	9. 99907	15
46	29 52 29 44	30 8 30 16	81752 81944	192 190	18248	82038	192 193	18154	00094	99906 99905	14
47	29 36	30 24	82134	190	17866	82230	190	17770	00096	99904	12
49	29 28	30 32	82324	190 189	17676	82420	190	17580	00096	99904	11
50	II 29 20	0 30 40	8. 82513	188	11. 17487	8, 82610	189	11. 17390	10. 00097	9- 99903	10
51 52	29 12	30 48 30 56	82701 82888	187	17299	82799 82987	188 188	17201	00098	99902	8
53	29 4 28 56	30 50	83075	186	16025	83175	186	16825	00100	99901	
54	28 48	31 12	81261	185	16739	83361	186	16639	10100	00800	7
55 56	11 28 40	0 31 20	8. 83446	184	11. 16554	8. 83547	185	11. 16453 16268	10,00102	4. 99898	5
5°	28 33 28 34	31 28 31 36	83630 83813	183	16370	83732	184 184	16268 16084	00103	89898	4
57 58	28 24	31 36 31 44	83996	183	16004	83916 84100	182	15900	00103	99897 99896	3
82	28 8	31 53	84177	181	15823	84282	182	15718	00105	99895	1
∞	28 0	32 0	84258	181	15642	84464	182	15536	90100	99894	·
M.	Hour P. M.	Hour A. M.	Costse.	Diff. r'.	Secant.	Cotangent.	Diff. 1'	Tangent.	Cosecant.	Sine.	M.
93°											86°

4.										1	175
M,	Hour A. M.	Hour P. M.	Store.	DIE. r.	Cosecant.	Tangent.	DHf. r'.	Cotangent.	Secunt.	Costae.	M.
0	11 a8 o	0 32 0	8, 84358	181	11. 15642	8. 84464 84646	182	11. 15536	10.00106	9. 99894	60
1	27 52	32 8	84539 84718 84897	179	15461	84646 84826	180	15354	00107	00801	59 58
3	27 44 27 36	32 16 32 24	84718	179 178	15282 15103	85006	180	15174	00108 00109	99892	50
4	27 28	32 32	85075	177	14925	85185	179 178	14994 14815	00109	10800	57 56
ş	11 27 20	0 32 40	8, 85252	177	11. 14748	8. 85363	177	11. 14617	10, 001 10	0.00000	55
	27 12	32 48 32 56	85429 85605		14571	85540	177	14460 14283	00111	99889 99888	54
7	27 4 26 56	32 56 33 4	85780	175 175	14395	85717 85893	176	14107	00113	00887	53 52
9	26 48	33 12	85955	173	14045	86069	174	13931	00114	99886	51
10	11 26 40 26 23	0 33 20	8,86128	173	11. 13872	8. 86243	174	11. 13757	10,00115	9. 99885 99884	50
11		33 28 33 36	86301 86474	173	13699 13526	86417 86591	174	13583	00116	00881	49 48
13	26 16	33 44	86474 86645	171	13355	86763	172	13237	00118	00883	47 46.
14	26 8	33 52	90910	171	13184	86935	171	13065	00119	9988z	
15	11 26 0	34 °	8. 86987	169 169	11. 13013	8. 87106 87277	171	11. 12894	10. 00120	9. 99880 99879	45
	25 52 25 44	34 8 34 16	87156 87325	166	12675	87447	170 169	12553	00121	99879	44 43
17	25 36	34 24	87494 87661	169 167 168	12506	87447 87616	169 168	12553 12384	00122	99879 99878	43
19	25 28	34 32	87661		12339	87785		12215	00123	99877	41
20	11 25 20 25 12	0 34 40 34 48	8. 87829	166	11. 12171	8. 87953 88120	167 167	11. 12047	10. 00124	9. 99876 99875	40
23		34 48 34 56	87995 88161	165	11839	88287	166	11713	00120	00874	39 38
23	24 56	35 4	88326	164	11674	88453 88618	165	11547 11382	00127	00872	37 36
24	24 48	35 12	88490 8, 88654	164	11510	88618	165		00128	99872	
25 26	11 24 40 24 32	0 35 20 35 28	88817	163	11. 11346	8, 88783 88948	165 163	11. 11217	10, 00129	9. 99871	35 34
27 28	24 24	35 36	88980	162	11020	89111	163	10889	00131	99870 99869	33
	24 16	35 44	89142	162	10858	89274	163	10726	00132	1 กกซีกซี	32
29	24 8	35 52 0 36 0	89304 8.89464	160	10696	89437	161	10563	00133	99867 9. 99866	31 30
30	11 24 0 23 52	0 36 0 36 8	89625	159	11. 10536 10375	8. 89598 89760	160		10, 00134 00135	00805	20
32	23 44	36 16	89784	159	10216	89920	160	10240 10080	00136	99864	29 28
33	23 44 23 36 23 28	36 24 36 32	89943	159 158	10057	90080	160	09920	00137 00138	99863 99862	27 26
34	23 28	36 32 0 36 40	8. go26o	157	11.09740	90240 8. 90399	159	11.00601	10, 001 30	0.00861	25
35 36	23 12	36 48	90417	157	09583	90557	158	09443 09285	00140	00860	24
37 38	23 4	36 56	90574	156	09426	90715 90872	157	09285	00141	99859 99858	23
38 39	22 56 22 48	37 4 37 12	90730 90885	155	09270	90072	157 156	09128 08971	00142	99857	22 21
40	11 23 40	0 37 20	8. 91040	155	11. 08060	8, 91185	155	11.08815	10. 00144	9. 99856	20
41	22 32	37 28	91195	154	088oc	91340	155	08660	00145	00855	18
42	22 24 22 16	37 36	91349	153	08651 08498	91495 91650	155	08505 08350	00146 00147	99854 99853	
43 44	22 10	37 44 37 52	91502	153 152	08345	91803	153 154	08197	00147	99852	17
45 46	11 22 0	0 18 0	8. 91807	152	11.08101	8. 91957	153	11.08043	10. 00149	0.00851	15
46	21 52	188	91959	151	0804 1	92110	152	07890	00150	99850 99848	14
47 48	21 44 21 36	38 16 38 24	92110	151	07890 97739	92262 92414	152 151	07738 07586	00158 00153	00847	13
49	21 28	38 32	92411	150	07589	92565	151	07435	00154	99846	111
50	11 21 20	0 38 40	8. 92561	149	11.07439	8, 92716	150	11.07284	10. 00155	0. 00845	10
51 52	21 12 21 4	38 48 38 56	92710 92859	149 148	07290	92866 93016	150	07134 06984	00156	99844 99843	8
53	21 4 20 56	30 50	93007	147	07141 06993 06846	93010	149 148	I 06835 I	00157 00158	00842	
54	20 48	39 12	93154	147	06846	93313	149	00087	00159	99841	3
55 56	11 20 40	0 39 20	8. 93301	147	11. 06699	8. 93462	147	11.06538	10, 00160	9. 99840 99839	5
50	90 33 90 24	39 28 39 36	93448 93594	146 146	06552 06406	93609 93756	347 147	06391 06244	00161	00818	4 3
57 58	20 16	39 44	93740	145	06260	93903	146	06097	00163	00827] 2
59 60	20 8	39 52	93740 93885	145	06115	94049	146	05951 05805	00164 00166	99836 99834	ij
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94°									_	-	85°

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56 78 9 10 11 12 13 14 15 16 17 18	11 19 20 19 12 19 4 18 56 18 48 11 18 40 18 24 18 16 18 8 11 18 0 17 52 17 44 17 36 17 28	0 40 40 40 48 40 56 41 4 41 12 0 41 28 41 36 41 44 41 52 0 42 0 42 8 42 16	8. 94746 94887 95029 95170 95310 B. 95450 95589 95728 95867 96005	11 13 15 18 +20 22 24 26 29	11. 05254 05113 04971 04830 04690 11. 04550 04411 04272	8. 94917 95060 95202 95344 95480 8, 95627 95767	13 15 18 20	04940 04798 04656 04514	00173 00173 00175 00176	0 0	99828 99827 99825 99824	54 53 52
78 9 10 11 12 13 14 15 16 17 18	19 12 19 4 18 56 18 48 11 18 40 18 32 18 24 18 16 18 8 11 18 0 17 52 17 44 17 36 17 28	40 48 40 56 41 4 41 12 0 41 28 41 36 41 44 41 52 0 42 0 42 8 42 16	94887 95029 95170 95310 B. 95450 95589 95728 95867 96005	13 15 18 +20 22 24 26 29	05113 04971 04830 04690 11. 04550 04411 04272	95060 95202 95344 95486 8, 95627 95767	15 18 20 22	04940 04798 04656 04514	DOI 73 DOI 75 DOI 76	0	99827 99825 99824	53
78 9 10 11 12 13 14 15 16 17 18	19 4 18 56 11 18 40 18 32 18 24 18 16 18 8 11 18 0 17 52 17 44 17 36 17 28	40 56 41 4 41 12 0 41 20 41 28 41 36 41 44 41 52 0 42 0 42 8 42 16	95029 95170 95310 B. 95450 95589 95728 95867 96005 B. 96143	15 18 +20 22 24 26 29	04830 04690 11. 04550 04411 04272	95344 95486 8, 95627 95767	20	04556	00175	0	99825 99824	52
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15 16 17 18	17 18 0 17 52 17 44 17 36 17 28	0 42 0 42 8 42 16	8. 96143		04133	95047	29 31	03953	00181	0	99819	47
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17	17 44 17 36 17 28 11 17 20	42 16		33	11. 03857	8, 96325 96464	33	11. 03675	00184	0	9. 99817	45
19	17 36 17 28 11 17 20			35	03720	96464	35 38	03536	00185	0	99815	44
19	17 28		96417	37	033447	06730	40	03390	00156	0	99814	43
	11 17 20	42 33	96553 96689	42	03311	96877	42	03123	00187	0	99813	41
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21	17 12	42 48	96960	44	03040	97150	46	02850	00100	0	99810	30
22	17 4	42 56	97005	48	02905	97285	49	02715	00191	0	99809	3
23	16 56	43 4	97229	50	02771	97421	51	02579	00102	0	99808	3
24	16 48	43 12	97363	53	02037	97556	53	02444	00193	0	99807	3
25	11 16 40	0 43 20	8. 97496	55	11, 02504	8. 97691		11, 02300	10, 00194	1	9. 99806	3
26	16 32	43 28	97629	57	02371	97825	55 58	02175	00196	1	99804	34
27	16 24	43 36	97762	59	02238	97959	60	02041	00197	1	99803	3.
28	16 16	43 44	97894	59	02106	98092	62	orgos	00198	1	99802	33
29	16 8	43 52	98026	64	01974	98225	64	01775	00199	1.	99801	-31
30	11 16 0	0 44 0	8. 98157	66	11.01843	8, 98358	66	11.01642	10,00200	1	9, 99800	31
31	15 52	44 8	98288	68	01712	98490	69	01510	00202	1	99798	20
32	15 44	44 16	98419	70	01581	98622	71	01378	00203	1	99797	
33	15 36	44 24	98549	72	01451	98753 98884	73	01247	00204	1	99795	27
34	15 28	44 32	98679	75	01321		75		-	_		-
35	11 15 20	0 44 40	8. 98808	77	11.01192	8, 99015	77 80	11.00985	10,00207	1	9-99793	21
36	15 12	44 48	98937	81	01063	99145	82	00855	00200	1	99791	2
37 38	15 4	44 56	99066	83	00934	99235	84	00595	00210	1	99790	2
39	14 56	45 4 45 12	99194	86	00578	99534	86	00406	00212	1	99788	12
	11 14 40	1.0	8, 99450	88	11.00550	8. 99662	89	11.00338	10. 00213	1	9. 99787	20
40 41	14 32	0 45 20 45 28	99577	90	00423	99791	QI	00200	00214	1	99780	10
42	T4 24	45 36	99377	02	00296	99919	93	18000	00215	T	99785	1 4
43	14 16	45 44	99830	94	00170	9, 00046	95	10, 99954	00217	1	99783	1
44	14 8	45 52	99956	96	00044	00174	97	99826	00218	2,	99782	ti
45	11 14 0	0 40 0	9, 00062	99	10. 99918	Q. 0030I	100	10. 99699	10. 00219	1	9. 99781	13
46	13 52	46 8	00207	101	99793	00427	102	99573	00220	1	99780	1.
47	13 44	46 16	00332	103	99668	00553	104	99447	00222	1	99778	3,
48	13 36	45 24	00456	105	99544	00579	301	99321	00223	1	99777	13
49	13 28	46 32	00581	107	99419	00805	108	99195	00224	1	99770	I
50	11 13 20	0 45 40	9.00704	110	10. 99296	9.00930	111	10. 99070	10. 00225	I	9-99775	1
51	13 12	46 48	00828	112	99172	01055	113	98945 98821	00227	1	99773	1
52	13 4	46 56	10095 F		99049 98026	01179	115	98621	00228	1	99772	
53	12 56	47 4	01074	116	98920	01303	117	98573	00231	1	99771	16
54	12 48	47 12	01196	-		01427	-		10. 00232	1	99768	Н
55	11 13 40	G 47 20	9. 01318	121	10. 98682	9. 01550	122	10, 98450 98327	00233	1	99767	
56	12 32	47 28	01440	123	98439	01673	126	98204	00235	1	99765	1
57 58	12 24	47 36	01501	125	98318	01790	128	98082	00230	l î	99764	П
50	12 8	47 44 47 52	01002	120	98197	02040	131	97960	00237	1	99763	
59	13 0	47 52 48 0	01923	132	98077	02103	133	97838	00239	i	99761	ь
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м,	Hour s. M.	Hour A. M.	Conine.	Diff	Secant.	Coungent	Diff	Tangent.	Cosecant	Diff.	Stec.	13

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м.	Hour A. M.	Hours, M.	Sine,	Diff.	Cosecunt.	Tangent.	Diff.	Cotangent,	Secant,	Diff.	Cosine.	12
0	11 12 0	0 48 0	9,01923	0	10. 98077	9. 02162	0	10, 97838	10, 00239	0	9. 99761	6
1	11 52	48 8	02043	2	97957	02283	2	97717	00240	0	99760	1
2	11 44	48 16	02163	1 6	97837	02404	4	97596	00241	0	99759	13
3	11 36	48 24	02283		97717	02525		97475	00243	0	99757	В
4	11 28	48 32	02402	7	97598	02645	8	97355	00244	0	99757 99756	L
5	11 11 20	0 48 40	9, 02520	9	10, 97480	9. 02,766	9	13, 97234	10, 00245	0	9-99755	Г
6	11 12	48 48	02039	11	97361	02885	11	97115	00247	a	99753	L
7	11 4	48 56	D2757	13	97243	03005	13	95995	00248 00248	0	99752	
8	10 56	49 4	02874	15	97126	03124	15	96995 96876	00249	0	99751	п
9	10 48	49 12	02992	17	97008	03242	17	96758	00251	0	99749	L
0	11 10 40	0 49 20	9. 03109	19	10, 96891	9. 03361	10	10, 96639	10, 00252	0	9.99748	t
L	10 32	49 28	03226	20	06774	03479	21	96521	00253	0		п
2	10 24	49 36	03342	22	96774 96658	03597	23	96403	00255	0	99747	
3	10 16	49 44	03458	24	96542	03714	24	96286	00255		99745	
4	10 8			26	96426		26		00256		99744	Ŀ
_	_	49 52	03574			03832		96168	00258	0	99742	Ŀ
5	11 10 0	50 8	9, 03690	28	10, 96310	9,03948	28	10. 96052	10, 00259	0	9. 99741	в
6	9 52		03805	30	96195	04065	30	95935 95819	00260	0	99740	В
3	9 44	20, 10	03920	31	96080	04181	32	95819	00252	0	99738	В
	9 36	50 24	04034	33	95966	04297	34	95703	00263	0	99737	н
9	9 28	50 32	04149	35	95851	04413	36	95587	00264	0	99736	ь
0	11 9 20	0 50 40	9. 04262	37	10. 95738	9, 04528	38	10, 95472	10,00266	0	9-99734	t.
1	9 12	50 48	04376	39	95624	04643	39	95357	00267	1	99733	
2	9 4 8 56	50 56	04490	#I	95510	04758	41	95242	00269	î	99731	
3	8 56	51 4	04603	43	95397	04758 04873 04987	43	95127	00270	i	99730	E
4	8 48	51 12	04715	44	95285	04087	45	95013	00272	Î	99728	li
5	11 8 40	0 51 20	9. 04828	46	10, 95172	9.05101		10, 94899		1		
8	8 32	51 28	04940	48	95060	+05214	47	94786	10,00273		9.99727	i,
7	8 24			50			49	94760	00274	1	99726	Į.
6 I	8 16		05052	52	94948	05328	51	94672	00276	1	99724	B
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-	_	51 52	05275	54	94725	05553	54	94447	00279	1.	99721	
0	11 8 0	0 52 0	9. 05386	56	10. 94614	9. 05666	56	10, 94334	10, 00280	1	9. 99720	13
3	7 52	52 8	05497	57	94503	05778	58	94222	00282	1	99718	13
2	7 44	52 16	05607	59 61	94393		60	94110	00283	1	99717	1:
3-	7 36	53 24	05717		94283	06002	62	93998	00284	1	99716	å
4	7 28	52 32	05827	63	94173	06113	64	93887	00286	1	99714	1 3
5	11 7 20	0 52 40	9.05937	65	10. 94063	9, 06224	66	10, 93776	10, 00287	I	9. 99713	1
6	7 12	52 48	06046	67	93954	06335	68	93665	00280	r	99711	ı
	7 4	52 56	06155	69	93845m	06445	60	93555	00200	1	99710	
7	7 4 6 50	53 4	06264	70	93736	06556	71	93444	00202	il	99708	В
٥	6 48	53 12	06372	72	93628	06066	73	93334	00293	ī	99707	2
5	11 6 40	0 53 20	9. 06481	74	10, 93519							2
	6 32	53 28	06589	76	93411	9. 06775	75	93115	10, 00295	I	9. 99705	
	6 24	53 36	06696	28		06994	77			1	99704	ľ
1	616		06804	78 80	93304 93196	07103	79 81	93006	00298	1	99702	
1	6 8	53 44	06011	81	93190		83		00299	1	99701	18
	_	53 52				07211		92789	00301	1	99699	3
1	11 6 0	0 54 0	9. 07018	83	10, 92982	9. 07320	84	10, 92680	10, 00302	1	9, 99698	Р
5	5 52	54 8	07124	85	92876	07428	86	92572	00304	1	99696	3
3	5 44	54 16	07231	87	92769	07536	88	92404	00305	1	99695	
	5 36	54 24	07337	89	92663	07043	90	92357	00307	T	99693	Į.
)	5 28	54 32	07442	91	92558	07751	92	92249	00308	t	99692	1
7	11 5 20	0 54 40	9.07548	93	10. 92452	9. 07858	94	10.92142	10,00310	1	9, 99690	1
1	5 12	54 48	07653	94	92347	07964	96	92036	00311	T.	08000	ß
2	5 4	54 56	07758	96	92242	08071	98	91929	00313	11	94687	И
3	4 56	55 4	07863	98	92137	DS177	99	91823	00314	1	99686	П
į	4 48	55 12	07968	100	92032	08283	101	91717	00316	i	99684	
1	11 4 40	0 55 20	9, 08072	102	10. 91928	9. 08 189	101	10, 01011	10, 00317	_	37.4	
5	4 32	55 28	08176	104	01824	08495	105	91505		1	9, 99683	13
-	4 24	55 36	08280	106	91720	08600	107		00319		99081	13
7	4 16		08383	107	91720	08705		91400	00320	1		В
٦,		55 44	08486				109	91295	00322	1	99678	В
9		55 52		109	91514	08810	111	91190	00323	T.	99977	Ħ
۲1	4 6	56 0	08389	111	91411	08914	113	91086	00325	1	99675	U
	Hour F. M.	Hour A. M.	Cosine.	Diff.	Secant.	Cotangent.	THE	Tungent.	Cosecant.	Diff.	Sine.	3
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M.	Hour A. M.	Hour P. M.	Sine.	DIA.	Cosecsat	Tangent.	Diff.	Cotangent.	Secant.	Diff.	Cosine.	-
0	11 4 0	0 56 0	9. 08589	0	10.91411	9. 08914	0	10. 91086	10, 00325	0	9.99675	60
1	3 52	56 8	08592	2	91308	09019	2	90981	.00326	0	99674	5
2	3.44	56 16	08795	3	91205	09123	3	90877	00328	0,	99572	3
3	3 36	56 24	08897	5	91103	09227	5	90773	00330	0.	99670 99669	5
4	3.28	56 32	08999		1001	09330	7	99670	00331	0		
570	11 3 20	0 56 40	9.09101	8	10, 90899	9. 09434	8	10. 90566	10,00333	1.00	9, 99667	5
	3 12	56 48	09202	10	90798	09537	10	90463	00334	0	99664	5
7	3 4 2 56	56 56	09304	11	90696	09640	13	90360	00337	0	09663	5
	2 45	57 4 57 12	09405	13	90595	09845	15	90250	00339	0	99661	5
9		200		-			16	10, 90053	TO, 00 141	0	9. 99659	5
10	11 2 40	0 57 20	9. 09606	16	10, 90394	9. 09947	18	89951	00342	0	99658	13
11	2 32 2 24	31	09707	10	90193	10150	20	80850	00344	0	99656	4.4
	2 16	57 30 57 44	09907	21	90093	10252	21	89748	00345	0	99655	4
13	2 8	57 52	10006	22	89994	10353	23	89647	00347	0	99653	4
14	11 2 0	0 58 B	0. 10106	24	10. 89894	9. 10454	24	10, 89546	10, 00349	0	0.00651	4
15	1 52	58 8	10205	26	89795	10555	20	89445	00350	0	99650	1
	1 44	58 16	10304	27	80606	10056	28	89344	00352	0	99648	1
17	1 36	58 24	10402	20	89598	10756	20	89244	00353	I	99647	4
10	1 28	55 32	10501	30	89499	10856	31	89144	00355	1	99645	4
20	11 1 20	0 58 40	9. 10599	32	10, 89401	9, 10956	33	10, 89044	10,00357	1	9. 99643	A
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49 49 49 50 10 24 18405 00 81453 18979 99 81631 00514 2 99485 12 39 18454 10 39 18547 69 81453 19053 71 80937 00516 2 99485 12 50 12 18547 69 81453 19053 71 80937 00516 2 99485 12 15 14 91 10 48 18709 73 81291 19229 74 80771 00520 2 99485 0 9 15 1 49 12 10 48 18709 73 81210 19312 75 80688 00522 2 99478 8 15 14 4 18871 75 81120 19312 75 80688 00522 2 99478 8 15 14 4 18871 75 81120 19312 75 80688 00522 2 99478 8 15 14 4 18871 75 81120 19312 75 80688 00522 2 99478 8 15 14 4 18871 75 81120 19312 75 80688 00522 2 99478 8 15 14 4 18871 75 81120 19312 75 80688 00522 2 99478 8 15 14 4 18952 76 81048 19478 78 80522 00526 2 99478 75 14 14 12 18523 76 81048 19478 78 80522 00526 2 99478 75 14 14 12 18523 76 80687 9 19561 78 80522 00526 2 99474 6 15 14 14 12 18523 76 80807 19725 8 80527 00530 2 99474 75 15 10 848 16 11 44 19973 8 80727 19725 8 80527 00530 2 99478 75 15 14 8 8 11 15 12 19313 8 80727 19725 8 80527 00530 2 99466 2 19948 8 11 52 19313 8 80527 197807 8 80503 00534 2 99466 2 19948 8 11 52 19313 8 80527 19807 8 80503 00535 2 99466 2 19948 8 11 52 19313 8 80527 19807 8 80503 00538 2 99466 2 19948 8 11 52 19313 8 80527 19807 8 80503 00538 2 99466 2 19948 8 11 50 19943 8 8057 19971 87 80003 00538 2 99466 0 148 0 12 0 19433 8 8057 19971 87 80003 00538 2 99466 0	40	49 52		18282	1 25							99490	
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\$\frac{51}{52}\$ 49 \cdot 4 \text{10} \cdot 48 1870 73 81911 1924 80711 \text{00520} 2 2 \frac{99480}{9948} 8 \frac{52}{52}\$ 49 4 10 56 18870 77 8120 19305 76 80685 00522 2 99478 8 8 11 18871 77 81129 19305 76 80605 00522 2 99474 6 78 80622 00526 2 99474 6 55 10 84 81 11 12 19935 76 80687 19956 78 80522 00524 2 99474 6 55 43 11 12 19193 80 80687 19945 81 8037 00534 2 99470 4 57 48 11 36 19193 80 80827 19975 82 8013 00534 4 99468 3 54 11 36 19193 80 8027 19880 85 8013 00534 4 99466 2 99464 1 60 48 0 12 0 19333 85 80567 19971 87 8029 00538 2 99464 1 60 48 0 12 0 1833 85 80567 19971 87 8029 00538 2 99464 1 184 19975 86 184 19975 184 19975 185 80567 19971 87 8029 00538 2 99462 0 185 185 185 185 185 185 00536 2 99462 0 185 185 185 185 185 00536 2 185 185 185 185 00536 2 00536 2 00536 2 00536 2 00536 2 00536 2 00536 2 00536 2 00536 2 00536 2 00536 2 00536 \qu	49			18547	69	81453	19063	71	80937	00516	2	99484	11
51 49 12 10 45 15700 73 81210 19323 74 80771 00530 2 99437 8 7 8 1 8 1 1 1 2 1 18571 75 81120 19325 75 80688 00532 2 99437 8 8 1 48 50 11 4 18871 75 81120 19305 75 80688 00532 2 99437 8 8 1 48 50 11 12 1 1852 75 81048 19305 75 80688 00532 2 99437 8 8 1 48 11 12 10 1852 75 81048 19305 75 80638 00532 2 99437 8 8 1 48 11 12 10 1952 75 81048 19305 75 80532 10 10 10 10 10 10 10 10 10 10 10 10 10						10, 81372						9. 99482	
53 48 56 11 12 18952 75 81129 19393 75 80602 00524 2 99476 7 55 10 48 40 11 12 20 9,1903 75 81048 19478 78 80522 00526 2 2 99474 6 55 10 48 40 11 12 20 9,1903 75 10,8067 9,19561 79 10,80439 10,00528 2 9,9472 5 56 48 32 11 28 19113 79 80887 19543 81 80327 00530 2 99470 4 57 48 24 11 36 19193 80 80807 19725 82 80275 00530 2 99470 4 58 48 16 11 44 19273 82 80807 19725 82 80275 00532 2 99468 3 58 48 16 11 44 19273 82 80727 19807 84 80193 00534 2 99468 3 59 48 8 11 52 19353 83 80647 19889 85 80111 00536 2 99462 0 60 48 0 12 0 19433 85 80567 19971 87 80029 00538 2 99462 0 61 HOULP M. HOULP M. Cosine. Diff. Secant Cotangent. Diff. Tangent Cosecunt. Diff. Sine M.	52							74				99480	2
54 48 48 11 12 18528 76 81c48 19478 78 80522 00526 2 99474 6 55 10.849 11 120 1,1903 76 10.8049 1	53	48 56	11 4	18871	1 75	81129	19395	78		00524		99476	
57 48 24 II 30 19193 80 86087 19735 82 80275 00532 2 99468 3 5 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	54	48 48	11 12			81048	19478	78		00526	2	99474	
57 48 24 II 30 19193 80 86087 19735 82 80275 00532 2 99468 3 5 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	55				78		9. 19561	79	10. 80439			9.99472	
58 48 16 11 44 19273 82 80277 19807 84 80103 00534 2 99466 2 9 48 8 11 52 19353 83 80647 19889 85 80111 00536 2 99404 1 60 48 0 12 0 19433 85 80567 19971 87 80029 00538 2 99402 0 M. Hours H. Hours H. Cosine. Diff. Secant Cotangent. Diff. Tangent Cosecunt. Diff. Sine M.	57	48 24			16	80807			80357		3	99470	
59 48 8 11 52 19353 83 80647 19389 85 80111 00536 2 99404 1 60 48 0 12 0 19433 85 80567 19971 87 80039 00338 2 99462 0 M. Hours. M. Hours. M. Cosins. Diff. 3ecant Cotangent. Diff. Tangent Cosecant. Diff. 6ine M	58	48 16	11 44	19273	82	80727	19807	84	80193	00534	2	99466] 2]
M. Hours, M. Hours, M. Cosine. Diff. Secant Cotangent. Diff. Tangent Cosecant. Diff. Sine M	59	48 8		19353		80647		85	80111	∞536		99404	
The state of the s	_				_			<u> </u>					
96° 81°		HOUF P. M.	HOULYN	Cosine.	Diff.	Secant	Cotangent.	Diff.	Tangent	Cossoant.	Diff.	Sine	М
	96°												81.

90											1	70°
M.	Hour a. M.	Hour p. m.	Sine.	Diff.	Concent.	Tangent.	Diff.	Cotangent	Secant.	Diff.	Cosine.	M.
۰.	10 48 0	I 12 0 12 8	9. 19433	0	10, 80567 80487	9. 19971	0	10. 80029	10. 00538 00540	0	9. 99462	60
1 2	47 52 47 44	12 16	19513 19592	3	80408	20053 20134	3	79947 79865	00542	0	99458	59 58
3	47 36 47 28	12 24 12 32	19672 19751	4 5	80328 80249	20216	4 5	79784 79793	00544 00546	8	99456 99454	57 56
- 4 5	10 47 20	I 12 40	9. 19830	6	10, 80170	9. 20378	6	10. 79622	10, 00548	0	9. 99452	55
	47 12	12 48 12 56	19988	8	80091 80012	20459 20540	8	79541 79460	00550 00552	l °	99450 99448	54 53
7	47 4 46 56	I3 4	20067	10	79933	20621	10	79379	00554	0	99446	52
يو	40 40	13 12 1 13 20	20145	11	79855	9, 20782	12	79299	10, 00558	0	99444	51 50
10	10 46 40 46 32	I 13 20 I3 28	20302	13	79698	20002	13 14 16	79138	00560	0	99440	49 48
12	46 24 46 16	13 36 13 44	20380 20458	15 16	79620 79542	20942 21022	16	79058 78978 78898	00562 00564		99438 99436	48
13	46 8	13 44 13 52	20535	18	79465	21102	17 18	78898	00566	ő	99434	47 46
15 16	10 45 0	I 14 0 IA 8	9. 20613 = 20691	19	10. 79387	9, 21182	19 21	10, 78818 78739	10, 00568	1	9, 99432	45 44
17 18	45 52 45 44	14 8 14 16	20768	20 21	79232	21341	22	78659 78580	00573	1	99427	43
18	45 36 45 28	14 24 14 32	20845 20922	23 24	79155 79078	21420 21499	23 25	78580 78501	90575 90577	1	99425 99423	42 41
20	10 45 20	I 14 40	9. 20999	25 20	10, 79001 78924	9. 21578	26	10, 78422	10, 00570	1	9. 99421	40
21 22	45 12	14 48 14 56	21076	26 28	78924 78847	21657	27 28	78343 78264	00581 00583	1 1	99419 99417	39 38
23	45 4 44 56	15 4	21153 21229	29	78771	21736 21814	30	78186	00585	1	99415	37
24	44 48 10 44 40	15 12	21306	30	78694 10, 78618	21893 9, 21971	31	78107	10, 00589	1	9,99411	36 35
26	10 44 40 44 32	1 15 20 15 28	9. 21382 21458	31 33	78542	22049	34	7795í	00591	1	99409	33
27 28	44 24 44 16	15 36 15 44	21534 21610	34 35	78466 78390	22127 22205	35 36	77873 77795	00593 00596	I	99407 99404	33 32
29	44 8	15 52	21685	37	78315	22283	38	77717	00598	1	99402	31
30	10 44 0	1 16 o	9. 21761 21836	38	10. 78239 78164	9. 22361 22438	39 40	10. 77639 77562	10,00600	1	9. 99400 99398	30 29
31 32	43 52 43 44	16 16	21912	39 40	78088	22516	41	77484	00604	1	99396	28
33 34	43 36 43 28	16 24 16 32	21987	42 43	78013 77938	22593	43 44	77407 77330	00606 00608	1 1	99394 99392	27 26
35	10 43 20	I 16 40	9. 22137	44	10. 77863	9. 22747	45	10. 77253	10, 00610	1	0.00300	25
36	43 12 43 4	16 48 16 56	22211	45	77789 77714	22824 22001	47 48	77176 77099	00612 00615	1	99388 99385	24 23
37 38	42 56	17 4	22361	47 48	77639	22977	49	77023	00617	1	99383	22
39 40	42 48 10 42 40	17 12	9. 22509	49 50	77565	23054 9, 23130	50 52	76946 10, 76870	00619	1	99381	21
41	42 32	17 28	22583	52	77417	23206	53	76794	00623	1	99377	19 18
42 43	42 24 42 16	17 36 17 44	22657	53 54	77343 77269	23283 23359	54 56	76717 76641	00625 00628	I 2	99375 99372	17
44	42 8	17 52	22731 22805	55	77195	23435	57	76565	00630	2	99370	16
45 46	10 42 0 41 52	1 18 0 18 8	9. 22878	57 58	10. 77122 77048	9. 23510 23586	58 60	10, 76490 76414	10, 00632 00634	2 2	9. 99368 99366	15 14
47 48	41 44	18 16	23025 23098	59	76975 76902	23661	61 62	76339 76263	00636 00638	2 2	99364	13
49	41 36 41 28	18 24 18 32	23098	62	76829	23737 23812	63	76188	00641	2	99362 99359	13
50	10 41 20	18 40	9. 23244	63	10, 76756 76683	9. 23887	65	10. 76113	10, 00643	2	99357	10
51 52	41 12 41 4	18 48 18 56	23317 23390	64	76610	23962 24037	67	76038 75963	00647	2 2	99355 99353	8
53 54	40 56 40 48	19 4 19 12	23462	67 68	76538 76465	24112 24186	69 70	75963 75888 75814	00649	2 2	99351 99348	7
55 56	10 40 40	1 19 20	23535 9. 23607	69	10, 76393	9. 24261	71	10. 75739	10, 00654	2	9. 99346	5
56	40 32 40 24	19 28 19 36	23679	71 72	76321 76248	24335	73 74	75665 75590	00656 00658	2 2	99344 99342	4 3
57 58	40 16	19 44	23752 23823	73	76177	24410 24484	75 76	75516	00660	2	99340	2
59	408	19 52 20 0	23895 23967	74 76	76105 76033	24558 24632	76 78	75442 75368	00663	2 2	99337 99335	;
M.	Hour E M.	Hour A. M.	Cosine.	Diff.	Secaht.	Cotangent.	Diff.	Tangent	Cosecant.	Diff.	Sine.	М.
99°									<u> </u>	ت-		80°
-												
					18	57						

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SINKS	TANGENTS	AND	SECANTA	

100	P 100°											
M.	Houra. M.	Hour P. M.	Sine.	Diff.	Concent.	Tangent,	Diff.	Cotangent.	Secant.	Diff.	Costne,	M.
0	10 40 0	1 20 0	9. 23967		10, 76033	9. 24632 84706	0	10, 75368	10. 00665	0	9- 99335	60
1 2	39 52 30 44	20 8 20 16	24039 24110	1 2	75961 75890	24779		75294 75221	00660	0	99333 99331	59 58
3	39 44 39 36 39 28	20 24 20 32	24181	3	75819	24779 24853 24926	4	75147	00672	8	99328	57 56
4	39 28 10 39 20	I 20 40	94253	5	75747 10, 75676	9. 25000	5	75074	10,00676	-	99326 9-99324	35 35
5	39 12	20 48	24395 24466	7	75605	25073	7	74927 74854	00678	:	99322	54
7	39 4 38 56	20 56 21 4	24400 24536	:	75534 75464	25146 25219	١	74781	00683	:	99319 99317	53 52
9	38 48	21 12	24007	10	75393	25292	11	74708	00685		99315	51
IO II	10 38 40 38 32	21 28	9. 24677	11	10, 75323 75252	9. 25365 25437	13	10. 74635 74563	10, 00687	°	9. 99313 99310	50
ts	38 24	21 36	24748 24818	14	75182	25510	14	74490	00692	0	99308	49 48
13 14	38 16 38 8	21 44	24888 24958	15	75112 75042	25582 25655	15	74418 74345	00694 00696	;	99306 99304	47
15	10 38 0	1 22 0	9, 25028	17	10, 74972	9. 25727	18	10, 74273	10,00699	1	9. 99301	45
16	37 52 37 44	22 8 22 16	25098 25168	18	74902 74832	25799 25871	19	74201 74129	00701 00703	1	99299 99297	44 43
17	37 36	22 24	25237	90	74763	25943	21	74057 73985	00700	1 1	99294	42
19	37 28 10 37 20	22 32 1 22 40	9. 25376	23	74693	26015 9. 26086	24	73985	10,00710	-	9,99290	#
21	37 12	22 48	25445	24	74555 74486	26158	25	71842	00718	1	99288	39 38
23	37 4 36 56	23 56 23 4	25514 25583	25 26	74486 74417	26229 26301	26	73771 73699	00715 00717	:	99285 99283	38
24	36 48	23 4 23 12	25652	27	74348	26372	28	73628	00719	[i	99281	37 36
25 26	10 36 40	1 23 20	9. 25721	28	10. 74279	9. 26443 26514	29	10. 73557 73486	10.00722	1	9. 99278	35
27	36 32 36 24	23 28 23 36	25790 25858	30	74210 74142	28732	31	73415	00724 00726	1	99276 99274	34 33
28	36 16	23 44	25927	32	74073 74005	26655 26726	33	73345	00729	1	99271	32
30 30	36 8 10 36 0	23 52 1 24 0	25995 9. 26063	33		9. 26797	34	73274	10, 00733	1	99269	31 30
31	35 52	24 8	26131	35 36	10, 73937 73869	26867	35 36	73133	00736	1	99264	29 28
32 33	35 44 35 36	24 16	26199 26267	30 38	738ot 73733	26937 27008	38	73063	00738 00740	1	99262 99260	25
34	35 28	24 32	26335	39	73665	27078	40	72922	00743	1	99257	ać
35 36	10 35 20 35 12	1 24 40 24 48	9, 26403 26470	40 41	10. 73597	9. 27148	41 42	10, 72852 72782	10, 00745	1	9, 99255	25 24
37 38	35 4	24 56	26538 26605	42	73530 73462	27288	44	72712	00750	1	99250	23
38	35 4 34 56 34 48	25 4 25 12	26605 26672	43 44	73395 73328	27357 27427	45	72643 72573	00752 00755	1	99248 99245	22
40	10 34 40	1 25 20	9. 26739	45	10, 73261	9, 27496	47	10, 72504	10, 00757	2	9. 99243	90
4I 43	34 32 34 24	25 28 25 36	26806 26873	47	73194 73127	27566 27635	48	72434 72365	00759	:	99241 99238	91 31
43	34 16	25 44	26940	49	73060	27704	51	72296	00764	2	99236	17
44	34 8 10 34 0	25 52 1 26 0	9, 27073	50	72993	27773 9-27842	52	72227 10, 72158	10,00769	1	99233	16
45 46	10 34 0 33 52	26 8	9. 27073 87140	52	72860	27011	53 54	72089	00771	1	99229	14
47	33 44 33 36	26 16 26 24	27206 27273	53	72794 72727	27980 28049	55 56	72020	00774 00776	:	99226 99224	13 12
49	33 36	26 32	27339	55 56	72727	28117	58	710F1 71883	00//0		99221	111
50	10 33 20	I 26 40	9. 27405	57 58	10, 72595	9, 28186	59 60	10, 71814	10,00781	3	9. 99219	10
51 52	33 12 33 4	26 48 26 56	27471 27537	58 59	72529 72463	28254 28323	61	71746 71677	00783 00786	2	99217	8
53	32 56	27 4	97602	60	72398	19882	62	71609	00788	2	99818	7
54	32 48 10 32 40	27 12 1 27 20	9- 27734	61	72332 10, 72266	28459 9, 28527	63	71541	00791	븕	99209	5
55 56	32 32	27 28	87799 87864	64	72201	28595	66	71405	00796		99204	4
57 58	32 24 32 16	87 36 87 44	27864 27930	65	72136 72070	28002 28730	67 68	71338 71270	00798 00800	:	99200	3
59 60	328	87 52	27995 28060	67	72005	28798 28865	69	71202	00801	8	99197	1
	32 0	88 o		68	71940		71	71135	00805	-	99195	•
M.	Hour & M.	Hour A. M.	Costne.	Diff.	Secent.	Cotangent.	Diff.	Tangest.	Cosscant.	Dig.	Man.	x.
100	•											25.

M.	Hour P. M.	Hour A. M.	Cosine.	Diff.	Secant.	Cotangent.	Diff.	Tangent.	Coseount.	Diff.	Sine.	M. 78°
59 60	24 0	35 52 36 0	31788	62	68212	32747	65	67253	00960	3	99040	۰
58 50	24 16 24 8	35 44	31669 31728	60	68331 68272	32623 32685	63 64	67377 67315	00954 00957	2 3	99046 99043	2
57 58	24 32 24 24	35 28 35 36	31549 31609	59	68451 68391	32498 32561	61	67502 67439	00949 00952	2 2	99051 99048	3
55 56	IO 24 40	1 35 80	9. 31490	57 58	10, 68510	9. 32436	59	10, 67564	10. 00946	2	9. 99054	5
53 54	24 56 .24 48	35 4 35 12	31370 31430	55 56	68630 68570	32311 32373	57 58	67689	00941 00944	2 2	99059 99056	7
52	25 4	34 56	31310	54	686ao	32248	55 56	67752	00938	2	99062	8
50 51	10 25 20 25 12	1 34 40 34 48	9. 31189 31250	52 53	10, 68811	9. 32122 32185	54	10. 67878	10, 00933 00936	2 2	9. 99067 99064	10
49	25 28	34 32	31129	51	68871	32059	53	6794i	00930	2	99070	11
47 48	25 44 25 36	34 16 34 24	31008 31068	49 50	68992 68932	31933 31996	51 52	68067 68004	00925	2 2	99075 99072	13
45 46	25 52	34 8	30947 31008	47 48	60053	31870	49 50	68130	00928	2	9. 99080 99078	15 14
44	26 8 10 26 0	33 52	30826	46	10, 69113	31743 9. 31806	47	68257	00917	2	99083	16
42 43	26 24 26 16	33 36 33 44	30704 30765 30826	43	69296 69235	31616 31679	45	68384 68321	00912 00914	2 2	99086	17
41	26 72	. 33 28	30643	42	69357	31552	44	68448	00909	2	99088	19 18
39 40	26 48 10 26 40	33 12 1 33 20	30521 9, 30582	40	10, 69418	31425 9. 31489	43	10, 68511	10, 00907	2	99096	21 20
37 38	27 4 26 56 26 48	33 4	30459	39	69541	31361	41	68639	10000	2	99099	22
36 37	27 12 27 4	32 48 32 56	30336 30398	37 38	69664 69602	31233 31297	39 40	68767 68703	00896 00800	2 2	99104	24 23
35 36	10 27 20	1 12 40	9. 30275	36	10, 69725	9. 31 168	38	10, 68812	10, 00894	2	9. 99106	25
33 34	27 36 27 28	32 24 32 32	30151	34 35	69849 69787	31040 31104	36 37	68960 68896	00888	1	99112	27 26
31 32	27 44	32 16	30090	33	60010	30975	33 35 36	69025	00886	1	99117	28
30	10 28 0 27 52	1 32 0 32 8	9. 29966 30028	31 32	10, 70034 69972	9. 30846 30911	32	10, 69154 69089	10, 00881	1	9. 99119	30 20
29	28 8	31 52	29903	30	70097	30782	31	69218	00878	i	99124 99122	32 31
27 28	28 24 28 16	31 36 31 44	29779 29841	28 20	70221 70159	30652 30717	39 30	69413 69348 69283	00873 00876	1	99127	33
25 26	28 32	31 28	9. 29654 29716	20 27 28	10, 70346 70284	9. 30522 30587	27 28	10. 69478 69413	00870	I	9. 99132	35 34
24	20 40	31 12	29591	25 26	70409	30457	26	69543	00865	4	99135	37 36
23	29 4 28 56	31 4	29529	23 24	70534 70471	30326 30391	25	69674 69609	00861	i	99140 99137	38 37
21 22	29 12	30 48	29403 29466	22	70597	30261	23	69739	00858 00860	1	99142	39 38
20	10 29 20	30 32 1 30 40	29277 9. 29340	21	70723	30130 9. 30195	22	10, 69805	00853 10. 00855 00858	1	99147	4I 40
17 18 19	29 36 29 28	30 24	29214	19	70786	30064	19	69936 69870	00850	1	99150	42
16 17	29 52 29 44	30 8 30 16	29087 29150	17	70913 70850	29932 29998	17	70002	00845 00848	1	99155 99152	44 43
15	10 30 0	1 30 0	9. 29024	16	10. 70976	9. 29866	16	10, 70134	10, 00843	1	9-99157	45
13 14	30 t6 30 8	29 44 29 52	28896 28960	13 14	71 104 71040	29734 29800	14	70266 70200	00838 00840	1	99162 99160	47 46
12	30 24	29 36	28833	12	71167	29668	13	70332	00835	3	99165	49 48
10	10 30 40 30 32	1 29 20 29 28	9. 28705 28769	10 11	10. 71295 71231	9. 29535 29601	11	10. 70465 70399	10. 00830 00833	0 0	9. 99170	50
9	30 48	29 12	28641	9	71359	29468	10	70532	00828	0	99175 99172	52 51
7	31 4 30 56	28 56 29 4	28512 28577	7	71552 71488 71423	29335 20402	8	70732 70665 70598	00823	0	99177	53
ş	10 31 20 31 12	1 28 40 28 48	9. 28384 28448	ş	10. 71616 71552	9. 29201 29268	5	10, 70799	10, 00818	0	9. 99182 99180	55 54
4	31 28	28 32	28319	4	71681	29134	4	70933 70866	00815	٥	99185	57 56
3	31 44 31 36	28 16 28 24	28190 28254	3	71810 71746	29000 29067	3	71000	00813	:	99190 99187	58 57
ı	31 52	28 8	28125	1	71875	28933	1	10. 71 135 71067	00808	0	9. 99195	59 58
0	Houra. M. 10 32 0	1 28 0	g, 28060	0	10, 71940	Tangent. 9, 28865	DEF.	Cotangent.	Secant. 10. 00805	Diff.	Cosine.	M. 60
11°		Hour P. M.	Sine.	Diff.	Cosecant.				,			68°
440												

12°												
M.	Hour a. m.	Hour P. N.	Sine.	Diff.	Coeccant.	Tangent.	Diff.	Cotangent.	Secant.	Diff.	Cosine.	×.
۰	10 24 0	1 36 0	9. 31 788	0	10. 68212	9. 32747	0	10. 67253	10.00960	0	9. 99040	60
1	23 52 23 44	36 8 36 16	31847 31907	1 2	68153 68093	32810	1 2	67190 67128	00962		99038 99035	59 58
3	23 36	36 24	31966	3	68034	32933	3	67067	00968	0	99032	57 56
4	23 28	36 32	32025	4	67975	32995	4	67005	00970	P	99030	
ş	10 23 29 23 12	1 36 40 36 48	9. 32084 32143	5	10. 67916 67857	9. 33°57 33119	8	10, 66943	10. 00973	0	9. 99027 99024	55
	23 4	36 56	12202	7	67798	33180	7	66820	00978		99022	54 53
8	22 56 22 48	37 4	32261		67739 67681	33242		66758	00981	0	99019	52
9	22 48 10 22 40	37 12 1 37 20	32319 9. 32378	9	10, 67622	33303 9- 33365	9	10, 66635	10, 00987	- ;	9,99013	51 50
11	22 32	1 37 20 37 28	32437	10	67563	33426	11	66574	00989	i	11000	
12	22 24	37 36	32495	11	67505	33487	12	66513	00992	1	99008	49 48
13 14	22 16 22 8	37 44 37 52	32553 32612	12	67447 673 8 8	33548 33609	13 14	66452 66391	00995 00998	1	99005 99002	47 46
15	10 22 0	1 38 O	9. 32670	14	10, 67330	9. 33670	15	10. 66330	10, 01000	1	9, 99000	45
16	21 52	38 8	32728	15	67272	33731		66269	01003	1	9. 99000 98997	44
17	21 44 21 36	38 16 38 24	32786 32844	16	67214 67156	33792 33853	17	66208 66147	01000	1	98994 98991	43
19	21 28	38 32	32902	18	67098	33913	19	66o87	01011	i	08080	41
20	10 21 20	1 38 40	9. 32960	19	10. 67040	9- 33974	20	10, 66026	10, 01014	1	9. 98986	40
21	21 12	38 48 38 56	33018	20	66982 66925	34°34 34°95	2I 22	65966 65006	01017 01020	1	98583 98980	39 38
23	21 4 20 56	39 4	33133	22	66867	34155	23	65905 65845	01022	1	98978	37
24	20 40	39 12	33190	23	66810	34215	24	65785	01025	1	98975	37 36
25 26	10 20 40 20 32	1 39 20 39 28	9. 33248 33305	24 25	10, 66752 66695	9. 34276 34336	25	10. 65724 65664	10, 01028	1	9. 98972	35 34
27	20 24	39 36	33362	26	66648	34396	27	65604	01033	1	98967	33
28	20 16	39 44	33420	27 28	66580	34456	28	65544	01036	1	98964	32
29 30	20 8	39 52 1 40 0	33477 9- 33534	20	66523 10. 66466	34516 9. 34576	30	65484	01039	1	98961 9. 98958	31 30
31	19 52	40 8	33591	29	66400	34635	31	65365	01045	l il	98955	20 20 28
32	19 44	40 16	33647	30	66353	34695	32	65305	01047	1	98953	
33 34	19 36 19 28	40 24 40 32	33704 33761	31 32	66236 46239	34755 34814	33	65245 65186	01050		98950 98947	27 26
35	10 19 20	I 40 40	9. 33818	33	10. 66182	9. 34874		10.65126	10, 01056	3	9, 98944	25
36	19 12	40 48	33874	34	66126 6606g	34933 34992	35 36	65067 65008	01059	*	98941	24
37 38	19 4 18 56	40 56 41 4	33931 33987	35 36	65013	35051	37 38	64040	01064	2	98938 98936	23
39	18 48	41 12	34043	37	. 65957	35111	39	64949 64889	01067	2	98933	21
40	10 18 40	1 41 20	9. 34100	38	10. 65900	9- 35170	40	10, 64830	10, 01070	8	9. 98930	20
4 ^I 4 ²	18 32 18 24	41 28 41 36	34156 34212	39 40	65844 65788	35229 35288	41 42	64771 64712	01073 01076	1	98927 98924	18
43	18 16	41 44	34268	41	65732	35347	43	64653	01079	2	98021	17
44	18 8	41 52	34324	43	65676	35405	44	64595	01081	2	98919	
45 46	10 18 0	1 42 0 42 8	9. 34380 34435	43	10. 65620 65564	9. 35464	45 46	10, 64536 64477	10, 01084	2 2	9. 98916 98913	15 14
40	17 44	42 16	34491	45	65509	35523 35581	47 48	64419	0109 0		98910	13
48	17 36	42 24	34547	46	65453	35640 35698		64360 64302	01093	2 2	9890 7 98904	12
49 50	17 28 10 17 20	42 32 I 42 40	34602 9. 34658	47	65398		50	10, 64243	10. 01099	-	9. 98901	10
51	17 12	42 48	34713	48	10. 65342 65287	9- 35757 35815	51	64185	01102	2	08808	8
52	17 4 16 56	42 56	34769	49	65231	35 ⁸ 73	52	64127 64069	01 104 01 107	2 2	98896 98893	
53 54	16 56 16 48	43 4 43 12	34824 34879	50	65176	35931 35989	53 54	64011	01110	3	98890	7
55	10 16 40	1 43 20	9. 34934	52	10. 65066	9. 36047	55	12. 63953	10, 01113	3	9. 98887	5
56	16 32 16 24	43 28	34989	53	65011	36105 36163	56	63895 63837	01110	3	98884 98881	4
57 58	16 24 16 16	43 36 43 44	35044 35099	54	64956 64901	36221	57 58	63779	01119	3	98878	3 2
59	16 8	43 52	35154	55. 56	64846	36279	59	63721	01125	3	98875	!
60	16 0	44 0	35209	57	64791	36336	60	63664	01128	3	98872	۰
ж.	Hour P. M.	Hour a. M.	Cosine.	Diff.	Secant.	Cotangent.	Diff.	Tangent.	Corecant.	Diff.	Sine.	×.
102	•											170

18°				•							1	1660
×.	Hour a M.	Hour P. M.	Sine.	Diff.	Conecanti	Tangent.	Diff.	Cotangent.	Secant.	Diff.	Cosine.	и.
۰	10 16 0	I 44 0	9. 35209	۰	10. 64791	9. 36336	۰	10.63664	10. 01 128	۰	9. 98872	60
1 2	15 52 15 44	44 8 44 16	35263 35318	1 2	64737 64682	36394 36452	1 2	63606 63548	01131	0	98869 98867	59 58
3	15 44 15 36	44 24	35373	3	64627	36500	3	63491	01136	0	98864	57 56
4	15 28	44 32	35427	4	64573	36566	4	63434	01139	0	98861	
ş	10 15 20 15 12	1 44 40 44 48	9. 35481 35536	4	10. 64519 64464	9. 36624 36681	ş	10. 63376 63319	10. 01 142	0	9. 98858 98855	55 54
7	15 4 14 56	44 56	35590	ş	64410	36738	6	63262	01145 01148	0	o8852	53
š	14 56 14 48	45 4 45 12	35590 35644 35698	7	64356 64302	36795 36852	7	63205 63148	01151 01154	:	98849 98846	52 51
10	10 14 40	I 45 20	9. 35752	9	10. 64248	9. 36909	-	10. 63091	10. 01157	1	9. 98843	30
11	14 32	45 28	9. 35752 35806	10	64194	36966	10	63034	01160	1	98840	43
12 13	14 24 14 16	45 36 45 44	35860 35914	11	64140 64086	37023 37080	11	62977 62920	01 163 01 166	1	98837 98834	48
14	14 8	45 52	35968	12	64032	37137	13	62863	01169	i	08821	46
15 16	10 14 0	I 46 0	9, 36022	13	10. 63978	9. 37193	14	10, 62807	10, 01172	1	9. 98828	45
	13 52	46 8 46 16	36075 36129	14	63925 63871	37250 37306	15	62750 62694	01175 01178	I	98825 98822	44
17 18	13 44 13 30 13 28	46 24	36182	15 16	63818	37363	17	62637	01 181	i	98819	42
19		46 32	36236	17	63764	37419		62581	01184	1	98816	41
20 21	10 13 20	1 46 40 46 48	9. 36289 36342	18 18	63658	9- 37476	19	10, 62524 62468	10, 01 187	1	9. 98813 98810	40
22	13 4 12 56	46 56	36395	19	63605	37532 37588	20	62412	01193	1	98807	39 38
23	12 56 12 48	47 4 47 12	36449 36502	20	63551	37044	2 I 22	62356 62300	01196	1	98804 98801	37 36
24	10 12 40	1 47 20	0. 26555	22	63498 10. 63445	37700 9-37756	23	10, 62244	01199 IO, 01202	÷	9. 98798	35
25 26	12 32	47 98	9. 36555 36608	23	63392	27812	24	10. 62244 62188	01205	1	98795	34
27 28	12 24 12 16	47 36 47 44	36660 36713	24 25	63340 63287	37868 37924	25 26	62132 62076	01208	1 1	98792 98789	33 32
29	12 8	47 52	36766	25	63234	37980	27	62020	01214	;	98786	31
30	10 12 0	1 48 0	9. 36819	26	10. 63181	9. 38035	28	10. 61965	10, 01217	2	9. 98783	30
31 32	11 52	48 8 48 16	36871 36924	27	63129 63076	38091 38147	29 30	61909	01220 01223	2	98780 98777	29 28
33	11 44 11 36	48 24	36976	29	63024	38202	31	61798	01220	2	08774	27 28
34	11 28	48 32	37028	30	62972	38257	32	61 743	01229	8	98771	
35 36	10 11 20 11 12	1 48 40 48 48	9. 37081 37133	31 32	10, 62919 62867	9. 38313 38368	32 33	10. 61687 61632	10. 01232 01235	2 2	9. 98768 98765	25 24
37 38	11 4	48 50	37185	32	62815	38423	34	61577	01238	2	98762	23
38	10 56 10 48	49 4	37237 37289	33	62763 62711	28470	35 36	61521 61466	01241 01244	2 2	98759 98756	22 21
39 40	10 10 40	49 12 I 49 20	9- 37341	34	10. 62659	38534 9. 38589	37	10, 61411	10, 01247	2	0. 08753	20
41	10 32	49 28	37393	35 36	62607	38644	37 38	61356	01250	2	98750	19 18
43	10 24	49 36 49 44	37445 37497	37 38	62555 62503	38699	39 40	61301 61246	01254 01257	2 2	98746 98743	18
44	10 8	49 52	37549	39	62451	38754 38868	41	61192	01260	2	98740	17 16
45 46	10 10 0	1 50 0	9. 37600	39	10, 62400	9. 38863	42	10. 61137	10, 01263	2	9. 98737	15
40	9 52 9 44	50 8 50 16	37652 37703	40 41	62348 62297	38918 38972	43 44	61082	01266 01260	2 2	98734 98731	14
47 48	9 36	50 24	37755 37806	42	62245	20027	45	60973	01272		98728	12
49	9 28	50 32	37806	43	62194	39082	45	60918	01275		98725	11
50 51	10 9 20 9 12	1 50 40 50 48	9. 37858 37909	44	10. 62142 62091	9. 39136	46 47	60810	10. 01278	3	9. 98722 98719	10
52	9 4 8 56	50 56	37960	45	62040	39245	47 48	60755	01285	3	98715	8
53 54	8 56 8 48	51 4 51 12	38011 28062	47	61989 61938	39299 39353	49 50	60701 60647	01288	3	98712 98709	7
55	IO 8 40	1 51 20	9. 38113	48	10.61887	9, 39407	51	10, 60593	10, 01294	3	9. 98706	5
55 56	8 33	51 28	38,64	49	61836	39461	52	60539 60485	01297	3	98703	4
57 58	8 24 8 16	51 36 51 44	38215 38266	50 51	61785 61724	39515 395%	53 54	60485 60431	01300	3	98700 98697	3 2
59	88	51 52	38317	52	61734 61683	39623	55	60377	01306	3	98694	1
80	8 0	52 0	38368	53	61632	39677	56	60323	01310	3	98690	·
M.	Hour r. M.	Hour A. M.	Cosine.	Diff.	Secant.	Cotangent.	Diff.	Tangent.	Cosecant.	Diff.	Sine.	M.
103	•											76°

SINES, TANGENTS, AND SEC	S.	TANGENTS	AND	SECANTS	
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14.			24412	~, .		110, 11	10	BECANI				
N.	********	Hour P. M.	Sine.	Diff.	Cosecant.	Tangent.	Diff.	Consessed	Secant	Dig.		165.
_	Hour A. M.			-			-	Cotangent.			Cosine.	×.
î	10 8 0 7 52	1 52 0 52 8	9. 38368 38418	0	10, 61632 61582	9. 39677	°	10. 60323 60260	01313	8	9. 98690 98687	60
2	7 44 7 30	52 16	38469	2	61531 61481	39731 39785	2	60215	01316	l۰l	98684	52 58
3	7 36 7 28	52 24	38519	2	61481	39838	3	60162 60108	01319	٥	98681	57
4	10 7 20	52 32 1 52 40	38570 9. 38620	3	61430	39892 9-39945	4	10, 60055	01 322 10. 01 325	- 0	98678 9. 98675	56
5	7 12	52 48	38670	5	61330	39999		60001	01 329		03671	55 54
7	7 4 6 56	52 56	38721		61279	40052	ş	59948 59894	01332	•	98668	53
	6 48	53 4 53 12	38771 38821	7	61229	40106 40159	7	59894 59841	01335 01338	:	98665	52 51
10	10 640	1 53 20	0, 38871	8	10, 61129	9. 40212	9	10. 59788	10, 01341	1	9. 98659	50
11	6 32	53 28	38921 38971	9	61079 61029	40266	10	59734 59681	01344 01348	!!	98656 98652	49 48
13	6 24	53 36 53 44	39021	10	60979	40319 40372	10	59628	01351	1 1	98649	42
14	6 8	53 52	39071	11	60929	40425	12	59575	01354	1	98646	47 46
15	10 6 0	1 54 0 54 8	9. 39121	12	10, 60879 60830	9. 40478	13	10, 59522	10, 01357	1	9. 98643	45
	5 52 5 44	54 8 54 16	39170 39220	13	60780	40531 40584	14	59469 59416	01360 01364	;	98640 98636	44
17 18	5 44 5 36	54 24	39270	15	60730	40030	15	59364	01367	1	98633	42
19	5 28	54 32	39319	15	60681	40689	17	59311	01370	1	98630	41
20 21	10 5 20 5 12	1 54 40 54 48	9. 39369 39418	16 17	10, 60631 60582	9. 40742	17	10. 59258 59205	10. 01373	1	9. 98627 98623	20
22	5 4	54 56	39467	18	60533 60483	40795 40847	19	59153	01377 01380	1	98620	39 38
23 24	4 56 4 48	55 4 55 12	39517 39566	19	60483 60434	40900 40952	20 21	59100 59048	01383 01386	1	98617 98614	37 36
25	10 4 40	1 55 20	9. 39615	20	10, 60385	9. 41005	22	10. 58995	10, 01390	1	9. 98610	35
26	4 32	55 28	39664	21	60336	41057	23	58043	01393	1	98607	34
27 28	4 24	55 36 55 44	39713 39762	23	60287 60238	41109 41161	23	58891 58839	01396	;	98604	33
29	4 8	55 44 55 52	39811	24	60189	41214	24 25	58786	01399 01403	3	98597	32 31
30	10 4 0	1 56 O	9. 39860	24	10, 60140	9. 41266	26	10. 58734 58682	10. 01406	2	9. 98594 98591 98588	30
31 32	3 52 3 44	56 8 56 16	39909 39958	25 26	60091 60042	41318	27 28	58682 58630	01409 01412	2 2	98591	29 28
33	3 36	56 24	40006	27	59994	41422	29	58578	01416	2	98584	27
34	3 28	56 32	40055	28	59945	41474	30	58526	01419	2	98581	
35 36	10 3 20 3 12	1 56 40 56 48	9. 40103	29 29	10. 59897 59848	9. 41526 41578	30 31	10. 58474 58422	10, 01422 01426	2 2	9. 98578 98574	25 24
37 38	3 4	56 56	40200	30	59800	41629	32	58371	01429	2	98571 98568	23
38	2 56 2 48	57 4 57 12	40249	31 32	59751	41681	33	58319 58267	01432	2 2	98568 98565	22
39 40	10 2 40	57 12 1 57 20	9. 40346	33	59703 10. 59654	9.41784	34	10. 58816	10. 01435	2	9. 98561	20
41	2 32	57 28	40394	33	59606	41836	35 36	58164	01442	3	98558	19 18
42	2 24 2 16	57 36 57 44	40442 40490	34	59558	41887	36	58113 58061	01445 01449	2 2	98555 98551	18
43 44	2 8	57 44 57 52	40538	35 36	59510 59462	41939 41990	37 38	58010	01452	:	98548	17 16
45 46	10 2 0	1 58 o	9. 40586	37	10. 59414	9. 42041	39	10. 57959	10. 01455	2	9. 98545	15
	1 52 I 44	58 8 58 16	40634 4068a	37 38	59366 59318	42093 42144	40	57907 57856	01459 01462	3	98541 98538	14
47 48	1 36	58 24	40730	39	59310	42195	42	57805	01465	3	08535	13 12
49	1 28	58 32	40778	40	59222	42246	43	57754	01469	3	98531	11
50 51	10 1 20 I 12	1 58 40 58 48	9. 40825 40873	41 42	10. 59175 59127	9. 42297 42348	43 44	10. 57703 57652	10. 01472 01475	3 3	9. 98528	10
52	14	58 56	40921	42	59079	42399	45	57601	01479	3	98521	8
53	0 56	59 4	40968 41016	43	59032 58984	42450	45 46	57550	01482	3	98518 98515	7
54	0 48 10 p 40	59 12 1 59 20	9. 41003	44	10. 58022	42501 9. 42552	47	57499 IO. 57448	01485	3	9-98511	3
55 56	0 32	59 28	41111	45 46	10. 58937 58889	⊿2 602	49	57397	01492	3	98508	4
57 58	0 24	59 36	41158	46	58842 58795	42653	50	57347	01495	3	98501 98501	3
50 59	0 8	59 44 59 52	41252	47 48	58748	42704 42755	50 51	57296 57245	01499 01502	3	98498	1
59 60	0 0	2 0 0	41300	49	58700	42755 42805	52	57195	01506	3	98494	•
M.	Hour P. M.	Hour A. M.	Cosine.	Diff.	Secant.	Cotangent.	Diff.	Tangent.	Conecant.	Dig.	Sine.	M.
104	,						_					750

			_			_				_		161
M.	Hour A. M.	Hours, M.	Sine.	Diff.	Cosecant.	Tangent.	Diff.	Cotangent.	Secant	Diff.	Cosine.	24
0	10 0 0	2 0 0	9.41300	0	10, 58700	9. 42805	0	10. 57195	10. 01505	0	9. 98494	6
1	9 59 52	0 8	41347	1	58653	42856	1	57144	01509	0	98491	5
2	59 44	0 16	41394	2	58606	42996	- 3	57094	01512	0	98488	5
3	59 36	0 24	41441	2	58559	42957	2	57043	01516	0	98484	5
4	59 28	0 32	41488	3	58512	43007	3	56993	01519	0	98481	5
56	9 59 20	2 0 40	9. 41535	4	10. 58465	9. 43057	4	10. 56943	10, 01523	0	9. 98477	1 5
6	59 12	0 48	41532	5	58418	43108	5	56192	01526	0	98474	5
7	59 4	0 56	41628	5	58392	43158		56842	01529	0	98471	5
	58 56	1 4	41675		58,325	43208	7	56792	01533	0	98467	3
9	58 48	1 12	41722	7	58278	43258	7	56742	01536	1	98464	3
101	9 58 40	2 I 20	9. 41769	- 8	10, 58232	9. 43308	8	10. 56692	10, 01540	1	9. 98460	3
L	58 32	1 28	41815	8	58185	43358	9	56642	01543	1	95457	14
12	58 24	1 36	41861	9	58139	43408	10	56592	01547	1	98453	×
13	58 16	1 44	41908	10	58092	43458	11	56542	01550	1	98450	1
14	58 8	1 52	41954	11	58046	43508	11	56492	01553	. 1	98447	1
15	951 0	2 2 0	9. 42001	11	10. 57999	9. 43558	12	10, 55442	10, 01557	1	9. 98443	14
16	57.52	2 8	42047	12	57953	43007	13	56393	01560	1	98440	L
17	57 44	2 16	42003	13	57007	43557	14	56343	01504	1	98436	1
	57 36	2 24	42140	14	57860	43707	15	56293	01567	1	98433	14
19	57 28	2 32	42186	14	57814	43756	16	56244	01571	1	98429	1.
to:	0 57 20	2 2 40	9-42733	15	10. 57768	9. 43806	16	10, 56194	10.01574	T	9. 98426	F.
15	57 12	2 48	42278	16	57722	43855	17	56145	01578	1	98422	ŀ
22	57 4	2 56	42324	17	57676	43905	18	56095	01581	1	98419	ы
13	56 56	3 4	42370	17	57630	43954	19	56046	01585	1	98415	п
24	56 48	3 12	42416	18	575B4	44004	20	55996	01588	1	98412	L
25	9 56 40	2 3 20	9. 42461	10	10. 57539	9. 44053	20	10, 55947	10, 01591	1	9. 98300	Г
25	56 32	3 28	42507	20	57493	44102	21	55898	01595	2	98405	lá
27	56 24	3 36	42553	21	57447	44151	22	55849	01598	2	98402	П
8	56 16	3 44	42599	21	57401	44301	23	55799	01002	2	98308	U
29	56 B	3 52	42044	22	57356	44250	24	55750	01605	2	95395	1
30	9 56 0	2 4 0	9. 42590	23	10, 57310	9. 44299	25	10, 55701	10, 01600	2	9. 98391	t
11	55 52	4 8		24	57265	44348	25	55652	01612	2	98388+	L
12	55 44	4 16	42735 42781	24	57219	44397	26	55603	01616	2	98384	1 :
33	55 36	4 24	42526	25	57174	44446	27	55554	01610	2	98381	1 :
14	55 28	4 32	42872	26	57128	44495	28	55505	01623	2	98377	L
15	9 55 20	2 4 40	9. 42917	27	10, 57083	9. 44544	29	10, 55456	10, 01627	2	9. 98373	١
36	55 12	4 48	42962	27	57038	44502	20	55408	01630	2	98370	L
	55 4	4 56	4,3008	28	56992	44641	30	55359	01534	2	98366	П
37	54-56	5 4	43053	20	56947	44690	31	55310	01637	2	98363	L
19	54 48	5 12	43098	10	50002	44738	32	55262	-01641	2	98359	1
10	9 54 40	2 5 20	9. 43143	30	10, 56857	9-44787	33	10, 55213	10. 01644	2	9. 98356	t
11	54 32	5 28	43188	31	56812	44836	34	55164	01648	2	98352	l.
12	54 24	5 36	43233	32	56767	44884	34	53116	01651	2	98349	i.
43	54 16	5 44	43278	33	56722	44933		55067	01655	3	98345	L
14	54 8	5 52	43323	33	56677	44981	35	55010	01658	3	98342	ь
	954 0	2 6 0	9,43367	34	10, 56633	9. 45029		10, 54971	10, 01662		9. 98338	t
5	53 52	6 8	43412	35	56588	45078	37	54922	01666	3	98334	Г
7	53 44	6 16	43412	35	56543	45126	38	54874	01669	3	98331	
7 8	53 30	6 24	43502	36	56498	45174	39	54826	01673	3	98327	l
49	53 28	6 32	43546	37	56454	45222	40	54778	01676	3	98324	L
0	24	2 6 40		38	10, 56409		41	10, 54729	10, 01580		9, 98120	
1	9 53 20 53 12	6 48	9- 43591	39	56365	9. 45271	42	54681	01683	3	98317	ľ
2	53 4	6 56	43035 43680	39	56320	45367	43	Eafora	01687	3	98313	1
3	53 4 52 56	7 4	43724	40	56276	45415	43	54633 54585	01691	3	98300	1
54	52 48	7 12	43769	41	56231	45463	44		01694	3	98306	I
	9 52 40			-				54537	10, 01608	-		+
56		1 - 1	9, 43813	43	10, 56187	9-45511	45	10, 54489		3	9, 98302	1
17	52 32		43857	43	56143	45559	45	54441	01701	3	98299	ı
57	52 24	7 36	43901	43	56099	45000	47	54394		3	98195	1
20	52 16 52 8	7 44	43946	44	56054	45654	47	54346	01709	3	G8253	1
59	5a 8	7 53	43990	45	56010	45702	48	54298	01713	3	98284	i
		8 0	44034	46	55966	45750	49	54250	01716	4	90404	1
M.	9- "		11.41				-		_	-	-	1.5

193

100		· · ·									1	168.
M.	Hout a. m.	Hour P. M.	Sine.	DIF.	Concent.	Tangent.	DIF.	Cotangent.	Secent.	Diff,	Cosine.	M.
0	9530	280	9-44034	0	10. 55966	9-45750	0	10. 54250	10, 01716	0	9. 98284	60
I	51 53	8 8	44078	1	55922	45797 45845	1	54203	01719	٥	98281	5% 58
2	51 44 51 36	8 16 8 24	44122 44166	1 2	55878 55834	45845 45892	2	54155 54108	01723 01727	0	98277 98273	50
3	51 36 51 28	8 32	44210	3	55790	45940	3	54060	01730	اۃ	98270	57 56
ş	9 51 20	2 8 40	9.44253	4	10. 55747	9.45987	4	10. 54013	10. 01734	0	9. 98266	55
	51 12	8 48	44297	4	55703 55659	46055 46082	5	53965	01738	0	98262	54
7	51 4 50 56	8 56	44341	8	55659	46082	. 8	53918	01741	0	98259	53
ŝ	50 56 50 48	9 4	44385 44428	6	55615 55572	46130 46177		53870 53823	01745 01749	0	98255 98251	52 51
10	9 50 40	2 9 20	9-44472		10. 55528	9, 46224	7	10. 53776	10. 01752	i	9. 98248	50
11	50 32	9 28	44516	7	55484	46271	و	53729	01756	1	98244	42 48
12	50 24 50 16	9 36	44550	9	55441	46319		53681	01760	1	98240	48
13	50 16 50 8	9 44 9 52	44602 44646	10	55398	46366 46413	10	53634 53587	01763 01767	I	98237 98233	47 46
15	9 50 0	2 10 0	9, 44689	11	55354	0.46460	12	10. 53540	10, 01771	+	9. 98229	45
16	49 52	10 8	44733	ii	55267	46507	12	53493	01774	l ;	98226	144
17	49 44 49 36	10 16	44776 44819	12	55224	46554 46601	13	53446	01778	1	98222	43
18		10 24	44819	13	55181	46601	14	53399	01782	1	98218	42
19 20		10 32	44862	14	55138	46648 9, 46694	15	53352	10, 01789	1	98215	41
21	9 49 20 49 12	2 10 40 10 48	9. 44905 44948	14	10. 55095 55052	9, 40094	15 16	10. 53306 53259	01793	1	98207	
22		10 56	44992	16	55008	46741 46788		53212	01796	l i	98204	39 38
23	49 4 48 56	11 4	45035	16	54965	∡68 2 5	17	53165	01800	1	98200	37 36
24	48 48	11 12	45077	17	54923	46881	19	53119	01804	1	98196	
25 26	9 48 40 48 32	2 11 20	9. 45120	18	10, 54880 54837	9. 46928 46975	19	10. 53072 53025	10, 01808	2	9. 98192	35 34
	48 24	11 36	45163 45200	19	54794	47021	21	52979	01815		98185	33
27 28	48 16	11 44	45249	20	54751	47068	22	52032	01819	2	98181	32
29	48 8	11 52	45292	21	54708	47114	22	52886	01823	2	98177	31
30	9 48 0	2 12 0	9-45334	21	10. 54666	9.47160	23	10. 52840	10, 01826	2	9. 98174 98170	30
31 32	47 52 47 44	12 8	45377 45419	22	54623 54581	47207 47253	*	52793 52747	01830	2	98170	20 28
33	47 36	12 24	45462	23	54538	47299	25	52701	01834 01838	2	98162	27
34	47 28	12 32	45504	24	54496	47346	26	52654	01841	2	98159	26
35 36	9 47 20	2 12 40	9-45547 45589 45632	25 26	10. 54453	9-47392	27	10, 52608	10. 01845 01849	2 2	9. 98155	25
30	47 12 47 4	12 48 12 56	45509	26	54411 54368	47438 47484	20	52562 52516	01862	3	98151 98147	24 23
37 38	_46 <6	13 4	45074	27	54326	47530	29	52470	01853 01856	2	98144	22
39	46 48	13 12	45716	28	54284	47576	30	52424	01860	2	98140	21
40	9 46 40	2 13 20	9-45758 45801	28	10, 54242	9. 47622	31	10, 52378	10, 01864 01868	3	9, 981 36	20
41 42	46 32 46 24	13 28 13 36	45801	29 30	54199 54157	47668 47714	32 32	52332 52286	01871	3	98132 98129	19 18
43	46 16	13 44	45843 45885	31	54115	47760	33	52240	01875	3	98125	17
44	468	13 52	45927	31	54073	47760 47806	34	52194	01879	3	98121	
45 46	9 46 0	2 14 0	9. 45969	32	10. 54031	9.47852	35 36	10, 52148	10, 01883	3	9. 98117	15
40	45/32 45 44	14 8 14 16	46053 46053	33 33	53989 53947	47897	36 36	52103 52057	01890	3	98113 98110	14
47 48	45 36	14 24	46095	34		47943 47989	37	52011	01804	3	98106	12
49	45 28	14 32	46136	35	53905 53864	48035	37 38	51965	01898	3	98102	11
50	9 45 20	2 14 40	9. 461 78	36	10, 53822	9, 48080	39	10, 51920	10, 01902	3	9, 98098	10
51 52	45 12	14 48 14 56	46220 46262	36	53780	48126 48171	39 40	51874 51829	01906	3	98094 98090	8
53	45 4 44 56	14 56 15 4	46303	37 38	53738 53697	48217	41	51783	01913	3	98087	3
54	44 48	15 12	46345	38	53655	48262	42	51738	01917	3	98083	
55 56	9 44 40	2 15 20	9. 46386	39	10, 53614	9. 48307	43	10, 51693	10, 01921	3	9. 98079	5
56	44 32	15 28	46428 46460	40	53572	48353	43	51647 51602	01925	3	98075 98071	4
57 58	44 24	15 36 15 44	46511	41 41	53531 53489	48398 48443	14	51557	01929	4	98067	3
59	44 8	15 52	46552	42	53448	48480	45	51511	01937	4	08063	1
60	44 0	16 0	46594	43	53406	48534	46	51466	01940	4	98060	•
M.	liour p. m.	Hour A. M.	Cosine.	Diff.	Secknt.	Cotangent.	Dif.	Tangent.	Cosecant.	Diff.	Sine.	M.
106												73°

17*			221.23	~, -				,	~•			162"
M.	Hour a. m.	Hour P. M.	Sine.	Diff.	Cosecant.	Tangent.	Diff.	Cotangent.	Secant.	Dif.	Cosine.	M.
۰	9 44 0	2 16 0	9. 46594	۰	10. 53406	9-48534	•	10. 51466	10, 01940	۰	9. 98060	60
1 2	43 52 43 44	16 8 16 16	46635 46676	1	53365 53324	48579 48624	1	51421 51376	01944	°	98056 98052	59 58
3	43 36	16 24	46717	2	53283	48669	2	51331	01952	0	98048	57 56
4	43 28	16 32	46758	3	53242	48714	3	51286	01956	0	98044	
ş	9 43 20 43 12	2 16 40 16 48	9. 46800 46841	3	10. 53200 53159	9. 48759 48804	4	10, 51241 51196	10,01960	8	9. 98040 98036	55 54
7	43 4	16 56	46882	5	53118	48849	ş	51151	01964 01968	0	98032	53
8	42 56 42 48	17 4	46923 46964	8	53077 53036	48894 48939	7	511061	01971 01975		98029 98025	52 51
10	9 42 40	2 17 20	9. 47005	7	10. 52995	9. 48984	7	10. 51016	10. 01979	H	9, 98021	50
11	42 32	17 28	47045	7	52955	49029		50971	01983	1	98017	49 48
12	42 24 42 16	17 36 17 44	47086 47127	9	52914 52873	49073 49118	9	50927 50882	01987 01991	;	98013	48 47
14	42 8	17 52	47168	ģ	52832	49163	10	50837	01995	1	98005	46
15 16	9 42 0	2 18 0 18 8	9. 47209	10	10, 52791	9. 49207	111	10. 50793	10, 01999	1	9. 98001	45
17	41 52 41 44	18 8 18 16	47249 47290	11	52751 92710	49252 49296	12 12	50748 50704	02003	1 1	97997 97993	44 43
18	41 36	18 24	47330	12	52670	49341	13	50659	02011	1	97993 97989	42
19	41 28	18 32	9. 47411	13	52629 10. 52589	49385	14	50615	02014	1	97986	41 40
21	9 41 20 41 12	18 48	47452	14	52548	49474	15 16	50526	02022	1	9. 97982 97978	39
22	41 4	18 56	47492	15	52508	49519		50481	02026	ı	97974	39 38
23 24	40 56 40 48	19 4 19 12	47533 47573	15	52467 52427	49563 49607	17	50437 50393	02030 02034	2 2	9797° 97966	37 36
25	9 40 40	2 19 20	9. 47613	17	10. 52387	9. 49652	18	10. 50348	10. 02038	3	9. 97962	35
26	40 32	19 28 19 36	47654	17	52346	49696	19	50304 50260	02042	2 2	97958	34
27 28	40 24 40 16	19 36 19 44	47694 47734	19	52306 52266	49740 49784	21	50216	02046 02050	2	97954 97950	33 32
29	40 8	19 52	47774	19	52226	49828	21	50172	02054	2	97946	31
30 31	9 40 0 39 52	2 20 0	9.47814 47854	20	10, 52186 52146	9. 49872 49916	22	10. 50128 50084	10, 02058	2 2	9. 97942 97938	30 29
32	39 44	20 16	47894	21	52106	49960	24	50040	02005	3	97934	28
33	39 36	20 24	47934	22	52066 52026	50004	24	49996	02070	2	97930	27
34	9 39 20	20 32	47974 9. 48014	23	10, 51986	50048 9, 50092	25	49952 10, 49908	02074	-	97926	25
35 36	39 12	20 48	48054	24	51946	50136	26	49864	02082	3	97918	24
37 35	39 4 38 56	20 56 21 4	48094 48133	25 25	51906 51867	50180 50223	27 28	49820 49777	02086 02090	3	97914 97910	23
39	38 48	21 12	48173	26	51827	50267	29	49733	02094	3	97906	21
40	9 38 40	2 21 20	9. 48213	27	10. 51787	9.50311	29	10. 49689	10. 02098	3	9. 97902	20
41 42	38 32 38 24	21 28	48252 48292	27 28	51748 51708	50355 50398	30 31	49645 49602	02102	3	97898 97894	19 18
43	38 16	21 44	48332	29	51668	50442 50485	32	49558	02110	3	07800	17
44	38 8	21 52	48371	29	51629 10, 51589	50485	32	49515	02114	3	97886	16 15
45 46	9 38 o 37 52	2 22 0	9. 48411 48450	30 31	51550	9. 50529 50572	33	10, 49471 49428	02122	3	9. 97882 97878	15
47 48	37 44	22 16	48490	31	51510	50616	35	49384	02126	3	97874	13
48 49	37 36 37 28	22 24 23 32	48529 48568	32 33	51471 51432	50659 50703	35 36	49341 49297	02130 02134	3	97870 97866	12
50	9 37 20	2 22 40	9. 48607	33	10,51393	9. 50746	37	10. 49254	10. 02139	3	9. 97861	10
51	37 12	22 48 22 56	48647 48686	34	51353	50789	37 38	49211	02143	3	97857 97853	8
52 53	37 4 36 56	22 56	48725	35 35	51314 51275	50833 50876	39	49167 49124	02147 02151	3	97849	7 6
54	36 48	23 12	48764	35 36	51236	50919	40	49081	02155	4	97845	
55 56	9 36 40 36 32	2 23 20 23 28	9. 48803 48842	37	10. 51197 51158	9. 50962	40 41	10, 49038 48995	10, 02159	4	9. 97841 97837	5
57 58	36 24	23 36	48881	37 38	51119	51048	42	48052	02167	4	97833	3
	36 16	23 44	48920	39	51080	51092	43	48908 48865	02171	4	97829 97825	2
59 60	36 8 36 0	23 52	48959 48998	39 40	51041 51002	51135 51178	43	48822	02175 02179	4	97821	;
M.	Hour P. M.	Hour A. M.	Cosine.	Diff.	Secant.	Cotangent	Diff.	Tangent.	Conecant.	Diff.	Sine.	N.
107	` 	·		'		L		·	·			790
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18°											1	161*
M.	Houra. M.	Hour P. M.	Sine.	Diff.	Cosecant.	Tangent.	Diff.	Cotangent.	Secant.	Diff.	Cosine.	M.
۰	9360	8 24 0	9. 48998	٥	10. 51002	9. 51178	0	10. 48822	10.02179	0	9. 97821	60
1 2	35 52 35 44	24 8 24 16	49037 49076	ı	50963 50924	51221 51264	I	48779 48736	02183	°	97817	59 58
3	35 44 35 36	24 24	49115	•	50885	51306	;	48694	02192	اة ا	97808	27
4	35 28	24 32	49153	, 3	50847	51349	3	48651	02196	٥	97804	57 56
5	9 35 20	2 24 40	9. 49192	3	10, 50808	9. 51392	3	10.48608	10, 02200	•	9. 97800	55
6	35 12	24 48	49231 49269	4	50769	51435	4	48565 48522	02204	°	97796	54
3	35 4 34 56	24 56 25 4	49308	4	50731 50692	51478 51520	5	48480	02208	1 3	97792 97788	53 52
9	34 48	26 12	49347	5	50653	51563	6	48437	02216	i	97784	57
10	9 34 40	2 25 20	9. 49385	6	10. 50615	9. 51606	7	10, 48394	10, 02221	1	9-97779	50
11	34 32	25 28	49424	7	50576	51648	8	48352	02225	1 1	97775	49
12	34 24 34 16	25 36 25 44	49462 49500	8	50538 50500	51691 51734	9	48309 48266	02229 02233	1	97771 97767	48 47
14	34 8	25 52	49539	١٥	50461	51776	10	48224	02237	l i l	97763	46
15 16	9 34 0	2 26 0	9-49577	9	10. 50423	9. 51819	10	10, 48181	10, 02241	1	9- 97759	45
	33 52	26 8	49615	10	50385	51861	11	48139	02246	1	97754	44
17 18	33 44 33 36	26 16 26 24	49654 49692	11	50346 50308	51903 51946	13	48097 48054	02250 02254	:	97750	43
19	33 28	26 32	49730	12	50270	51988	13	48012	02258	1	97746 977 42	42 41
20	9 33 20	2 26 40	9. 40768	13	10, 50232	9. 52031	14	10. 47969	10. 02262	1	9. 97738	40
21	33 12	26 48	49806	13	50194	52073	15	47027	02266	1	97734	39 38
22	33 4	26 56	49844 49882	14	50156	52115	15	47885	02271	3	97729	38
23 24	32 56 32 48	27 4 27 12	49002	14	50118 50080	52157 52200	17	47843 47800	92275 02279	2	97725 97721	37 36
25	9 32 40	2 27 20	9. 49958	16	10, 50042	9. 52242		10. 47758	10. 02283	1	9-97717	35
25 26	32 32	27 28	49996	16	50004	52284	17 18	47716	02287	2	97713	34
27	32 ,24	27 36	50034	17	49966	52326	19	47674	02292	3	97708	33
28 29	32°16	27 44 27 52	50072	18	49928 49890	52368 52410	20	47632	02296	2 2	97704	32
30	9 32 0	2 28 0	9, 50148	19	10, 49852	9. 52452	21	47590 10. 47548	10, 02304	3	97700	31
31	31 52	28 8	50185	20	49815	52494	23	47506	02300	3	97691	20
32	31 44	28 16	50223	20	49777	52536	22	47464	02313	2	97687	20 28
33	31 36 31 28	28 24 28 32	50261	21	49739	52578 52620	23	47422	02317	2	97683	27 26
34	31 28	2 28 40	50298 9. 50336	21	10, 49664	9. 52661	24	47380	02321	2	97679	
35 36	31 12	28 48	50374	23	49626	52703		10. 47339 47297	02330	3	9. 97674 97670	25 24
37 38	31 4	28 56	50411	23	49589	52745 52787	25 26	47255	02334	3	97666	23
38	30 56 30 48	29 4	50449	24	49551	52787	27	47213	02338	3	97662	23
39 40	.9 30 48	29 12	50486 9. 50523	25	49514	52829 9. 52870	27	47171	02343	3	97657	2[
41	30 32	29 28	50561	25 26	10. 49477 49439	52912	29	10. 47130 47088	10. 02347 02351	3 3	9. 97653 97649	20 19
43	30 24	29 36	50598	26	40402	52953	29	47047	02355	3	97645	18
43	30 16	29 44	50635	27	49365	52995	30	47005	02360	3	97640	17
44	30 8 9 30 0	29 52 2 30 0	9. 50710	28	49327	53037	31	46963	02364	3	97636	16
45 46	29 52	30 8	9. 50710 50747	20	10, 49290 49253	9. 53078 53120	31 32	10, 46922 46880	10, 02368	3 3	9.97632 97628	15 14
47 48	29 44	30 16	50784	30	49216	53161	33	46839	02377	3	97623	13
	29 36	30 24	50821	30	49179	53202	34	46798	02381	3	97619	12
49	29 28	30 32	50858	31	49142	53244	34	46756	02385	_3_	97615	11
50 51	9 29 20	2 30 40 30 48	9, 50896 50933	31	10. 49104 49067	9. 53285 53327	35 36	10. 46715 46673	10. 02390 02394	4	9. 97610 97606	10
52		30 56	50970	33	49030	53368	36	46632	02394	1	97602	8
53	29 4 28 56	31 4	51007	33	48993	53409	37 38	46591	02403	4	97597	7
54	28 48	31 12	51043	34	48957	53450	38	46550	02407	4	97593	
55 56	9 28 40 28 32	2 31 20 31 28	9. 51080 51117	35	10, 48920 48883	9. 53492	18 39	10. 46508 46467	10, 02411 02416	4	9. 97589 97584.	5
57	28 24	31 36	51154	35 36	48846	53533 53574	40	46426	02410	4	97580	1
57 58	28 16	31 44	51191	37	∡88 oq	53615	41	46385	02424	4	97570	3 2
59	28 8 28 0	31 52 32 0	51227	37 38	48773	53656	41	46344	02429	[4]	97571	اۃ
_			51264		48736	53697	42	46303	02433	-	97567	
м.	Hour P. M.	Hour A. M.	Cosine.	Diff.	Secant.	Cotangent.	Diff.	Tangent.	Cosecant.	Diff.	Sine.	M.
108	•											710

190				_							1	100°
M.	Hour A. M.	Hour P. M.	Sine.	Diff.	Cossoant.	Tangent.	DIA.	Cotangent.	Secant.	Diff.	Cosine.	M.
a	9 28 0	2 32 0	9. 51264	0	10. 48736	9. <u>53697</u> 53738	0	10. 46303	10, 02433	۰	9. 97567	60
1 2	27 52 27 44	32 8 32 16	51301 51338	1	48699 48662	5373° 53779	1	46262 46221	02437 02442	°	97563 97558	59 58
3	27 36	32 24	51374	2	48626	53820	2	46180	02446	0	97554	57 56
4	27 28	32 32	51411	2	48589	53861	3	46139	02450	0	97550	
5	9 27 20 27 12	2 32 40 32 48	9. 51447 51484	3	10. 48553 48516	9. 53902	3	10.46098 46057	10, 02455 02459	0	9- 97545 97541	55 54
7	27 4	32 56	51520	4	48480	53943 53984	5	46016	02464	1	97536	53
8	26 56 26 48	33 4 33 12	51557	5	48443 48407	54025 54065	5	45975	02468	I	97532	52
18	9 26 40	33 12 2 33 20	9. 51629	1 6	10. 48371	9. 54106	7	45935 10. 45894	10, 02477	÷	97528 9-95523	51 50
111	26 32	33 28	51666	7	48334 48298	54147	7	45853	02481	1	97519	49 48
12	26 24 26 16	33 36	51702	7	48298 48262	54187		45813	02485	1	97515	
13 14	26 8	33 44 33 52	51738 51774	8	48226	54228 54269	9	45772 45731	02490 02494	1	97510 97506	47 46
15	9 26 0	2 34 0	9. 51811	9	10, 48189	9 54309	10	10. 45691	10, 02499	1	9. 97501	45
16	25 52	34 8 34 16	51847 51883	10	48153 48117	54350	11	45650	02503	1	97497	44
17 18	25 44 25 36	34 16 34 24	51919	11	48081	54390 54431	11	45610 45569	02508	1	97492 97488	43 42
19	25 28	34 32	51955	11	48045	54471	13	45529	02516	ī	97484	41
20	9 25 20	2 34 40	9. 51991	12	10, 48009	9. 54512	13	10. 45488	10, 02521	1	9- 97479	40
2I 22	25 12 25 4	34 48 34 56	52027 52063	12 13	47973 47937	54552	14	45448 45407	02525 02530	2 2	97475 97470	39 38
23	24 56	35 4	52099	14	47901	54593 54633	15	45367	02534	2	97466	37 36
24	24 48	35 12	52135	14	47865	54673		45327	02539	2	97461	
25 26	9 24 40 24 32	2 35 20 35 28	9. 52171 52207	15	10. 47829 47793	9. 54714 54754	17	10. 45286 45246	10. 02543	2 2	9- 97457	35 34
27 28	24 24	35 36	52242	16	47758	54794 54835	17	45206	02552	2	97453 97448	33
	24 16 24 8	35 44	52278	17	47722 47686	54835	19	45165	02556	2	97444	32
29 30	9 24 0	35 52 2 36 0	9. 52350	18	10.47650	54875 9. 54915	19 20	45125 10, 45085	10. 02565	2	97439 9- 97435	31 30
31	23 52	36 8	52385	18	47615	54955	21	45045	02570	2	97430	29 28
32	23 44 23 36	36 16	52421	19 20	47579	54995	21 22	45005	02574	2	97426	28
33 34	23 36 23 28	36 24 36 32	52456 52492	20	47544 47508	55°35 55°75	23	44965 44925	02579	3	97421 97417	27 26
35 36	9 23 20	2 36 40	9. 52527	21	10. 47473	9. 55115	23	10, 44885	10, 02588	3	9- 97412	25
36	23 12 23 4	36 48 36 56	52563 52598	21 23	47437 47402	55155	24	44845 44805	02592	3	97408	24
37 38	23 4 22 50	36 56 37 4	52634	23	47366	55195 55235	25 25	44765	02597	3	97403 97399	23 22
39	22 48	37 12	52669	23	47331	55275	25 26	44725	02606	3	97394	21
40 41	9 22 40	2 37 20 37 28	9. 52705	24	10. 47295 47260	9. 55315	27	10, 44685	10, 02610	3	9. 97390	20
42	22 24	37 28 37 36	52740 52775		47225	55355 55395	27	44645 44605	02619	3	97385 97381	19 18
43	22 24 22 16	37 44	52775 52811	25 26	47189	55434	29	44566	02624	3	97376	17 16
44	22 8 9 22 0	37 52 2 38 0	\$2846 9. 52881	26 27	47154	55474	29	44526 10. 44486	02628	3	97372	
45 46	9 22 0	38 8	52016	27	10. 47119 47084	9. 55514 55554	30 31	44446	10, 02633	3	9. 97367 97363	15 14
48	21 44	38 16	52951 52986	27 28	47049	55593	31	44407	02642	3	97358	13
48	21 36 21 28	38 24 38 32	52986 53021	29	47014 46979	55633 55673	32	443 ⁶ 7 443 ² 7	02647	4	97353 97349	12
50	9 21 20	2 38 AD	9. 53056	30		9. 55712	33	10. 44288	10, 02656	4	9- 97344	10
51	21 12	38 48	53092	30	10, 46944 46908	55752	34	44248	02660	4	97340	8
52	21 4 20 56	38 56 39 4	53126 53161	31 32	46874 46839	55791 55831	35	44209 44169	02665 02669	4	97335	
53 54	20 48	39 12	53196	32	46804	55870	35 36	44130	02674	1 2	97331 97326	7
55 56	9 20 40	2 39 20	9.53231	33	10. 46769	9. 55910	37	10, 44090	10. 02678	4	9. 97322	5
50	20 32 20 24	39 28 39 36	53266 53301	33 34	46734 46699	55949 55989	37 38	44051 44011	02683 02688	4	97317 97312	4 3
57 58	20 16	39 44	53336	34	46664	56028	39	43972	02692	4	97308	2
59	20 8 20 0	39 52	53370	35	46630	56067	39	43933	02697	4	97303	1
_		40 Q	53405	36	46595	56107	40	43893	02701	4	97299	٥
M.	Hour P. M.	Houra, M.	Cosine.	DIE.	Secant.	Cotangent.	Diff.	Tangent.	Cosecant.	Diff.	Sine.	Ж.
106			-									70°

STNES	TANGENTS.	AND	SEC VILLA

290						•						159°
м.	Hour A. M.	Hour P. M.	Sine.	Diff.	Cosecant.	Tangent.	Diff.	Cotangent.	Secant	DIN.	Cosine.	M.
0	9 20 0	2 40 0 40 8	9. 53405	٥	10. 46595	9. 56107	0	10. 43893	10, 02701	0	9. 97299	60
1 2	19 52 19 44	40 16	53440 53475	1	46560 46525	56146 56185	;	43854 43815	02706 02711	:	97294 97289	59 58
3	19 36	40 24	53509	2 2	46491	56224 56264	2	43776	02715	1 :	97285 97280	57 56
4	9 19 20	40 32 2 40 40	53544 9.53578	3	46456 10, 46422	9. 56303	3	43736 10. 43697	10. 02724	۱ %	9. 97276	55
8	19 12	40 48	53613	.3	46387	56342	4	43658	02729	0	97271	54
7	19 4 18 56	40 56 41 4	53647 53682	4	46353 46318	56381 56420	1 4	43619 43580	02734 02738	1:	97266 97262	53 52
9	18 48	41 12	53716	5	46284	56459	ş	43541	-02743	1	97257	51
10	9 18 40 18 32	2 41 20 41 28	9. 53751 53785	6	10. 46249 46215	9. 56498 56537	6	10. 43502 43463	10, 02748 02752	1	9. 97252 97248	50
12	18 24	41 36	£1810	7	46181	56576	8	43424	02757	1	97243	49 48
13	18 16 18 8	41 44	53854 53888	7	46146 46112	56615 56654	8	43385	02762 02766	1	97238	47
14	9 18 0	41 52 2 42 0	9. 53922	1 8	10, 46078	9. 56693	10	43346 10, 43307	10. 02771	l i	97234	46 45
16	17 52	8 دئما	53957	9	46043	56732	10	43268	02776	1	97224	44
17 18	17 44 17 36	42 16 42 24	53991 54025	10	46009 45975	56771 56810	11	43229 43190	02780 02785	1	97220 97215	43
19	17 28	42 32	54059	ii	45941	56849	12	43151	02790	Li	97210	41
20 21	9 17 20	2 42 40	9. 54093	II I2	10. 45907	9. 56887 56926	13	10. 43113 43074	10, 02794	2 2	9. 97206 97201	40
21	17 12 17 4	42 48 42 56	54127 54161	12	45873 45839	56965	13	43074	02799 02804	1 2	97196	39 38
23	16 56	43 4	54195	13	45805	57004	15	42996	02808 02813	2 2	97192	37 36
24 25	16 48 9 16 40	2 43 20	54229 9. 54263	14	45771	57042 9. 57081	15	42958	10, 02818	1 2	97187	36 35
26	16 32	43 28	54297	15	45703	57120	17	42880	02822	2	97178	34
27 28	16 24 16 16	43 36	54331 54365	15	45669 45635	57158 57197	17	42842 42803	02827 02832	2	97173 97168	33 32
29	16 8	43 44 43 52	54399	16	45601	57235	19	42765	02837	2	97163	31
30	9 16 0	2 44 0	9- 54433	17	10. 45567	9-57274	19	10, 42726 42688	10, 02841 02846	2	9-97159	30
31 32	15 52 15 44	44 8 44 16	54466 54500	17	45534 45500	57312 57351	20	42649	02851	3	97154 97149	29 28
33	15 36	44 24	54534	19	45466	57389	2I 22	42611	02855	3	97145	27 26
34	15 28 9 15 20	44 32 2 44 40	54567 9. 54661	20	45433 10. 45399	57428 9. 57466	22	42572 10. 42534	10, 02865	3	97140	25
35 36	15 12	44 48	54635 54668	20	45365	57504	23	42496	02870	3	97130	24
37 38	15 4 14 56	44 50	54668 54702	3I 2I	45332 45298	57543 57581	24	42457 42419	02874	3	97126	23
39	14 48	45 4 45 12	54735	22	45265	57619	25	42381	02879 02884	3	97116	21
40	9 14 40	2 45 20	9. 54769 54802	23	10. 45231	9. 57658	26 26	10, 42342	10, 02889 02893	3	9.97111	20
41	14 32 14 24	45 28 45 36	54836	23 24	45198 45164	57696 57734	27	42304 42266	02898	3	97107 97102	19 18
43	14 16	45 44	54869	24	45131	57772 57810	28 28	42228	02903	3	97097	17 16
45	9 14 0	45 52 2 46 0	54903 9. 54936	25 25	45097 10. 45064	9.57849	29	42190 10.42151	10. 02913	3	97092	15
46	13 52	46 8	54969	20	45031	57887	30	42113	02917	4	97083	14
47 48	13 44 13 36	46 16 46 24	55003 55036	26 27	44997 44964	57925	30 31	42075 42037	02922	1 1	97078	13
49.	13 28	46 32	55069	28	44931	57963 58001	31	41999	02932	4	97073 97068	11
50	9 13 20	2 46 40 46 48	9. 55102	28	10, 44898 44864	9. 58039 58077	32	10, 41961	10. 02937	4	9. 97063	10
51 52	13 12 13 4	46 56	55136 55169	29 29	44831	58115	33 33	41885	02941 02946	4	97059	8
53	12 56 12 48	47 4	55202	30	44798	58153 58191	34	41847 41800	02951	4	97049	7
54 55	9 12 40	47 12 2 47 20	55235 9. 55268	30 31	44765	9. 58229	35	10, 41771	02956	4	97044 9- 97039	5
56	12 32	47 28	55301	32	44699	58267	35 36	41733 41696	02965	4	97035	4
57 58	12 24 12 16	47 36 47 44	55334 55367	32 33	44666 44633	58304 58342	37	41696 41658	02970	4 5	97030 97025	3
59 60	12 8	47 52	55400	33	44600	58342 58380	37 38	41620	02975	5	97020	1
_	12 0	48 0	55433	34	44567	58418	39	41582	02985	5	97015	٥
м.	Hour P. M.	Houra. M.	Cosine.	Diff.	Secant.	Cotangent.	Diff.	Tangent.	Conscant.	Diff.	Sine.	M.
110	•											88.

210						_	1					1.5
M.	Hour A. M.	Hour e. se,	Sins.	Dia.	Conceant.	Tangent.	Diff.	Cotangent,	Secunt.	Diff.	Cosine,	Ŀ
0	9 12 0	2 48 0 48 8	9- 55433	0	10-44567	9. 58418	0	10, 41582	10, 02985	0	9. 97015	Р
1 2	11 52	48 8 48 16	55466	1	44534	58455 58493	1	41545	02990	0	97010	1
3	11 44	48 24	55499 55532	2	44501 44468	58531	2	41507	02995	0	97005	ı
4	11 28	48 32	55504	2	44436	58569	2	41431	03004	0	96996	ı
	9 11 20	2 48 40	9-55597	3	10, 44403	9. 58606	3	10, 41394	10, 03000	0	0. 05001	t
5	11 12	48 48	55030	3	44370	58644	4	41356	03014	0	95985	ŀ
7	11 4	48 56	55663	4	44337	52681	4	41319	03019	1	96981	1
	10 56	49 4	55695	4	44305	58719	5	41281	03024	1	95975	ı
9	10 45	49 12	55728	5	44272	58757		41243	03029	1	96971	1
10	9 10 40	49 20	9. 55761	3	1C. 44239 44207	9. 58794	6 7	41168	03034	1	9, 96966	1
2	10 24	49 35	55793 55826	6	44174	58869	7	41131	03043	1	96957	١
3	10 16	49 44	55858	7	44142	58907	7 8	41093	03048	1	96952	1
4	10 8	49 52	55891	7	44100	58944	9	41055	03053	1	06947	1
5	9 10 0	2 50 0	9.55923	8	10. 44077	9. 58981	9	10, 41010	10. 03058	1	9. 95942	t
16	9 52	50 8	55956	9	44044	59019	10	40381	03063	1	96937	ı
7 8	9 44	50 15	55988	9	44012	59055	10	40944	03068	1	96932	1
	9 30	50 24	50021	10	43979	59094	11	40005	03073	I	96927	ı
9		50 32	56053	1	43947	59131	12	40869	03078	2	96922	4
11	9 9 20	2 50 40 50 48	9, 56085	11	41882	59205	12	10, 40832	10, 03083	2	9. 96917	1
: 1		50 56	56150	12	43550	59243	14	40795 40757	03003	2	96907	1
13	8 56	51 4	56162	12	43818	59280	14	40720	03097	2	96903	ı
14	8 48	51 12	56215	13	43785	59317	15	40653	03102	2	96898	ı
5	9 8 40	2 51 20	9. 50247	13	10. 43753	9-59354	15	10, 40546	10, 03107	2	9. 96893	t
6	8 33	51 28	56279	14	43721	59391	10	40609	03112	2	96888	ı
7	8 24	51 36	56311	14	43689	59429	17	40571	03117	2	96883	ı
8	8 16	51 44	56343	15	43657	59465	17	40534	03125	2	96878	١
19	88	51 52	56375	16	43625	59503	18	40497	03127	2	96873	Ł
30		2 52 0 52 8	9,56408 56440	10	10, 43593 43560	9. 59540	19	10, 40400	10. 03132	2	9. 96868	ı
12	7 52 7 44	52 8 52 16	56472	17	43528	59577	19	40423	03137	3	90803	ł
33	7 36	52 24	56504	16	43496	50651	20	40349	03147	3	96853	ł
14	7 28	52 32	56536	18	43464	59688	21	40312	03152	3	96848	ı
55	9 7 20.	2 52 40	9.56568	19	10, 43433	9- 59725	22	10, 40275	10. 03157	3	9. 96843	î
	7 12	52 48	56599	19	43401	59762	22	40238	03102	3	96838	۱
7	7 4	52 56	56631	20	43369	59799	23	40201	03167	3	96833 96828	ı
3	6 56	53 4	56663 56695	20	43337	59835	23	40105	03172	3	96828	
9	9 6 40	33	9. 55727	21	43305	59872	25	10. 40001	-03177	3	9. 95818	ł
ĭ	6 33	2 53 20 53 28	55759	27	43241	9, 59909 59940	25	40054	10. 03102	3	9, 90018	ı
3	6 24	53 36	56790	22	43210	59983	26	40017	03193	3	96808	ı
3	6 16	53 44	56822	23	43178	60019	27	39981	03197	4	96803	ı
4	6 8	53 52	56854	24	43146	60056	27	39944	03202	4	96799	L
5	9 6 0	2 54 0	9. 56886	24	10, 43114	g. 600g3	28	10, 39907	10. 03207	4	9. 96793 96788	Ī
5	5 52	54 8	56917	25	43083	60130	28	39870	03212	4	96788	1
3	5 44	54 16 54 24	56949	25	43051	60106	29	39834	03217	4	96783	ı
9	5 28	54 24 54 32	57012	26	43030	60240	30	39797 39760	03222	4	96772	ı
0	9 5 20	2 54 40	9. 57044	27	10, 42050	9, 60276	31	10. 30724	10, 03233	4	9. 96767	ł
ī	5 12	54 48	57075	27	42925	60313	31	39687	03238	4	96762	1
2		54 56	57107	28	42893	60349	32	39651	03243	4	96757	1
3	4 56	55 4	57138	28	42862	60386	33	39614	01248	4	96752	1
4	4 48	55 12	57169	29	42831	60422	33	39578	03253	4	95747	1
5	9 4 40	2 55 20	9. 57201	29	10, 42799	9. 60459	34	10, 39541	10, 03258	5	9. 96742	ſ
0	4 32	55 28	57232	30	42768	60495	35	39505	03263	5	96737	1
8	4 24	55 36	57264 57295	30	42736	60532	35	39468	03268	5	96732	ı
0	4 8	55 44 55 52	57326	31	42074	60005	36	39433	03273	5	95727	1
9	4 0	56 0	57358	32	42642	60641	37	39359	03183	5	96717	1
		-				-				-		t
	Hour v. n.	Hour A. St.	Cosins.	DIE	Senant.	Cotanggot.	DIE.	Tangent.	Conscant	Diff.	Sine	

SINES	TANGENTS	AND SECANTS

220	•								-		1	1570
M.	Hour A. N.	Hour P. M.	Sine.	Diff.	Cosecant.	Tangent.	Diff.	Cotangent.	Secant.	Diff.	Cosine.	N.
•	9 4 0	2 56 O	9. 57358	٥	10, 42642	9, 60641	0	10. 39359	10. 03283	۰	9. 96717	60
:	3 52 3 44	56 8 56 16	57389 57420	1	42611 42580	60677 60714	1 1	39323 39286	03289	0	96711 96706	59 58
3	3 36	56 24	57451	2	42549	60750	2	39250	03299	ő	96701	57
4	3 28	56 32	57482	2	42518	60786	3	39214	03304	•	96696	56
5	9 3 20 3 12	2 56 40 56 48	9- 57514 57545	3	10. 42486 42455	9. 60823 60859	3	10. 39177 39141	10, 03309	0	9. 96691 96686	55
7 8	3 4	56 56	57576	4	42424	60895	1 7	39141	03314	1	96681	54 53
1	2 56 2 48	57 4	57607	4	42393	60931	5	39069	03324	1	96676	52
10	9 2 40	57 12 2 57 20	57638 9. 57669	5	42362 10. 42331	.g. 61004	뒿	39033 10. 38996	03330	1	96670 9. 96665	51
11	2 32	57 28	57700	5	42300	61040	7	38960	10. 03335 03340	1	9. 96665 96660	50 49
12	2 24 2 16	57 36	57731	6	42269	61076	7 8	38924	93345	1	96655	48
13 14	2 8	57 44 57 52	57762 57793	7	42238 42307	61112	ŝ	38888 38852	03350 0335 5	1	96650 96645	47 46
15	9 2 0	2 58 O	9. 57824	8	10. 42176	9. 61 184	. 9	10. 38816	10, 03360	Ť	9. 96640	45
16	1 52	58 8	57855	8	42145	61220	10	3878 0	03366	1	96634	44
17	1 44 1 36	58 16 58 24	57885 57916	9	42115	61256	10	38744 38708	03371	1 2	96629 96624	43 42
19	1 28	58 32	57947	ió	42053	61328	ii	38672	03381	2	96619	41
20	9 1 20	2 58 40	9. 57978	10	10, 42022	9. 61 364	12	10. 38636	10, 03386	2	9. 96614	40
21 22	I 12	58 48 58 56	58008 58039	11	41992 41961	61400 61436	13	38600 38564	03392 03397	2 2	96608 96603	39 38
23	0 56	59 4	58070	12	41930	61472	14	38528	03402	2	96598	37
24	0 48	59 12	58101	12	41899	61508	14	38492	03407	2	96593	36
25 26	9 0 40	2 59 20 59 28	9. 58131 58162	13	10, 41869 41838	9. 61544 61579	15	10. 38456 38421	10. 03412 03418	2 2	9. 96588 96582	35 34
27 28	0 24	59 36	58192	14	41808	61615	15 16	38385	03423	2	96577	33
28 29	o 16	59 44	58223 58253	14	41777	61651 61687	17	38349		2	96572	32
30		59 52 3 0 0	9. 58284	15	41747	9, 61 722	17	38313 10, 38278	03433 10. 03438	3	96567 9. 96562	31 30
31	9 0 0 8 59 52	l o 8	58314	16	41686	61758	18	38242	03444	3	96556	20
32	59 44	° o 16	58345	16	41655	61 794 61830	19	38206	03449	3 3	96551	28
33 34	59 36 59 28	0 24	58375 58406	17	41625 41594	61865	20	38170 38135	03454 03459	3	96546 96541	27 26
35	8 59 20	3 0 40	9. 58436	18	10, 41564	9.61901	21	10. 38000	10, 03465	3	9. 96535	25
36	59 12	0 48	58467 58497	18 19	41533	61936 61972	21	38064 38028	03470	3	96530 96525	24
37 38	59 4 58 56	0 56 I 4	58527	19	41503 41473	62008	23	37992	03475 03480	3	96520	23
39	58 48	1 12	58557	20	41443	62043	23	37957	03486	3	96514	21
40	8 58 40 58 32	3 I 20 I 28	9. 58588 58618	20	10, 41412	9. 62079	24	10. 37921 37886	10. 03491	3	9. 96509	20 19
41 42	58 24	1 28 1 36	58643	21	41382 41352	62150	24 25	37850	93496 93592	4	96504 96498	18
43	58 16	144	58678	22	41322	62185	26	37815	03507	4	96493 96488	17 16
44	58 8 8 58 0	1 52 3 2 0	58709 9. 58739	23	41291	9, 62256	26	37779 10. 37744	10, 03517	4	9, 96483	15
45 46	57 52	3 2 0	58769	23	41231	62292	27	37708	03523	4	96477	14
47 48	57 44	2 16	58799	24	41201	62327	28	37673	03528	4	962,72	13
48 49.	57 36 57 28	2 24	58829 58859	24 25	41171	62362 62398	29	37638 37602	03533 03539	4	96467 96461	111
50	8 57 20	3 2 40	9. 58889	25	10.41111	9. 62433	30	10. 37567	10. 03544	4	9. 96456	10
51	57 12	2 48	58919	26	41081	62468	30	37532	03549	4	96451	8
52 53	57 4 56 56	2 56 3 4	58949 58979	26 27	41051 41021	62504 62539	31 32	37496 37461	03555 03560	5	96445 96440	
54	56 48	3 12	59009	27	40991	62574	32	37426	03565	Š	96435	7 6
55 56	8 56 40	3 3 20	9. 59039	28	10, 40961	9. 62609	33	10. 37391	10, 03571	5	9. 96429 96424	5 4
50	56 32 56 24	3 28 3 36	59069 59098	28 20	40931 40902	62645 62680	33 34	37355 37320	03576 03581	5	96419	3
57 58	56 16	3 44	59128	29	40872	62715	35	37285	03587	5	96413	2 1
59 60	56 8 56 0	3 52 4 0	59158 59188	30 31	40842 40812	62750 62785	35 36	37250 37215	03592 03597	5	96408 96403	
M.		, ,		_			Diff.	Tangent.	Cosecant.	Diff.	Sine.	м.
	Hour r. M.	Hour A. M.	Cosine.	Diff.	Secant.	Cotangent.	Dia.	. Lugent.	Joseph .	D		
112	•											67°

M.	Hour a. is.	Hours. u.	Sine.	Diff.	Cosecant.	Tangerit.	Diff.	Cotangent.	Secart.	Diff.	Coalne.	M
0	8 56 o	3 4 0	9. 59188	0	10, 40812	9. 62785	0	10, 37215	10. 03597	0	9. 96403	6
ī	55 52	4 8	59218	0	40782	62820	1	37180	03603	0	96397	5
2	55 44	4 16	59247	1	40753	62855	1	37145	03608	0	96393	3
3	55 36	4 24	59277	1	40723	62890	2	37110	03613	0	96387	5
4	55 28	4 32	59307	2	40693	62926	. 2	37074	03619	- 0	96381	15
5	8 55 20	3 4 40	9. 59336	2	10, 40664	9, 62961	3	10. 37039	10, 03624	0	9. 90376	5
	55 12	4 48	59366	3	40634	62996	3	37004	03630	1	96170	1 5
7	55 4 54 56	4 56	59396		40504 40575	63031	4	36959 36934	03635	1	96365 96360	3
9	54 56 54 48	5 4 5 12	59425 59455	4	40545	63101	5	36899	03646	1	96354	5
0	\$ 54 40	3 5 20	9. 59484	5	10, 40516	9. 63135	5	10. 76865	10, 03651	1	9. 96349	13
1	54 32	5 28	59514		40486	63170	6	36830	03657	i	96343	k
2	54 24	5 36	59543	5	40457	63205	7	36795	03662	1	95338	К
3	54 16	5 44	59573	6	40427	63240		36760	03667	1	96333	L
4	54 8	5 52	59602	7	40398	63275	7 8	36725	03673	1	96327	R
5	8 54 0	3 6 0	9. 59632	7	10, 40368	9.63310	9	10. 36690	10, 03678	1	9. 95322	1
16	53 52	6 8	59661		40339	63345	9	36655	03684	1	96316	13
7	53 44	6 16	59690	8	40310	63379	10	36621	03689	2	96311	1
	53 36	6 24	59720	9	40280	63414	10	36586	03695	2 2	96305	ľ
9	53 28	6 32	59749	9.	40251	63449	11	36551	03700	_	95300	Ŀ
0	8 53 20	3 6 40 6 48	9- 59778	10	10, 40222	9. 63484	12	10. 36516	10. 03706	2 2	9. 95294	1
1 2	53 12	6 48	59808 59837	11	40102	63519	12	36481	03711	2	96284	13
3	53 4 52 56	7 4	59866	11	40134	63553 63588	13	36447	03722	2	96278	l
4	52 48	7 12	59895	12	40105	63623	14	36377	03727	2	96273	
15	8 52 40	3 7 20	9. 59924	12	10, 40076	9, 63657	14	10, 36343	10. 03733	2	0, 95257	t
6	52 32	7 28	59954	13	40046	63692	15	36308	03738	2	96262	Н
7	52 24	7 36	59983	13	40017	63726	16	36274	03744	2	96256	l
8	52 16	7 44	60013	14	39988	63761	16	36239	03749	3	95251	Ŀ
19	52 8	7 52	60041	14	39959	63796	17	36204	03755	3	95245	
O	8 51 0	3 8 0	9. 60070	15	10. 39930	9, 63830	17	10. 36170	10, 03760	3	9, 95240	1
3.	51 52	8 8	60099	15	39901	63865	18	36135	03766	3	96234	3
2	- 51 44	8 16 8 24	60128	15	39872 39843	63899	19	36101 36066	03771	3	96223	2
3	51 36 51 28	8 32	60186	16	39814	63934	20	36032	03777	3	96218	13
	8 51 20	3 8 40	9, 60215	17	10, 39785	9. 64003	20		10. 03788		9. 96212	
5	51 12	8 48	60244	17	39756	64037	21	35963	93793	3	96207	1
	51 4	8 56	60273	18	39727	64072	27	35928	03799	3	96201	3
7	50 56	9 4	60302	18	30608	64100	22	35504	03804	3	96196	Ŀ
19	50 48	9 12	60331	19	39669	64140	22	35860	03810	4	96190	1
0	8 50 40	3 9 20	9. 60359 60388	10	10. 39541	9. 64175	23	10. 35825	10, 03815	4	9. 96185	13
1	50 32	9 28	60388	20	39613	64209	24	35791	03821	4	96179	D
2	50 24	9 36	60417	20	39583	64243	24	35757	03826	4	96174	
3	50 16	9 44	60446	21	39554	6,4278	25	35722	03832	4	96168	1
4	50 8	9 52	60474	21	39526	54312	25	35688	03838	4	96162	1
2	8 50 0	3 10 0	9. 60503	22	10, 39497	9. 64346	26	10. 35654	10, 03843	4	9. 96157	P
6	49 52	10 8	60532 60561	22	39468	64381	26	35519 35585	03849	4	96131	1
7	49 44	10 24	60589	23	39439	64449	28	35551	n3860	4	95140	П
9	49 28	10 72	60618	24	70781	64483	25	35517	03865	3	96135	Б
D.	8 49 20	3 10 40	9, 60646	24	10. 39354	9. 64517	29	10, 15481	10, 01871	5	9. 95129	h
1	49 12	10 48	60675	25	39325	64552	20	35448	D3877	5	96121	Г
2	40 4	10 50	60704	25	39295	64586	30	35414	03882	5	96118	l
3	48 56	11 4	60752	26	39268	6,620	31	35380	03888	5	96112	1
4	48 48	11 12	60761	26	39239	6,4654	31	35346	03893	5	96107	L
5	8 48 40	3 11 20	9.60789	27	10. 39211	9. 64688	32	10. 35312	10.03899	5	9. 96101	1
0	48 32	11 28	60818	27	30185	64722	32	35278	03905	5	96095	1
7	48 24	11 36	60846	28	39154	6,1756	33	35244	03910		96090	ı
0	48 16	11 44	60875	28	39125	64790	3.3	35210	03916	5	96084	ı
9	48 8 48 0	11 52	60931	29	39097	64824	34	35176	03921	5	96073	1
		_	-	29			3.5	35143				L
	Hour r. H.	Hour A. M.	Cosine.	Diff.	Secunt,	Cotangent,	Diff.	Tangent.	Cosecant.	Diff.	Sine.	P

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M.	Hour A. M.	Hour P. M.	Sine.	Diff.	Cosecant,	Tangent.	Diff.	Cotangent.	Secant.	Diff.	Cosine.	×.
•	8 48 o	3 12 0	9. 60931	۰	10. 39069	9, 64858	۰	10. 35142	10. 03927	•	9. 96073	60
1 2	47 52	12 8 12 16	60960 60988	0	39040	648y2 64926	1	35108 35074	03933 03938	°	96067 96062	58 58
3	47 36	12 24	61016	1	39012 38984	64960		35040	03944	0	96056	57 56
4	47 28 8 47 20	12 32 3 12 40	61045	2 2	38955 10. 38927	64994 g. 65028	3	35006 10. 34972	03950	÷	96050 9. 96045	50 55
5	47 12	12 48	61 101	3	38899	65062	3	34938	03961	ľ	06020	54
7	47 4 46 56	12 56 13 4	61129	3	38871 38842	65096 65130	4	34904 34870	03966 03972	1	96034 96028	53 52
و	46 48	13 12	61 186	4	38814	65164	5	34836	03978	i	96022	51
10 11	8 46 40 46 32	3 13 20 13 28	9. 61214 61242	5	20. 38786 38758	9. 65197 65238	6	10, 34803 34769	10. 03983	1	9. 96017	50
22	46 24	13 36	61270	ş	28710	65265	7	34735	03995	1	96005	49 48
13	46 16 46 8	13 44 13 52	61298 61326	6	38702 38674	65299 65333	7	34701 34667	04000	1 1	96000 95994	47 46
14	8 46 0	3 14 0		7	10, 38646	9. 65366	8	10, 24624	10. 04012	i	0.00088	45
15 15	45 52	14 8	9. 61354 61382	7	38618 38589	65400	9	34600 34566	04018	2	95982 95977	44 43
17 18	45 44 45 36	14 16 14 24	61411	8	28562	65434 65467	9 10	34533	04029	3	95971	42
19	45 28	14 32	61466	9	38534	65501	11	34499	04035	2	95965	41
22	8 45 20 45 12	3 14 40 14 48	9. 61494 61522	10	10, 38506 38478	9- 65535 65568	11	10. 34465 34432	10. 04040 04046	2	9. 95960 95954	40 39
22	45 4	14 56	61550	10	38450	65602	12	34398	04052	2	95948	39 38
23 24	44 56 44 48	15 4 15 12	61578 61606	11	38422 38394	65636 65669	13	34364 34331	04058	2 2	95942 95937	37 36
25 25	8 44 40	3 15 20	9.61634	12	10, 38366	9.65703	14	10, 34297	10. 04069	2	9. 95931	35
25	44 32 44 24	15 28 15 36	61632	12	38338 38311	65736 65770	15	34264 34230	04075	3	95925 95920	34 33
27 28	44 16	15 44	61717	13	38283	65803	16	34197	04086	3	95914	32
29	44 8	15 52 3 16 0	61745	13	38255 10. 38227	65837 9. 65870	16	34163	10.04098	3	95908	31 30
30 31	8 44 0 43 52	3 16 O	9. 61773 61800	14	38200	65904	17	34096	04103	3	65807	20 25
32	43 44	16 16 16 24	61828 61856	15	38172 38144	65937 65971	18	34083 34029	04109	3	95891 95885	27
33 34	43 36 43 28	16 32	61883	15	38117	66004	19	33996	04121	3	05870	26
35 36	8 43 20	3 16 40 16 48	9. 61911	16	10. 38089 38061	9. 66038 66071	30 20	10. 33962	10, 04127 04132	3	9. 95873 95868	25 24
30 37	43 12 43 4	16 48 16 56	61939 61966	17 17 18	38024	66104	21	33929 33896	04138	4	95802	23
37 38	42 56	17 4	61994 62021	18	38006 37979	66138 66171	2I 22	33862 33829	04144 04150	4	95856 95850	22 21
39 40	42 48 8 42 40	3 17 20	0. 62040	18	10. 37951	9, 66204	22	10. 33796	10, 04156	4	0. 05844	20
41	42 33	17 28	62076	19	37924 37896	66238 66271	23	33762	04161 04167	. 4	95839 95833	19 18
43	42 24 42 16	17 36 17 44	62104 62131	20	37860	66304	23 24	33729 33696	04173	1 7	05827	17 16
44	42 8	17 52	62159	20	37841	66337	25	3,3663	04179	14	95821	
45 46	8 42 0 41 52	3 18 O	9. 62186 62314	2I 2I	10. 37814 37786	9. 66371 66404	25 26	10. 33629 33596	10, 04185	1 4	9. 95815 95810	15 14
47 48	41 44	18 16	62241	22	37759	66437	26	33563	04196	1 5	05804	13
48 49	41 36 41 28	18 24 18 32	62268 62296	22	37732 37794	66470 66503	27 27	33530 33497	04202	5	95798 95792	11
50	8 41 20	3 18 40	9. 62323	23	10, 37677	0.66537	28	10, 33463	10. 04214	5	0. 05786	10
51 52	41 12 41 4	18 48 18 56	62350 62377	24	37650 37623	66570 66603	28 29	3343° 33397	04220	5	95780 95775	2
52 53	40 56	19 4	62405	24	27505	66636	100	33364	04231	5	95769	7
54	40 48	19 12	62432	25	37568 IO. 37541	9, 66702	30 31	33331 10. 33298	10. 04243	5	95763 9-95757	5
55 56	8 40 40 40 38	19 28	9. 62459 62486	25 26	37514	66735	31	33265	04249	5	95751	4
57 58	40 24	19 36	62513	26	37487	66735 66768 66801	32 32	33232	04255 04261	§	95745 95739	3
58 59	40 I6	19 44 19 52	62541 62568	27 27	37459 37432	66834	33	33199 33166	04267	6	95733	1
őó	40 0	20 0	62595	28	37405	66867	33	33133	04272	6	95728	۰
M.	Hour P. M.	Hour a. M.	Costne.	Diff.	Secant.	Cotangent.	Diff.	Tangent,	Cossonst.	Diff.	Sine.	M.
1140											•	

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OTATES THE VICENTIA AND SECURE												
SINES, TANGENTS, AND SECANTS.												
25°				_			_					151°
M.	Hour A. M.	Hour P. M.	Sine.	Diff.	Cosecant.	Tangent.	Diff.	Cotangent.	Secant.	Diff.	Cosine.	M.
0	8 40 0 39 52	3 20 0 20 8	9. 62595	°	10. 37405 37378	9. 66867 66900	°	10. 33133 33100	10. 04272 04278	0	9. 95728 95722	60
2	39 44	20 16	62649 62676	1	37351	66933 66966	1	33067	04284	0	95716	59 58
3	39 36 39 28	20 24 20 32	62703	1 2	37324 37297	66999	2 2	33034 33001	04290 04296	0	95710 95704	57 56
ž	8 39 20	3 20 40	9. 62730	2	10. 37270	9. 67032	3	10. 32968	10. 04302	1	9. 95698	55
	39 12 30 4	20 48	62757 62784	3	37243 37216	67065 67098	3	32935 32902	04308 04314	1 1	95692 95686	54 53
8	39 4 38 56 38 48	21 4	62811 62838	4	37189	67131 67163	4	32869 32837	04320	1	95680 95674	52
9	8 38 40	3 21 20	9. 62865	4	37162 IO. 37135	9. 67196	5	10, 32804	10. 04332	i	9. 95668	51 50
111	38 32	21 28	62892 62918	5	37108 37082	67229 67262	8	32771	04337	1	95663 95657	49 48
12 13	38 24 38 16	21 36 21 44	62945	5	37052 37055	67295	7 7 8	32738 32705	04343 04349	i	95651	47 46
14	38.8	21 52	62972	6	37055 37028 10. 37001	67327 9. 67300	8	32673 10. 32640	04355 10. 04361	1 2	95645	
15 16	8 38 o 37 52	22 8	9. 62999 63026	7 7	36974	67393	9	32607	04367	2	9. 95639 95633	45 44
17 18	37 44 37 36	22 16 22 24	63052	8 8	36948 36921	67426 67458	9	32574 32542	04373 04379	2 2	95627 95621	43 42
19	37 28	22 32	63106	š	36894	67491	10	32509	04385	2	95615	41
20 21	8 37 20 37 12	3 22 40 22 48	9. 63133	9	10. 36867 36841	9. 67524	11	10. 32476 32444	10. 04391 04397	2 2	9. 95609 95603	40
22	37 4 36 56	22 56	63159 63186	10	36814	67556 67589	12	32411	04403	2	05597	39 38
23 24	36 56 36 48	23 4 23 12	63213 63239	10	36787 36761	67622 67654	12	32378 32346	04409	2 2	95591 95585	37 36
25	8 36 40	3 23 20	9. 63266	11	10. 36734 36708	9.67687	14	10. 32313	10, 04421	3	9-95579	35
26	36 32 36 24	23 28 23 36	63292	11	36708 36681	67719 67752	14	32281 32248	04427 04433	3	95573 95567	34 33
27 28	36 16	23 44	63.45	12	36655	67785	15	32215	04439	3	95561	32
29 30	36 8 8 36 0	23 52 3 24 0	63372 9. 63398	13	36628	67817 9. 67850	16	32183	04445 10, 04451	3	95555 9-95549	31 30
31	35 52	24 8	63425	14	36575	67882	17	32118	04457	3	95543	29 28
32 33	35 44 35 36	24 16 24 24	63451 63478	14 15	36549 36522	67915 67947	17	32085 32053	04463	3	95537 95531	
34	35 28	24 32	63504	15	36496	67947 67980	18	32020	04475	3	95525	27 26
35 36	8 35 20 35 12	3 24 40	9. 63531	15 16	10, 36469 36443	9. 680 £2 68044	19	10. 31988 31956	10. 04481 04487	4	9. 95519 95513	25 24
37 38	35 4	24 56	63557 63583	16	36417	68077 68109	20 21	31923 31891	04493	4	95507	23 22
39	34 56 34 48	25 4 25 12	63610 63636	17	36390 36364	68142	21	31858	04500 04506	4	95500 95494	21
40	8 34 40	3 25 20	9. 63662 63689	18	10. 36338	9, 68174 68206	22 22	10, 31826	10. 04512	4	9. 95488 95482	20 10
41 42	34 32 34 24	25 28 25 36	63715	19	36311 36285	68239	23	31794 31761	04518	1	95476	18
43	34 16 24 8	25 44 25 52	63741 63767	19	36259 36233	68271 68303	23 24	31729 31697	04530 04536	4	95470 95464	17 16
44	8 34 O	3 26 0	9. 63794 63820	20	10. 36206	9. 68336	24	10. 31664	10. 04542	5	9. 95458	15
45 46	33 52	26 8 26 16	63820 63846	20 21	36180 36154	68368 68400	25 25	31632 31600	04548	5	95452 95446	14 13
47 48	33 44 33 30	26 24	63872	21	36128	68432	26	31568	04554 04560	5	95440	12
49	33 28	26 32 3 26 40	63898 9. 63924	22	36102	68465 9. 68497	27	31535 10. 31503	04566	5	95434	11
50 51	33 12	26 48	63950	23	36050	68529	28	31471	04579	5	95421	8
52 53	33 4 32 56	26 56 27 4	63976	23 23	36024 35998	68561 68593	28	31439 31407	04585 04591	5	95415 95409	
54	32 48	27 12	64028	24	35972	68626	29	31374	04597	5	95403	6
55 56	8 32 40 32 32	3 27 20 27 28	9. 64054 64080	24 25	10. 35946 35920	9. 68653 68630	30 30	31342	10, 04603	6	9- 95397 95391	5
57 58	32 24	27 36	64106	25 26	25804	68722	31	31278	04616	6	95384	3 2
58 59	32 16 32 8	27 44 27 52	64132 64158	26 26	35868 35842	68754 63786	31 32	31246 31214	04622 04628	6	95378 95372	1
12.	30 0	-6 -6	68.	1 46	25816	68818	32	21182	04624	6	05166	ا ہ

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280			<u> </u>	-								158°
M.	Hour A. M.	Hour P. M.	Sine.	Diff.	Cossont.	Tangent.	Diff.	Cotangent.	Secant.	Diff.	Costne.	M.
٥	8 32 0	3 28 0	9. 64184	0	10, 35816	9, 68818	٥	10. 31182	10, 04634	0	9. 95366	60
I 2	31 52 31 44	28 8 28 16	64210 64236	0	35790	68850 68882	1	31150 31118	04640 04646	°	95360	58 58
3	31 44 31 36	28 24	64262	i	35764 35738	68914	2	31086	04652	اة	95354 95348	57
4	31 28	28 32	64288	2	35712	68946	2	31054	04659	0	95341	56
ş	8 31 20	3 28 40	9. 64313	2	10. 35687	9. 68978	3	10. 31022	10. 04665	1	9-95335	55
	31 12	28 48 28 56	64339 64365	3	35661 35635	69010 69042	3	30990 30958	04671 04677		95329	54
7	30 56	29 4	64391	3	35600	69074	1	20026	04683	l i	95323 95317	53 52
9	30 48	29 12	64417	4	35583	69106	5	30894	04690	1	95310	Šι
10	8 30 40	3 29 20 20 28	9. 64442 64468	4	10. 35558	9. 69138	ş	10, 30862 30830	10. 04696	1	9. 95304	50
12	30 32 30 24	29 28 29 36	64494	5	35532 35506	69170	6	30798	04702	Hi	95298 95292	49 48
13	30 16	29 44	64519	5	35481	69234 69266	7	30766	04714	1	95286	47
14	30 8	29 52	64545		35455		7	30734	04721	1	95279	47
15 16	8 30 0 29 52	3 30 0 30 8	9. 64571 64596	6 7	IO. 35429	9. 69298 69329	8	10. 30702 30671	10. 04727 04733	2 2	9. 95273 95267	45
17	29 44	30 16	64622	7 8	354°4 35378	69361	وا	30639	94739	2	95261	44
18	29 36	30 24	64647		35353	69393	9	30607	04746	2	95254	42
19	29 28 8 29 20	30 32	64673 a, 64698	8	35327	69425	10	30575	04752	1-2	95248	41
20 21	8 29 20 20 12	3 30 40 30 48	64724	اۋا	10, 35302 35276	9. 69457 69488	111	10. 30543 30512	10.04758	1 2	9. 95242 95236	40
22	29 4	30 56	64749	ا ۋا	35251	69520	12	30480	04771	2	95229	39 38
23	28 56 28 45	31 4	64775 64800	10	35225	69552	12	30448	94777] 2	95223	37
24	28 45 8 28 40	31 12 3 31 20	9, 64826	10	35200	69584 9.69615	13	30416	04783 IO, 04789	1 3	95217	36
25 26	28 32	3 31 20	64851	ii	35149	69647	14	30353	04796	3 3	95204	35 34
27 28	28 24	31 36	64877	111	35123	69679	14	30321	04796 04802	3	95198	33
28	28 16 28 8	31 44 31 52	64902 64927	12	35098 35073	69710 69742	15	30290 30258	04808 04815	3	95192 95185	32 31
30	8 28 O	3 32 0		13	10. 35047	0. 60774	15	10. 30226	10.04821	3	9. 95179	30
31	27 52	32 8	9. 64953 64978	13	35022	9. 69774 69805	16	30195	04027	Ιš	95173	3
32	27 44 27 36	32 16 32 24	65003 65029	14	34997	69837 69868	17	30163	04833 04840	3	95167 95160	28
33 34	27 28	32 32	65054	14	34971 34946	69900	17	30133	04846	3	95154	27 26
35 36	8 27 20	3 32 40	9. 65079	15	10. 34921	9. 69932	18	10. 30068	10, 04852	4	9. 95148	25
36	27 12	32 48	65104	15	34896	69963	19	30037	04859	4	95141	24
37 38	27 4 26 56	32 56 33 4	65130	16	34870 34845	69995 70026	20	30005 29974	04865 04871	4	95135 95129	23
32	26 48	33 12	65155 65180	16	34820	70058	21	29942	04878	4	95122	21
40	8 26 40	3 33 20	9. 65205	17	10. 34795	9. 70089	21	10, 29911	10.04884	4	9. 951 16	20
41 42	26 32 26 24	33 28 33 36	65230 65255	17	34770 34745	70121 70152	22	29879 29848	04890 04897	1	95110 95103	19 18
43	26 16	33 44	65281	18	34719	70184	23	29816	04903	3	95097	17 16
44	26 8	33 52	65306	19	34694	70215	23	29785	04910	3	95090	
45 46	8 26 0 25 52	3 34 0 34 8	9. 65331 65356	19	10, 34669 34644	9. 70247 70278	24	29753	10, 04916 04922	5	9. 95084 95078	15
47		34 16	65381	20	34619	70309	25	29691	04922	5	95071	14 13
48	25 36	34 24	65406	20	34594	70341	25 26	29659	04935	5	95065	12
49	25 28 8 25 20	34 32	65431	21	34569	70372	26	29628	04941	1-5-	95059	"
50	25 12	3 34 40 34 48	9. 65456 65481	21	10. 34544 34519	9. 70404 70435	27	10, 29596 29565	10. 04948 04934	5	9. 95052 95046	10
52	25 4	34 56	65506	22	34494	70466	27	29534	04961	ş	95039	8
53 54	24 56 24 48	35 4 35 12	65531 65556	23	34469	70498 70529	28 28	29502 29471	04967 04973	6	95033 95027	7
	8 24 40	3 35 20	9. 65580	23	34444 10, 34420	9. 70560	20	10, 29440	10, 01080	8	9,0020	5
55 56	24 32	35 28	65605	24	34395	70592	30	29408	04986	6	95014	4
57 58	24 24 24 16	35 36	65630 65655	24	34370	70023	30	29377	04993	6	95007 95001	3 2
36	24 8	35 44 35 52	65680	25 25	34345 34320	70654 70685	31	29346 29315	04999 05005	6	04005	1
8	24 0	36 o	65705	25	34295	70717	32	29283	05012	6	94988	0
M.	Hour P. M.	Hour A. M.	Cosine.	Dig.	Secant.	Cotangent.	Diff.	Tangent.	Cosecant,	DIE.	Sine.	M.
116	-	<u> </u>								'		620
												-

M.	Hour A. M.	Hour P. M.	Sine.	Diff.	Cosecunt.	Tangent.	Diff	Cetanimen	Secant.	Dig	Costne.	12
-	-	_					-	Cotangent.	-	-		1
0	8 14 0	3 36 0	9, 65705	0	10, 34295	9. 70717	0	10, 29253	10.05012	0	9. 94958	١
1	23 52	36 8	65729	0	34271	70748	1	22252	05018	0	94982	1
2	23 44	36 16	65754	13	34246	70779	1	29221	05025	0	94975	1
3	23 36	36 24 36 32	65779 65804	1 2	34221	70810	2	29190	05031	0	94969	t
4	The same of the same of			-	34196		2	29159	05038	0	94962	1
50	8 23 20	3 30 40	9. 65828	2	10. 34172	9, 70873	3	10, 29127	10, 05044	1	9. 94956	ı
	23.12	36 48 36 56	65853 65878	2	34147	70904	3	29096	05051	I	94949	1
8	23 4			3	. 34122	70935 70950	4	29065	05057	I	94943	ı
9	22 48	37 4 37 12	65902 65927	3	34098		4	29034	05004	I	94936	ı
10		23		4	34073	70997	5	29003			94930	4
		3 37 28	9. 65952 65976	4	10. 34048	9. 71028	5	28941	10.05077	I	9-94923	1
2	22 32	37 36	66001	4	34024 33999	71059	6	28910	p5083	1	94917	١
3	22 16	37 44	66025	5	33975	71121	7	28879	-05096	i	94911	١
4	22 8	37 52	66050	5	33950	71 153		28847	05102	2	94898	1
5	8 22 0	3 38 0	9. 66075	6	10. 33925	9. 71 184	7 8	10. 28816	10.05109	2	9-94891	ł
6	21 52	38 8	66099	6	33901	71215	8	28785	05115	2	94885	ı
7	21 44	38 16	66124	7	33876	71246	9	28754	05122	2	94878	١
8	21 30	38 24	66148		33852	71277	9	28723	05129	2	94571	1
0	21 28	38 32	66173	7	33827	71308	10	28692	05135	2	94865	ı
o l	8 21 20	3 38 40	0, 66197	8	10. 33803	9. 71339	10	10, 28661	10, 05142	2	9. 94858	ŧ
1	21 12	38 48	66221	8	33779	71370	11	28630	05148	2	94852	ı
2	21 4	38 56	66246	9	33754	71401	II	28599	05155	2	94845	ı
3	20 56	39 4	66270	9	33730	71431	12	28569	05101	3	94839	ı
4	20 48	39 12	66295	10	33705	71462	12	28538	05168	3	04812	ł
5	8 20 40	3 39 20	9, 66319	10	10. 33681	9. 71493	13	10. 28507	10, 05174	3	9. 94826	t
6	20 32	39 28		11	33657	71524	13	28476	05181	3	94819	ı
7	20 24	39 36	66343 66368	II	33632	71555	14	28445	05187	3	94813	ı
8	20 16	39 44	66392	11	33608	71586	14	28414	05194	3	94806	ı
9	20 8	39 52	66416	12	33584	71617	15	28383	05201	3	94799	ı
0	8 20 0	3 40 0	9. 66441	12	10, 33559	9. 71648	15	10, 28352	10, 05207	3	9-94793	T
1	19 52	40 8	66465	13	33535	71679	16	28321	05214	3	94786	ı
2	19 44	40 16	66489	13	33511	71709	16	28291	05220	4	54780	ı
3	19 36	40 24	66513	13	33487	71740	17	28260	05227	4	94773	ı
4	19 28	40 32	66537	14	33463	71771	17	28229	05233	- 4	94767	L
5	8 19 10	3 40 40	9.66562	14	10. 33438	9. 71802	18	10, 28198	10, 05240	4	9. 94760	I
٥١	19 12	40 48	66586	15	33414	71833	19	28167	00247	4	94753	ı
7	18 56	40 56	66610	1.5	33390	71863	19	28137	05253	4	94747	ı
8	18 56	41 4	66634	15	33366	71894	20	28106	05200	4	94740	ı
9	18 48	41 12	66658	16	33342	71925	20	28075	05266	4	94734	Į.
0	8 18 40	3 41 20	9.66682	16	10. 33318	9. 71955	21	10, 28045	10. 05273	4	9-94727	ľ
!	15 32	41 28	66706	17	33294	71986	21	28014	05280	4	94720	ı
2	18 10	41 36	66731	17	33269	72017		27983	05286	5	94714	ŀ
3	18 8	47 44	66755	17	33245	72048	22	27952	05293	5	94707	ı
4	8 18 0		66779	18	33221				05300	5	94700	ŀ
	0 10	3 42 0	9. 66863 66827		10. 33197	9. 72100	23	27860	10.05306	5	9. 94694	I
	17 52	42 16	66851	19	33173	72140	24	27830	05313 05320	5	94687 94680	ŀ
3	17 30	42 24	66875	19	33149	72201	25	27799	05326	5	94674	ŀ
9	17 28	42 32	66899	20	33125	72231	25	27769	05333	5	94074	ŀ
2	8 17 20	3 42 40	9. 66922	20	10, 33078	9. 72262	26	10. 27738	10. 05340	5	9. 94660	H
i	17 12	43 48	66946	31	33054	72293	26	27707	05346	6	94654	ı
	17 4	42 56	66970	21	33030	72323	27	27077	95353	6	94647	ı
3	16 56	43 4	66994	91	33006	72354		27646	05360	6	94640	ı
í I	16 48	43 12	67018	22	32982	72384	27	27616	05366	6	94634	ı
H	8 16 40	3 43 20	9. 67042	22	10. 32955	9. 72415	28	10, 27585	10.05373	6	9. 94627	H
6	16 32	43 28	67066	23	32934	72445	29	27555	05350	6	94620	ı
7	16 24	43 36	67090	23	32010	72470	29	27924	05386	6	04014	ı
É	16 16	43 44	67113	23	33887	72506	30	27494	05393	6	94007	ı
9.1	16 8	43 52	67137	24	32863	72537	30	27463	05400	6	94600	ı
ó	16 0	44 0	67161	24	32839	72507	31	27433	05407	7	94593	
	Hour s. M.	Hour A. M.	Coules	Diff.			-		-	-		H
			Cosine.	47181.4	Secant	Cotangent .	Diff	Tangent.	Cosecunt.	Diff.	Sine.	1

280				1	2	-	Tarini.	-		lair.		151
Μ.,	Hour A. M.	Hour r. m.	Sine.	Diff.	Cosecant.	Tangent.	Diff.	Cotangent.	Secunt.	Diff.	Cosine.	M
o	8 16 10	3 44 0	9. 67161	0	10, 32839	9. 72567	0	10, 27433	10, 05407	0	9-94593	6
1	15 52	44 8	67185	0	32815	72598	T	27402	05413	0	94587	5
2	15 44	44 16	67208	7 1	32792	72628	1 2	27372	05420	0	94580	13
3	15 36	44 24	67232 67256	2	32768	72659 72689	2	27341 27311	05433	0	94573	5
4	-	44 32	9, 67280	2	32744	9. 72720	_	10. 27280	10, 05440	1	9. 94560	1
5	8 15 20	3 44 49 44 48	67303	2	32597	72750	3	27250	05447	î	94553	R
	15 4	44 48 44 56	67327	3	32673	72780	4	27220	05454	i	94546	ŀ
78	14 56	45 4	67350	3	32050	72811	4	27189	05400	1	94540	В
ò	14 48	45 12	67374	3	32626	72841	5	27159	05467	1	94533	Ŀ
0	8 14 40	3 45 20	9, 67398	4	10, 32602	9. 72572		10. 27128	10. 05474	1	9. 94526	ī.
T	14 32	45 28	67421	4	32579	72902	5	27098	05481	1	94519	Б
2	T4 24	45 36	67445	5	32555	72932	6	27068	05487	1	94513	Ŀ
3	14 16	45 44	67468	5	32532	72963	7	27037	05494	I	94506	и
4	14 8	45 52	67492	5	32508	72993	7	27007	05501	2	94499	Ŀ
5	B 14 0	3 46 0	9. 67515	.6	10. 32485	9. 73023	8	10. 26977	10, 05508	2	9. 94492	ŀ
6	13 52	46 8	67539	6	32461	73054	8	26946	05515	2	94485	P
78	13 44	46 16	67562	7	32438	73084	9	26916	05521	2	94479	Ľ
	13 36	46 24	67586	7	32414	73114	9	26886 26856	05528		94472	ľ
9	13 28	46 32	67609	7	32391	73144			05535	_		ŀ
0	8 13 20	3 46 40	9, 67633	8	10. 32367	9-73175	10	10. 26825	10, 05542	2	9. 94458	L
I	13 12	46 48	67656 67680	8	32344	73205	11	26795 26765	05549 05555	2	94451	ı
3	13 4	46 56		9	32320	73235 73265	12	26735	05502	3	94438	
3	12 48	47 4 47 12	67703	9	32274	73295	12	25705	05569	3	94431	l
	8 12 40	47.00	0. 67750	10	10. 32250	9. 73325	13	10. 26674	10. 05576	3	9. 94474	t
5	12 32	3 47 20 47 28	67773	to	32227	73356	13	26644	05583	3	94417	t
	12 24	47 36	67706	10	32204	73386	14	26614	05590	3	94410	Ł
3	12 16	47 44	67796 67520	11	32180	73416	14	26584	05596	3	94494	E
9	12 -8	47 52	67843	11	32157	73446	.15	26554	05003	3	94397	L
o.	8 12 0	3 48 0	0.67866	12	40, 32134	9-73476	15	10, 25524	10.05510	3	9. 94390	L
1	11 52	48 8	67890	12	32110	73507	10	26493	05617	4	94383	ı.
3	11 44	48 16	67913	1.2	32087	73537	16	25463	05624	4	94376	В
3	11 36	48 24	67936	13	32064	73507	17	25433	05631	4	94360	Ľ
4	11 28	48 32	67959	13	32041	73597	17	26403	05638	4	94362	L
5 1	8 11 20	3. 48 40	9. 67982	14	10, 32018	9. 73627	18	10. 26373	10, 05645	4	9-94355	ŀ
6	11 12	48 48	68006	1.4	31994	73657	18	26343	05651	4	94349	L
7	11 4	48 56	68029	14	31971	73687	19	26313	05658	4	94342	ı
8	10 56	49 4	68075	15	31945	73717	19	26283 26253	05665	4	94335 94328	н
9	10 48	49 12		15	31925	73747				4		t
0	8 10 40	3 49 20	9.68098	10	10. 31902	9-73777	20	26193	10. 05679 05686	5	9. 94321	ľ
1	10 32 10 24	49 28	68144	16	31879 31856	73807 73837	21	26163	05000	5	94314	t
3	10 24	49 36	68167	17	31833	73807	22	20103	05700	5	94300	L
il	10 8	49 44	68100	17	31810	73897	22	26103	05707	5	94293	L
5	8 10 n	3.50 0	9. 68213	17	10. 31787	9-73027	23	10, 26073	10.05714	5	9. 94286	t
3	9 52	50 8	68237	18	31763	73957	23	26043	05731	5	94279	1
7	9 44	50 75	68260	18	31740	73987	24	26013	05727	5	94273	U
8	9 36	50 24	68283	19	31717	74017	24	25983	05734	5,6	94266	н
9.	9 28	50 32	68305	19	31605	74047	25	25953	05741		94259	L
5	8 9 20	3 50 40	9.68328	19	10.31672	9-74077	25	10. 25923	10, 05748	6	9. 94252	Т
1	9 12	50 48	68351	20	31049	74107	26	25893	05755	6	94245	1
2	9.4	50 36	68174	20	31626	74137 74166	26	25863	05762	6	94238	1
3	8 56	51 4	68197	21	31603		27	25834	05769	6	94231	1
4	8 48	51 12	58420	21	31580	74196	27	25504	05776		94224	1
5	8 8 40	3 51 20	9. 68443	21	10, 31557	9. 74230	28	10. 25774	10.05783	6	9.94217	ı
6	8 32	51 28	68466	22	31534	74256	28	25744	05790	6	94210	1
3	8 24	51 36	68489	22	31311	74286	29	25714 25684	05797	7 7	94190	ı
2	8 16	51 44	68534		31456	74316	29	25655	05811	7	94180	1
9	8 0	51 52	68557	23	31443	74345 74375	30	25625	05818	7	94182	1
r.			_	- "		-	-		_	-	-	ŀ
	Hour e. st.	Houra. M.	Cosine.	Diff.	Secant.	Cotangent.	Diff.	Tangent.	Cosecant.	Diff.	Sine.	400

		**	200	Section 1			Sec. le	Service Street	AC 104	waster.	and the second	١.
M.	Hour A. M.	Hour P. N.	Sine.	Diff.	Cosecant,	Tangent,	Diff.	Cotangent,	Secant,	Diff.	Cosine.	M
0	8 8 0	3 52 0	9. 68557	0	10. 31443	9-74375	0	10. 25625	10. 05818	0	9. 94182	6
1	7 52	52 8	68580	0	31420	74405	0	25595	05805	0	94175	5
2	7.44	52 16	68603	1.0	31397	74435	1	25565	05832	0	94168	l:
3	7 36	52 24	68625	1	31 375	74405	1	25535	05839	0	94161	L
4	7 28	52 32	68648	1	31352	74494	2	25500	05846	0	94154	L
5	8 7 20	3 52 40	9. 68671	2	10, 31329	9-74524	2	10, 25476	10. 05853	1	9-94147	L
	7 12	52 48	68694	2	31300	74554	3	25445	05860	1	94140	L
7	7 4	52 56	68716	3	31284	74583	3	25417	05867	1	94133	L
	0 50	53 4	68739	3	31261	74613	4	25387	05874	1	94120	L
9	6 48	53 12	68762	3	31238	74643	4	25357	05861	1	94119	L
0	6 40	3 53 20	9. 68784	4	10, 31216	9. 74673	5	10. 25327	10. 05888	1	9. 94112	ı
1		53 28	58807 68829	4	31193	74702	5	25298-	05895	1	94105	l
2	6 24	53 36	68852	1	31171	74732	6	25265	05902	2	94098	ľ
3	6 8	53 44	68875	5	31148	74762	7	25238	05910	2	94095	ľ
4		53 52		5		74791		25209	05917			
5	8 6 0	3 54 0 54 8	9. 68897	6	10, 311.3	9. 74821	7	10, 25179	10, 05924	2	9, 94070	Ŀ
6	5'52	34	68920 68942	6	31050	74851 74880	8	25149	05931	2	94069	ľ
7 8	5 44	54 16 54 24	68965	7	31058	74910	9	25090	05938	2	94055	ľ
9	5 36	54 32	68987	7	31013	74939	9	25001	05952	-3	94048	ı
9	-		9, 69010		10, 30000	9. 74969	10	10, 25031	10, 05959	2	9. 94941	H
îl		3 54 40 54 48	69032	7	30968	74998	10	25002	05966	3	94034	
١			69055	8	30945	75028	11	24972	05973	3	94034	١
3	5 4 4 56	54 56 55 4	69077	0	30943	75058	II	24942	05950	3	94020	ı
41	4 48	55 12	69100	9	30923	75087	12	24913	05988	3	94012	ı
5	8 4 40	-	9. 69122	9	10. 30878	9. 75117	12	10. 24881	10, 05995	3	9. 94005	t
8	4 32	3 55 20 55 28	69144	10	30850	75146	13	24854	00002	3	93998	L
7	4 24	55 36	50167	10	30833	75176	13	24824	06000	3	03991	L
ś I	4 16	55 44	69189	10	30811	75205	14	24705	οδοιδ	3	93954	П
0	4 8	55 52	69212	11	30788	75235	14	24765	06023	3	93977	L
0	8 4 0	3 56 0	9, 69214	11	10. 30766	9. 75264	15	10, 24736	10, 06030	4	9. 93970	t
ĭ	3 52	56 8	69256	12	39744	75294	15	24706	06037	4	93953	п
a l	3 44	56 16	69279	12	30721	75323	16	24077	05045	4	93955	ı
3	3 36	56 24	69301	12	30699	75353	16	24647	06052	.4	93941	ь
4	3 28	56 32	69323	13	30577	75382	17	24618	06059	4	93941	L
5	8 3 20	3 56 40	9. 69345	13	10. 30655	9. 75411	17	10, 24589	10, 06066	4	9-93934	Г
6	3 11	56 48	69368	13	30632	75441	18	24559	06073	4	93927	ь
7	3 4	56 56	69390	14	30010	75470	18	24530	06080	4	93920	ь
8	2 56	57 4	69412	14	30588	75500	19	24500	06088	5	93912	н
9	2 48	57 12	69434	15	30566	75529	19	24471	06095	5	93905	L
0	8 2 40	3 57 20	9. 69456	15	10. 30544	9.75558	20	10. 24443	10, 06102	5	9. 93898	Г
1	2 32	57 28	69479	15	30521	75588	20	24412	06109	5	93891	I
2	2 24	57 36	69501	16	30499	75617	21	24383	05116	5	93884	
3	2 16	57.44	69523	16	30477	75647	21	24353	06124	5	93876	l
4	2 8	57 52	69545	16	30455	75676	22	24324	00131	5	93869	
5	8 2 0	3 58 0	9. 69567	17	10. 30433	9- 75705	22	10. 24295	10,06138	5	9. 93862	ı
6	1 52	58 8	69589	17	30411	75735	23	24265	06145	5	93855	ı
7	1 44	58 16	69611	17	30389	75794	23	24235	06153		93847	ı
8	1 36	58 24	69633		30367	75793	24	24207	66160	6	93840	ŀ
9	1 28	58 32	69655	18	30345	75822	24	24178	06167		93833	
0	8 1 20	3 58 40	9. 69677	19	10. 30323	9. 75852	25	10, 24148	10,06174	6	9. 93826	ı
1	1 13	58 48	69699	19	30301	75881	25	24119	18190	6	93819	1
2	0 56	58 56	69711	19	30279	75910	26	24000	06100	6	93811	l.
3	0 56	59 4	69743	20	30257	75939		24061	00190	6	93797	1
4	0 40	59 11	69765	20	30235	75969	27	24031		1		t
5	8 0 49	3 59 20	9. 69787	20	10. 30213	9-75995	27	10. 14002	10, 00211	7	9. 93789	1
6	0 32	59 28	69809	21	20101	76027	28	23973	06218	7	93782	1
7	0 24	59 36	69531	21	30109	76056	28	23944	00225	7	93775 93768	1
0		59 44	69853	21	30147		29	23914	00232	7	93760	1
9	0 8	4 0 0	69875 69897	22	30125	75115	29	23805	06245	1 5	93753	1
~	0 0	4 0 0	09097	22	30103	75144	-	23050	50247	-		1
0.1	Hour v. M.	Hour A. M.	Cosine.	Diff	Secant.	Cotangent.	Diff.	Tangent,	Conscent.	Diff.	Sing.	п

м.	Hour A. M.	Hour s. M.	Sine	Diff.	Cosecant.	Tangent.	DUT.	Cotangent.	Train.	Diff.		14
_	_	_		-	-	-	-	-		Diff.	Cotine.	1
0	8 0 0	4 0 0	9. 69897	0	,10, 30103	9. 76144	0	10, 23855	10. 05047	0	9-93753	1
1 2	7 59 52 59 44	0 16	69919	1	30059	75173 75202	0	23827 23798	05254 05252	0	93746	1
3	59 30	0 24	69963	î	30037	75211	I	23709	00203	0	93738	в
4	59 28	0 32	60984	Î	30016	76261	2	23739	05275	0	95731	l
	7 59 20	4 0 40	9. 70006	2	10. 20004	9. 75290	2	10, 23710	10, 06283	1		
5	50 12	0 48	70028	2	29972	76319	3	23681	05291	1	9-93717	
7		0 56	70050	3	29950	76348	3	23652	06298	1	93703	L
8	58 56	1 4	70072	3	29928	76377	4	23623	06305	1	03505	ľ
9	53 48	1 12	70093	3	29907	76406	4	23594	06313	2 .	93687	B
a.	7 53 40	4 1 20	9. 70115	. 4	10. 29885	9- 70435	5	10, 23565	10, 05320	1	9. 93680	F
1	58 32	1 28	70137	4	29863	76464	5	23535	06327	1	93573	ı
2	58 24	1 36	70159	4	29841	75493		23507	06335	1	93005	в
3	58 16 53 8	I. 44	70180	5	29520	76522	6	23478	06342	2	93653	ŀ
-		1 52	70202	.5	29798	76551	7	23449	05350	2	93650	U
5	7 50 0	4 2 0	9. 70224	5	10. 29770	9. 76580	7 8	10, 23420	10.00357	2	9. 93543	ı
7	57 52	2 16	70245	6	29755	76609 76639	8	23391	06364	2	93533	P
έl	57 36	2 24	70288	6	29733 29712	76668	9	23301	06372	2 2	93523	н
0.	57 28	2 32	70310	7	29600	76697	9	23332	06379 06386	2	93621	ı
0	7 57 20	4 2 40	9. 70332		10, 29668	9. 76725	10	10, 23275	10, 06394	2		4-
1	57 12	2 48	79353	7 8	29647	76754	10	23240	06401	3	93500	ı
2	57 4	2 56	70375	8	29625	76783	11	23217	05400	3	93391	ı
3	55 55	3 4	70390	8	29504	76812	11	23158	06416	3	93584	в
4	56 48	3 12	70018	9	29582	76841	12	23159	06423	3	93577	
5	7 50 40	4 3 20	9. 70439	9	10, 29551	9. 76870	12	10, 23130	10, 00431	3	0. 01560	î
6	55 31	3 28	70401	9	29539	76899	13	23101	00438		93562	В
7	55 24	3 36	70482	10	29518	76928	13	23072	65445	3	93554	ı
	56 16 56 B	3 44	70504	10	29496	76957	13	23043	. 05453	3	93547	ы
9.		3 57	70525	10	29475	76986	14	23014	06461	- 6	93532	L
5	7 55 0	4 4 0	9. 70547	11	10, 29453	9. 77015	14	10. 22085	10, 05468	4	9-93532	Ŀ
1	55 52	4	70568 70590	11,	29432	77044	15	22956	05475	4	935=5	l
3	55 44 55 30	4 16	70590	12	29389	77073 77101	15	22927 22899	06483	4	93517	В
4	55 28	4 32	70633	12	29367	77130	16	22870	06490	4	93510	B
5	7 55 20	4 4 40	9. 70654	13	10, 29346	9- 77159	17	10, 22841	10. 06505	$\overline{}$	93500	
6	55 12	4 48	70675	13	29325	77188		22512	06543	4	9-93495	
7	55 4	4 56	70697	13	29303	77217	17	22783	06520	4 5	93480	ı
8	54 56	5 4	70718	14	29282	77246	18	22754	06528	5	93472	l
9	54 48	5 12	70739	14	29261	77274	19	22726	06535	5	93465	Ŀ
O	7 54 40	4 5 20	9. 70761	14	10. 29239	9. 77303	19	10. 22697	10. 06543	5	9-93457	Г
1	54 32	5 28	70782	15	29218	77332	20	22668	06550	5	93450	П
2	54 24	5 36	70803	15	29197	77361	20	22639	06558	5	93442	в
3	54 16	5 44	70824	15	29176	77390	21	22510-	06565	5	93435	ı
4	54 8	5 52	70846	16	29154	77418	21	22582	06573	5	93427	
5	7 54 0	4 6 8	9. 70867	16	10. 20133	9- 77447	22	10. 22553	10, 06580	6	9.93420	Г
5	53 52 53 44	6 46	70883	16	20112	77479	22	22524	06588	6	93412	В
78	53.44 53.30	6 24	70931		29051 29069	77505	23	22495	06595	6	93405	В
9	53 28	6 32	70952	17	20048	77533 77502	24	22438	06610	6	93397	li
9	7 53 20	4 6 40	9. 70973	18	10, 20027	9- 77591	24	10, 22400	10, 06618	6	9,933-2	
1	53 12	6 48	70994	18	20006	77619	25	22351	06625	6		P
2	53 4	6 56	71015	19	23985	77643	25	22352	06633	6	93375 93367	П
3	52 56	7 4	71036	19	28964	77677	26	22323	06640	7	93360	1
4	52 48	7 12	71058	19	28942	77700	26	22294	06648	7	93352	ı
5	7 52 40	4 7 20	9. 71079	20	10. 28921	9-77734	26	10. 22266	10.06656	7	9-93344	г
6	52 32	7 28	71100	20	28900	77763	27	22237	06663	7	93337	п
7	52 29	7 36	71121	20	23370	22202	27 28	22209	06671	7	93329	п
8	52 16	7.44	71142	21	288c8	77520	28	22180	06678	7	93372	
9		7 52	71163	21	28837	77849	28	22151	06686	7	93314	
-	52 0	-	71184	21	38816	77877	29	22123	06693	7	93307	
-	Hour P. M.	Hour A. M.	Cosine.	Diff.	Secanti	Cotangent.	Diff.	Tangent.	Cosecant.	Diff.	Sing.	3

M.	Houra. M.	Hour P. M.	Sine,	Diff.	Cosecant.	Tangent.	Diff.	Cotangent.	Secant.	DIA.	Cosine.	3
0	7 52 0	4 8 0	9. 71184	0	10. 28816	9- 77877	0	10, 22123	10, 06693	0	9- 93307	6
ñ	51 52	8 8	71205	0	28795	77906	10	22094	06701	0	93299	3
2	51 44	8 16	71226	1	28774	77935	T	22065	06709	0	93291	13
3	51 36	8 24	71247	1	28753	77963	1	22037	06716	0	93284	113
4	51 28	8 32	71268	1	28732	77992	2	22008	06724	1	93276	13
5	7 51 20	4 8 40	9. 71289	2	10, 28711	9. 78020	2	10, 21980	10, 06731	1	9. 93269	Ŀ
	51 12	8 48	71310	2	28690	78049	3	21951	06739	1	93261	H
7	51 4	8 56	71331	2	28669	78077	3	21923	06747	1	93253	L
	50 56	9 4	71352	3	28648	78106	4	21894	96754	1	93246	ı.
9	50 48	9 12	71373	3	28627	78135	4	21865	06762	1	93238	L
0	7 50 40	4 9 20	9. 71393	3	10, 28607	9. 78163	. 5	10. 21837	10.06770	1	9. 93230	١
1	50 32	9 28	71414	4	28586	78192 78220	5	21808	06777	1 2	93223	Ŀ
2	50 24	9 36	71435	4	28544	78249	6	21780	06785	2	93215	ı
3	50 16	9 44	71456	4	28523	78277	7	21751	06793	2	93207	ŀ
4	-		71477	5	10, 28502	9, 78300		10, 21694	10, 06808		93200	Ļ
5	7 50 0	4 10 0	9 71498	5	28481	78334	7 8	21666	06816	2 2	9, 93192	١
	49 52	10 16	71519	5	28461	78363	8	21637	65823	2	93104	ı
7 8	49 44 49 36	10 24	71500	6	28440	78391	9	21600	06831	2	93109	1
9	49 28	10 32	71581	7	28419	78419	9	21581	06839	2	93161	ı
0	47.	4 10 40	9. 71602	7	10. 28108	9. 78448	9	10. 21552	10, 05846	3	9-93154	ł
1	7 49 20		71622	5	28378	78476	10	21524	06854	3	93140	ı
ž I	49 4	10 48	71643	7	28357	78505	10	21495	06862	3	93138	1
3	48 56	11 4	71664	8	28336	78533	11	21467	06860	3	93131	1
4	48 48	11 12	71685	8	28315	78552	11	21438	06877	3	93123	ı
5	7 48 40	A 11 20	9. 71705	9	10, 28205	9. 78590	12	10, 21410	10, 06885	3	9-93115	î
6	48 32	11 28	71726	9	28274	76618	12	21382	06892	3	93108	ı
7	45 24	11 36	71747	9	28253	78647	13	21353	06900	3	93100	1
7	48 16	11 44	71767	10	28233	78675	13	21325	06908	.4	93092	ł
9	48 8	11 52	71788	10	28212	78704	14	21296	06916	4	93084	1
0.	7 48 0	4 12 0	9, 71809	10	10, 28191	9, 78732	14	10, 21268	10,05923	4	9-93077	Г
1	47 52	12 8	71829	11	28171	78760	15	11240	06931	4	93009	1
2	47 44	12 16	71850	11	28150	78789	15	21211	06939	4	93061	1
3	47 36	12 24	71870	11	28130	75817	16	21153	05947	4	93053	1
4	47 28	12 32	71891	12	28109	78845	16	21155	00954	4	93046	Į.
5	7 47 20	4 12 40	9. 71911	12	10. 28089	9, 78874	17	10, 21126	10, 05962	5	9. 93038	ı
Ó	47 12	12 48	71932	12	28068 28048	78902 78030	17	21098	06970 06978	5	93030	1
8	47 4	12 56	71952 71973	13	28027	75930	17	21070	00970	5	93022	ı
	46 56	13 4	71973	13	28005	78987	18	21013	00993	5	93014	ı
9		4 13 20	9. 72014	14	10, 27986	0. 79015	19	10, 20985	10, 07001	-	9. 92999	ł
0	7 46 40 46 32	13 28	72034	14	27966	79043	19	20957	07000	5	92999	ı
2	46 24	13 36	72055	14	27945	79072	20	20935	07017	2	91981	ı
3	46 16	13 44.	72075	15	27925	79100	20	20000	07024	5	02070	1
4	46 8	13 52	72096	15	27904	79128	21	25872	07032	6.	92968	1
5	7 46 0	4 14 0	9. 72116	15	10. 27884	9- 79156	21	10, 20844	10, 07040	6	9. 92960	t
6	45 52	14 8	72137	16	27863	79185	22	20815	07048	6	92952	1
7	45 44	14 16	72157	16	27843	79213	22	20757	07056	6	92944	1
8	45 36	14.24	72177	16	27823	79241	23	20759	07064	6	92936	1
9	45 28	14 32	72198	17	27802	79209	23	20731	07071	6	92929	1
Ø.	7 45 20	4 14 40	9. 72218	17	10, 27782	9-79297	24	10, 20703	10, 07079	6	9, 92921	Ĩ
1.	45 12	14 48	72238	18	27762	79326	24	20074	07087	7	92913	1
2	45 4	14 56	72259	18	27741	79354	25	20646	07095	7 7	92905	1
3	44 56	15 4	72279	18	27721	79382	25	20518	07103		92897	1
4	44 48	15 12	72299	19	27701	79410	26	20590	07111	7	92889	1
5/0	7 44 40	4 15 20	g. 72320	19	10. 27680	9- 79438	26	10. 20562	10, 07119	7	9. 92881	1
0	44 32	15 aB	7#340	19	27660	79466	26	20534	07126	7 7	92874	ı
78	44 24	15 36	72360 72361	20	27640	79495	27	20505	07134	7	92866	1
0	44 I6	15 44 15 52	72301	20	27019	79523	27	20477	07142	7	92850	1
9	44 8	16 0	72421	21	27579	79579	28	20431	07158	8	02842	1
-	44	-		Diff.			-	-	11.0	Diff.		ţ.
r. I	Hour P. M.	Hour A. M.	Cosine.		Secant.	Cotangent.	DIff	Tangent.	Coccount,		Sine.	ī

12°						,						1470
-		-	r				1					_
х.	Hour A. M.	Hour P. M.	Sine.	Diff.	Concent.	Tangent,	Diff.	Cotangent.	Secant.	Diff.	Cosine.	M.
	7 44 0	4 16 e	9. 72421	0	10. 27579	9-79579	0	10. 20421	10. 07158	0	9. 92842	60
1 2	43 52 43 44	16 8 16 16	72441 72461	0	27559 27539	79607 79635	°	20393 203 <u>6</u> 5	07166 07174	°	92834 92826	58 58
3	43 36	16 24	72482	i	27518	79663	i	20337	07182		92818	37
. 4	43 28	16 32	72502	1	27498	79691	2	20309	07190	1	92810	57 56
ş	7 43 20	4 16 40	9. 72522 .	3	10. 27478	9. 79719	2	10, 20281	10.07197	1	9. 92803	55
	43 12	16 48 16 56	72542 72562	2 2	27458 27438	79747	3	20253	07205 07213	1	92795 92787	54
7	43 4 42 56	17 4	72582	3	27418	79776 79804	1 4	20196	07221	li	92779	53 52
9	42 48	17 12	72602	3	27398	79832	4	20168	07229	1	92771	Šī
10	7 42 40	4 17 20	9. 72622	3	10. 27378	9. 79860	5	10, 20140	10, 07237	1	9. 92763	50
111	42 32 42 24	17 28 17 36	72643 72663	4	27357 27337	79888 79916	5	20112	07245 07253	1 2	92755	#3
13	42 16	17 44	72683	1	27317	79944	6	20056	07201	2	92747 92739	47
14	42 8	17 52	72703	3	27297	79972	7	20028	07269	3	92731	47 46
15 16	7 42 0	4 18 0	9- 72723	5	10. 27277	9. 80000	7	10, 20000	10. 07277	-	9- 92723	45
	41 52	18 8	72743	ş	27257	80028 80056	7	19972	07285	2 2	92715	144
17 18	41 44 41 36	18 24	72763 72783	6	27237 27217	80084	8	19944	07293 07301	2	92707 92699	43 42
19	41 28	18 32	72803	6	27197	80112	9	19916 19888	07309	3	92691	4
20	7 41 20	4 18 40	9. 72823	7	10. 27177	9.80140	9	10. 19860	10. 07317	3	9. 92683	40
21 23	41 12	18 48 18 56	72843 72863	7	27157	80168 80195	10	19832	07325	3	92675	39 38
23	41 4 40 56	19 4	72883	7	27137 27117	80223	11	19777	97333 97341	3	92659	37
24	40 48	19 12	12902	8	27098	80251	111	19749	07349	3	92651	36
25	7 40 40	4 19 20	9. 72922	8	10. 27078	9. 80279	12	10. 19721	10. 07357	3	9. 92643	35
26	40 32 40 24	19 28	72942	9	27058	80307	12	19693	07365	3	92635	34
27 28	40 24 40 16	19 36 19 44	72962 72982	9	27038 27018	80335 80363	13	19665 19637	07373 07381	4	92627	33
29	40 8	19 52	73002	Ιó	26998	80391	13	19609	07389	1 4	92611	31
30	7 40 0	4 20 0	9. 73022	10	10. 26978	9. 80419	14	10, 19581	10. 07397	4	9. 92603	30
31	39 52	20 8 20 16	73041	10	26959	80447	14	19553	07405	4	92595 92587	29 28
32 33	39 44 39 36	20 24	73061 73081	11	26939 26919	80474 80502	15	19526 19498	07413 07421	4	92507	I ***
34	39 28	20 32	73101	11	26899	80530	16	19470	07429	3	92571	27 26
35 36	7 39 20	4 20 40	9. 73121	12	10. 26879	9. 80558	16	10, 19442	10. 07437	5	9. 92563	25
36	39 12	20 48 20 56	73140 73160	12	26860 26840	80586 80614	17	19414	07445	5	92555	1 24
37 38	39 4 38 56	21 4	73180	13	26820	80642	17	19358	07454 07462	5	92546 92538	23
39	38 48	21 12	73200	13	26800	80669	18	19331	07470	Š	92530	21
40	7 38 40	4 21 20	9. 73219	13	10. 26781	9. 80697	19	10. 19303	10. 07478	ş	9. 92522	20
41 42	38 32 38 24	21 28 21 36	73239 73259	14	26761 26741	80725	19	19275	07486	1 %	92514 92500	13
43	38 24 38 16	21 44	73278	12	26722	80753 80781	20	19247 19219	07494 07502	6	92498	1 ;;
44	388	31 52	73298	15	26702	80808	20	19192	07510	6	92490	:3
45	7 38 0	4 22 0	9. 73318	15	10, 26682	9. 80836	21	10. 19164	10, 07518	6	9. 92482	15
46	37 52 37 44	22 8	73337 73357	15	26663 26643	80864 8080a	21	19136	07527 07535	6	98473 98465	14
47 48	37 36	22 24 22 24	73377	16	26623	80919	23	19081	07535 07543	6	92457	13
49	37 28	22 32	73396	16	26604	80947	#3	19053	07551	7	99449	111
50	7 37 20	4 22 40	9. 73416	17	10. 26584	9. 80975	23	10, 19025	10. 07559 07567	7	9. 98441	10
51 52	37 12	22 48 22 56	7343 5 73455	17	26565 26545	81003 81030	24	18997 18970	07507	7	92433	1
53	37 4 30 56	23 4	73474	17	26526	81058	35	18942	07575 07584	7	92416	
54	36 48	23 12	73494	18	26506	81086	25	18914	07592	Ż	92408	ž
55 56	7 36 40	4 23 20	9. 73513	18	10. 26487	9. 81113	26	10, 18887	10, 07600	7	9, 92400	5
50	36 32 36 24	183 28 83 36	73533 73552	19	26467 26448	81141	26	18831	07603 07616	8	92392 92384	3
57 58	30 16	23 44	73572	13	26438	81 169 81 18	27	18804	07524	8	92376	ž
59	36 8	23 52	73591	80	26409	81224	27	18776	07633	8	92367	
	36 o	24 0	73611	20	26389	81252	28	18748	07641	8	92359	٥
ж.	Hour P. M.	Hour A. M.	Cosine.	Diff.	Secant.	Cotangent.	Diff.	Tangent	Cosecant.	DIE.	Sine.	×.
122	•											57°
										_		

10	Done i	Dane :	Sine.	Dia.	Comme	Towns	Diff.	Catanaget	Securit,	Diff	Cosine.	14
м,	Hour A. M.	Hour r. M.		-	Cosecant.	Tangent.	-			200		L
0	7 36 0	4 24 0	9. 73611	0	10. 26389	9. 81252	0	10. 18748	10. 07641	0	9. 92359	L
1	35 52	24 8	73630	0	26370	81279	0	18721	07649	0	92351	I
2	35 44	24 16	73650	1	26350	81307	1	18693	07657	0	92343	ŀ
3	35 36	24 24	73609	1	26331	81335	1.	18665	07665	0	91335	L
4	35 28	24 32	73689	1	26311	81362	2	18638	07674	1	92326	L
5	7 35 20	4 24 40	9. 73708	2	10. 26292	9. 81390	2	10, 18610	10, 07682	1	9. 92318	1
	35 12	24 45	73727	2	26273	81418	- 3	18582	07690	- 3	92310	ı
8	35 4 34 50	24 50	73747	2	26253	81445	3	18555	p7698	1	92302	ı
	34 50	25 4	73766	3	26234	81473	4	18527	07707	1	92293	ı
9	34 40	25 12	73785	3	26215	81500	4	18500	07715	1	92285	Į.
10	7 34 40	4 25 20	9. 70805	3	10, 26195	9.81528	5	10, 18472	10, 07723	1	9. 92277	ı
11	34 32	25 28	73824	3	26176	84556	5	18444	07731	2	92269	ł
12	34 24	25 36	73843 73863	4	26157	81583	5	18417	07740	2	92260	ł
13	34 16	25 44	73882	4	26137	81611	6	18389	07748	2	92252	ı
14	379	- 3.3		4		81638	-	18362	07750	-	92244	Į.
15	7 34, 0	4 25 0	9. 73901	5	10, 26099	9, 81666	7	10. 18334	10. 07765	2	9-92235	٠
16	33 52	26 8	73921	5	26079	81693	8	18307	07773	2	92227	ı
17	33 44	26 16 26 24	73940	5	26060 26041	81721	8	18279	07781	2	92219	١
	33 36		73959	6	26022	81748		18252	07789 07798	3	92211	l
19	33		73978			81776	9			3		ŀ
20 -	7 33 20	4 26 40	9-73997	- 6	10, 26003	9. 81803	9	10, 18197	10. 07806	3	9, 92194	۱
21	33 12	26 48	74017	7	25983	81858	10	18142	07814	3	92186	ı
12	33 4	26 56	74035	7	25964	81886	10	18114	07831	3	92177	l
23	32 56	27 4	74055	7 8	25945	81013	11	18087	07839	3	92169	ŀ
24	32 48	27 12	74074		-		-			3	-	ŀ
25	7 32 40	4 27 20	9- 74093	8	10. 25907	9. 81941	11	10, 18059	10. 07848	3	9, 92152	ı
26	32 32	27 28	74113		25887	81968	12	18033	07856	4	92144	ı
27 28	32 24	27 36	74132	9	25868	81996	12		07864	4	92136	ŀ
20	32 16 22 8	27 44	74151	9	25830	82023 82051	13	17977	07881	4	02110	۱
-			74170				13	17949	10. 07889			Į.
30	7 32 0	4 28 0	9. 74189	10	10. 25811	9. 82078	14	10. 17922	07898	4	9. 92111	L
31	31 52	28 8 28 16	74208	10	25792	82133	14	17504		4		ľ
32	31 44 31 36	28 24	74227	10	25773	82161	15	17839	07906	5	92094	ı
33	31 36 31 28	28 32	74265	11	25754 25735	82188	15	17812	07923	5	92077	ı
14		- 46		11	10, 25716	9. 82215	16	10. 17785	10. 07931	-	9. 92069	ł
35	7 31 20	4 28 40 28 48	9- 74284	111	25607	82243	16	17757	07940	5	92060	1
10		28 56	74393	12	25678	82270	17	17730	07945	5	92000	ı
17	30 56	29 4	74341	12	25659	82208	17	17702	07956	5	92044	۱
39	30 48	20 12	74360	12	25640	82325	18	17675	07965	3	92035	ı
	7 70 40	4 20 20		-	10, 25621		18	10. 17648	10. 07973	6	9. 92027	ł
40	7, 30 40	29 28	9-74379	13	25602	9. 82652		17620	07982	6	92018	١
41	30 32	29 36	74395 74417	13	25553	82407	19	17593	07992	6	92010	۱
13	30 16	29 44	74436	14	25564	S2435	20	17565	07998	6	92010	١
14	30 8	29 52	74455	14	25545	82462	20	17538	08007	6	91093	۱
	- 0	4 30 0	9- 74474	14	10. 25526	9, 82489	21	10. 17511	10, 08015	6	9. 91985	ŀ
5	7 30 a	30 8		15		82517	21	17483	08024	6	91970	۱
17	29 44	30 16	74493	15	25507 25488	82544	22	17450	08032	7	91993	١
47	29 36	30 24	74531	15	25469	82571	23	17429	08041	7	91959	۱
19	20 28	30 32	74549	18	25451	82500	22	17401	08040	7	01051	1
50	7 20 20	4 30 40	9- 74568	16	10, 25432	9. 82626	23	10, 17374	10, 08058	7	9, 91042	ŕ
12	29 12	30 48	74587	16	25413	82653	23	17347	08006	7	91934	ı
52		30 56	74606	17	25304	82681	24	17319	08075	7	91934	1
53	29 4	31 4	74625	17	25375	81708	24	17292	08083		91917	۱
53	28 48	31 12	74644	17	25350	82735	25	17205	08092	7	91903	ı
55	7 28 40	4 31 20	9- 74662	17	10. 25338	0.82762	25	10. 17238	10, 08100	8	9. 91900	ŕ
56	2ff 32	31 28	74681	15	25319	\$2700	20	17210	08100	8	gillas	1
57	25 24	31 36	74700	18	25300	82817	26	17183	08117	8	18210	I
50-	28 16	31 44	74719	18	25281	82844	27	17150	08126	8	91874	1
59	28 8	31 52	74737	10	25263	82871	27	17120	08134	8	91866	ĺ
60	28 0	32 0	74756	10	25244	82899	27	17101	08143	8	91857	ı
- 5	-	Hour s. H.	Cosine.	Diff.	Secant.	Cotangent.	-	Tangent.	Constant.	Diff.	Sine.	ŀ
đ.	Hour F. M.											

84°											1	45°
М.	Hour a. m.	Hour P. M.	Sine.	Diff.	Conocant.	Tangent.	Diff.	Cotangest.	Secant	Diff.	Couine,	M.
0	7 28 o	4 32 0	9. 74756	٥	10. 25244	9. 82899	٥	10, 17101	10, 08143	0	9.91857	60
1 2	27 52 27 44	32 8 32 16	74775	0	25225 25206	82926 82953	0	17074 17047	08151 08160	°	91849 91840	59 58
3	27 36	32 24	74794 74812	i	25188	82980	i	17020	08168		01812	57 56
4	27 28	32 32	74831	1	25169	83008	2	16992	08177	1	91823	
5	7 27 20 27 13	4 32 40 12 48	9- 74850 74868	2 2	10, 25150 25132	9. 83035 83062	3	10. 16965 16938	10, 08185	1	9. 91815 91806	55 54
		32 56	74887	2	25113	83089	3	16911	08202	i	91798	53
8	26 (6	33 4	74906	2	25094	83117	4	16883	08211	1	91789	52
9 10	26 48 7 26 40	33 12 4 33 20	74924 9-74943	3	25076 10. 25057	83144 9. 83171	4	16856	08219	1	91781	51 50
111	26 32	4 33 20 33 28	74961	3	25039	83198	5	16802	08237	2	91763	40
12	26 24	33 36	74980	4	25020	83225	5	16775 16748	08245	2	91755	49 48
13	26 16 26 8	33 44 33 52	74999 75017	4	25001 24983	83252 83280	6	16748	08254 08262	2 2	91746 91738	47 46
15	7 26 0	4 34 0	9. 75036	3	10, 24964	9, 83307	7	10. 16693	10, 08271	1 2	9. 91 729	45
16	25 52	34 8	75054	5	24946	83334 83361	Ž	16666	08280	2	91720	44
17	25 44 25 36	34 16 34 24	75073	ş	24927	83361 83388	8	16639 16612	08288 08297	3	91712	43
19	25 28	34 24 34 32	75091 75110	6	24909 24890	83415	ا ا	16585	08305	3	91695	42 41
20	7 25 20	4 14 40	9. 75128	6	10, 24872	9.83442	9	10. 16558	10. 08314	3	9. 91686	40
21	25 12	34 48	75147	6	24853	83470	9	16530	08323	3	91677	39 38
22 23	25 4 24 56	34 56 35 4	75165 75184	7	24835 24816	83497 83524	10	16503 16476	08331 08340	3	91660	30
24	24 48	35 12	75202	۱ 'n	24798	83551	11	16449	08349	3	91651	37 36
25	7 24 40	4 35 20	9. 75221	8	10. 24779	9. 83578 83605	11	10. 16422	10, 08357	4	9.91643	35
26 27	24 32 24 24	35 28 35 36	75239 75258	8	24761 24742	83632	12	16395 16368	08366 08375	4 4	91634	34 33
28	24 16	35 44	75276	9	24724	83659 83686	13	16341	08181	4	91617	32
29	24 8	35 52	75294	9	24706	83686	13	16314	08392	4	91608	31
30	7 24 0 23 52	4 36 0	9- 75313	9	10. 24687 24660	9. 83713 83740	14	16287	10. 08401 08409	4	9. 91599	30 20
31 32	23 52 23 44	36 8 36 16	75331 75350	10	24650	83768	14	16232	08418	3	91582	28
33	23 36	36 24	75368	10	24632	83795	15	16205	08427	5	91573	27 26
34	23 28	36 32	75386	10	24614	83822 9.83849	15	16178	08435 10, 08444	1.5	91565	25
35 36	7 23 20 23 12	4 36 40 36 48	9- 75405 75443	11	10, 24595 24577	83876	16	16124	08453	5	91547	22
37 38	23 4	36 56	7544 I	11	24559	83903	17	16097	08402	5	91538	23
38 39	22 56 22 48	37 4 37 12	75459 75478	12 12	24541 24522	83930 83957	17	16070 16043	08470 08479	1 8	91530	22 21
40	7 22 40	4 37 20	9- 75496	12	10. 24504	9. 83984	18	10. 16016	10, 08488	1 6	9.91512	20
41	22 32	37 28	75514	13	24486	84011	i8	15989	08406	6	91504	19 18
42	22 24 22 16	37 36	75533	13	24467. 24449	84038 84065	19	15962 15935	08505 08514	6	91495 91486	18
43 44	22 8	37 44 37 52	75551 75569	13	24431	84092	20	15908	08523	6	91477	ié
45	7 22 O	4 98 0	9. 75587	14	10, 24413	9. 84119	20	10. 15881	10. 08531	7	9.91469	15
46	21 52 21 44	38 8 38 16	75605 75624	14 14	24395 24376	84146 84173	21	15854 15827	08540 08549	7	91460 91451	14
47 48	21 36	38 24	75642	15	24358	84200	22	15800	82280	1 7	91442	12
49	21 28	38 32	75660	15	24340	84227	22	15773	08567	1 7	91433	11
50	7 21 20	4 38 40 38 48	9. 75678	15 16	10. 24322	9. 84254 84280	23	10, 15746	10. 08575 08584	7	9. 91425 91416	10
51 52	21 12 21 4	38 56	75696 75714	16	24304 24286	84307	23	15720 15693	08593	1	01407	8
53	21 4 20 56	39 4	75733	16	24267	84334	24	15666	08602	8	91398 91389	7
54	20 48	39 12	75751	17	24249	84361	24	15639	10.08610	8		
55 56	7 20 40	4 39 20 39 28	9. 75769 75787	17	10. 24231 24213	9. 84388 84415	25. 25	10, 15612	08628	8	9.91381	5
57 58	20 24	39 36	75805	17	24195	84442	26	15558	08617	8	91363	3
58	20 16 20 8	39 44	75823 75841	18	24177	84469 84496	26	15531	08646 08655	8	91354 91345	1
59 60	20 0	39 52 40 0	75859	18	24159 24141	84523	27	15504	08664	9	91336	6
м.	Hour P. M.	Hour A. M.	Cosine.	Diff.	Secant.	Cotangent.	Diff.	Tangent.	Cosecant.	Diff.	Sibe.	×.
						1						
194	•											55°

320												1140
И.	Hou A. M.	llour p. M.	Sine	DIE.	Cosecant.	Tangent.	Diff.	Cotangent.	Secant.	Diff.	Cosine.	Ħ.
0	7 20 0	4 40 0	9. 75859	0	10, 24141	9. 84523	0	10. 15477	10, 08664 08672	0	9. 91336	60
1	19 52 19 44	40 8 40 16	75877 75895	0	24123 24105	84550 84576	0	15450 15424	08672	:	91328	59 58
3	19 36	40 24	75913	1	24087	84576 84603	1	15397	08690	0	91310	57
14.	19 28	40 32	75931	1	24069	84630	2	15370	08699	1	91301	50
5	7 19 20	4 40 40	9- 75949 75967	I g	IQ. 24051 24033	9. 84657 84684	3	10. 15343 15316	10. 08708 08717	1	9. 91292	55 54
7 8		40 56	75985	3	24015	84711	3	15289	08726	i	91274	53
	19 4 18 56 18 43	41 4	76003	2	23997	84738	4	15262	08734	ا ! ا		52
9	7 18 40	41 12	76021 9. 76039	3	23979 10, 23961	9, 84764	4	15236	08743 10. 08752	1 2	91257	51
11	18 32	41 28	76057	3	23943	84818	5	15182	08761	2	91239	40
12	18 24	41 36	76075	4	23925	84845	5	22121	oS770	2	91230	48
13 14	18 16	41 44 41 52	76093 76111	4	23907 23889	84872 84899	8	15128 15101	o5779 o8788	2 2	91212	47 46
	7 18 0	4 42 0	9. 76129	4	10. 23871	9. 84925	7	10. 15075	10. 05797	1 2	9. 91203	45
15 16	17 52	42 8	76146	5	23854	84952	Ž	15048	08806	2	91194	44
17	17 44 17 36	42 16 43 24	76164	5	23836 23818	84979 850x6	8	15021 14994	08815 08824	3	91185	43 42
10	17 28	43 24 42 42	76200	5	23800	85033	8	14967	08833	3	91170	47
20	7 17 20	4 42 40	9. 76218	6	10, 23782	9. 85059 85086	9	10. 14941	10, 08842	3	9. 91158	40
21	17 12	42 48	76236	6	23764	85086	9	14914	o8851 o8859	3	91149	39
23	17 4 16 56	42 56 43 4	76253 76271	6	23747 23729	85113 85140	10	14887 14860	08868	3	91141	38 37
24	16 48	43 12	76289	7	23711	85166	11	14834	08877	4	91123	36
25	7 16 40	4 43 20	9. 76307	7	10. 23693	9. 85193	11	10. 14807	10. 08886	4	9. 91114	35
26 27	16 32 16 24	43 23 43 36	76324 76342	8	23676 23658	85220 85247	12	14780 14753	08895 08904	4	91 105 91000	34 33
28	16 16	43 44	76360	8	23640	85273	12	14727	08913	4	91087	32
29	16 8	43 52	76378	9	23622	85,300	13	14700	08922	4	91078	١,
30 31	7 16 0 15 52	4 44 ° 44 8	9. 76395 76413	9	23587	9. 85327	13	10. 14673	10. 08931 08940	5	0. 010(x)	30 29
32	15 44	44 16	76431	9	23569	85354 85380	14	14620	08949	5	12010	28
33	15 36	44 24	76448	10	23552	85407	15	14593	08958 08907	5	91042	27 26
34	7 15 20	44 49	76466 9. 76484	10	23534 10, 23516	85434 9, 85460	15	14565 10. 14540	10. 08977	5	91033 C. 91023	25
35 36	15 12	44 48	76501	11	23499	85487	16	1451 (o8986	5	91014	24
37 38	15 4	44 56	76519	11	23481	85514	16	14486	08995	6	91005	23
38 39	14 56 14 48	45 4 45 12	76537 76554	11	23463 23446	85540 85567	17	1446a 14433	09004	6	90990 90987	22
40	7 14 40	4 45 20	9. 76572	12	10. 23428	9. 85594	18	10, 14406	10. 09022	6	9. 90978	20
41	14 32	45 28	76590	12	23410	85620	18	14380	09031	6	90969	19
42 43	14 24 14 16	45 36 45 44	76607 76625	12	23393 23375	85647 85674	19	14353 14325	ono40 oro49	اۃ	90960 90951	18 17
44	14 8	45 52	76642	13	#3373 #3358	85700	20	14300	09058	1	90942	ić
45 46	7 14 0	4 46 0	9. 76660	13	10. 23340	9. 85727	20	10. 14273	10. 09067	7	9. 90033	15
40	13 52 13 44	46 8 46 16	76677 76695	14	23323 23305	85754 85780	20 21	14246	09076 09085	7 7	90924	14
47 48	13 36	46 24	76712	14	23288	85807	21	14193	00094	7	90906	12
49	13 28	46 32	76730	14	23270	85834	22	14166	09104	7	90896	11
50 51	7 13 20 13 12	4 46 40 46 48	9- 76747 76765	15	10. 23253 23235	9. 85860 85887	22	10. 14140	10, 09113	8	9. 90887 90878	10
52		46 56	76782	15	23218	85913	23	14087	09131	8	90869	8
53	12 56	47 4	76800	16	23200	85940	24	14060	09140	8	90560	7
54	7 12 48	47 12	76817 9. 76835	16	23183 10, 23165	85967	24	14033	10, 09158	8	90851 9. 90842	_
55 56	7 12 40 12 32	4 47 ±0 47 ±8	9. 76835 76852	16	23148	9. 85993 86020	24 25	13080	09158	8	90832	5 4
57 58	12 24	47 36	76870	17	23130	86046	25	13954	09177 09186	9	90083	3
58	12 16 12 8	47 44	76887	17	23113 23090	86073 86100	só só	13927	09195	9	90814	1
59	12 0	47 52 48 0	76904 76922	17	23073	86126	87	13900 13874	09195	9	90796	6
и.	Hour P. M.	Hour A. M.	Corine.	Diff.	Secant.	Cotangent.	Diff.	Tangent.	Cosecant.	DIF.	Sine	и.
							لت			لب		54.
125°												96

86°												148°
M.	Houra. M.	Hour P. M.	Sine.	Diff.	Cossonst.	Tangent.	Diff.	Cotangent.	Secant.	Diff.	Cosine.	¥.
٥	7 12 0	4 48 0	9. 76922	٥	10. 23078	9. 86126	0	10. 13874	10. 09204	٥	9. 90796	60
I 2	11 52 11 44	48 8 48 16	76939 76957	م ا	23061 23043	86153 86179	0	13847 13821	09213	0	90787	59 58
3	11 44 11 36 11 28	48 24	76974	1	23026	86206 86232	1	13794 13768	09232	0	90768	57 56
- 21	7 11 20	48 32	76991 9. 77009	1	23009	9. 86259	3	10, 13741	10. 09250	H	9º759 9- 9º750	55
ş	11 12	48 48	77026	2	22974	86285	3	13715	09259	1	90741	54
7	10 56	48 56 49 4	77043 77061	2	22957 22939	86312 86338	3	13688 13662	09269 09278	1	90731	53 52
9	10 48	49 12	77078	3	22922	86365	1	13635	09287	ī	90713	51
10	7 10 40	4 49 20	9. 77095	3	10. 22905	9. 86392 86418	4	10. 13608	10, 09296	2 2	9-90704	50
11	10 32 10 24	49 28 49 36	77112 77130	3	22570	86445	5 5	13582 13555	09306 09315	2	90694 90685	49 48
13	10 16	49 44	77147	4	22853	86471	6	13529	09324	2	90676	47 46
14 15	10 8 7 10 0	49 52 4 50 0	77164 9. 77181	4	22836	86498 9. 86524	7	13502	09333 10, 09343	2 2	9. 90657	45
16	9 52	50 8	77190	5	22801	86551	7	13449	09352	2	90648	44
17 18	9 44 9 36	50 16 50 24	77216	5	22784 22767	86577 86603	7	13423	09361 09370	3	90639 90630	43 43
19	9 28	50 32	77233 77250	5	22750	86630	8	13397 13370	09380	3	90620	41
20	7 9 20	4 50 40	9. 77268	6	10. 22732	9. 86656 86683	9	10. 13344	10. 09389	3	9. 90611	40
21 22	9 12	50 48 50 56	77285 77302	6	22715 22698	8670g	10	13317	09398 094 0 6	3	90502 90592	39 38
23	8 56	51 4	77319	7	22681	86736	10	13264	09417	4	90583	37 36
24	8 48 7 8 40	51 12 4 51 20	77336	7	22664 10. 22647	86762 g. 86789	11	13238	09426 10. 09435	4	90574 9. 90565	30 35
25 26	8 32	4 51 20 51 28	9- 77353 77379	7 7	22630	86815	111	13185	09445	1	90555	33
27 28	8 24 8 16	51 36	7737° 77387	8	22613	86842 86868	12	13158	09454	4	90546	33
29	8 8	51 44 51 52	77405 77422	8	22595 22578	86894	12	13132 13106	09 163 09473	5	90537 90527	32 31
30	780	4 52 0	9-77439	9	10. 22561	g. 86g21	13	10. 13079	10. 09482	5	9. 90518	30
31 32	7 52 7 44	52 8 58 16	77456 77473	9	22544 22527	86947 86974	14	13053 13026	09491	5	90509	29 28
33	7 36	52 24	77490	9	22510	87000	15	13000	09510	5	90490 90480	27 26
34	7 28	52 32	77507	10	22493	87027	15	12973	09520	5	9.90471	26 25
35 36	7 7 20 7 12	4 52 40 52 48	9. 77524 77541	10	10. 22476 22459	9. 87053 87079	15 16	12021	10, 09529 09538	8	90462	24
37 38	₹ 58	52 56	77558	111	22442	87106	16	12894 12868	09548	6	90452	23 22
39	6 48.	53 4 53 12	77575 77592	111	22425 22408	87132 87158	17	12842	09557 09566	6	90443 90434	21
40	7 6 40	4 53 20	9, 77600	11	10. 22391	9. 87185	18	10, 12815	10. 09576	6	9. 90424	20
41 42	6 32	53 28 53 36	77626 77643	12	92374 92357	87211 87238	18	12789	09585 09595	6	90415	19 18
43	6 16	53 44	77660	12	22340	87264	19	12736	09604	7	90396 90386	17 16
44	7 6 0	53 52 4 54 0	77677 9. 77694	13	92323 10, 82306	87290	19	12710	10. 09623	7	90386 9-90377	16
45 46	7 6 0 5 52	54 8	9. 77094	13	22289	9. 87317 87343	20	12657	09632	7	90368	14
47 48	5 44	54 16	77728	13	22272	87369	21	12631	00642	7	90358	13
49	5 36 5 28	54 24 54 32	77744 77761	14	22256 22239	87396 87422	21 23	12604 12578	09651 09661	7	90349 90339	111
SÓ	7 5 20	4 54 49	9. 77778	14	10, 22222	9. 87448	22	10, 12552	10.00670	8	9. 90330	10
51 52	5 I2,	54 48 54 56	77795 77812	15 15	22205 22188	87475 87501	22 23	12525 12499	09680 09680	8	90320	8
53	4 56	55 4	77829	15	22171	87527	23	12473	09699	8	90301	7
54	4 48	55 12	77846 9. 77862	15	22154	87554	24	12446	09708	8	90292	
55 56	7 4 40 4 32	4 55 20 55 28	77879	16	10. 22138 22121	9. 87580 87606	24	10. 12420 12394	. 10. 09718 09727	9	90273	5
57 58	4 24	55 36	77896	16	22104	87633	25 26	12367	09737	9	90263	3 2
50	4 16	55 44 55 52	77913 77930	16 17	22087 22070	87659 87685	26	12341 12315	09746 09756	9	90254 90244	1
59 ∞	4 0	55 52 55 0	77946	17	22074	87711	26	12289	09765	ģ	90235	٥
ж.	Hour P. M.	Hour a. M.	Cosins.	Diff.	Secant.	Cotangent.	Diff.	Tangent.	Cosecant.	Diff.	Sine.	×.
126	•											53°

87.				•		•					,	142*
×.	Hour A. M.	Hour P. M.	Sine.	Diff.	Concent.	Tangent,	Diff	Cotangent.	Secant.	Diff.	Cosine.	м.
1	7 4 0	4 56 0	9. 77946	0	10. 22054	9. 87711		10, 12280	10. 09765		9. 90235	60
ĭ	3 52	56 8	77062		22037	87738		12262	99775	0	90225	59 58
2	3 44 3 36	56 16 56 24	77980 77997	1	22020 22003	87764 87790	1	12236 12210	09784 09794	q	90216 90206	58 57
3	3 36 3 28	56 32	78013	;	21987	87817	;	12183	09803	ĭ	90197	36
5	7 3 20	4 56 40	9. 78030	-	10. 21970	9. 87843	2	10. 12157	10. 09813	•	9. 90187	55
	3 12 3 4	56 48 56 56	78047 78063	2 2	21953 21937	87869 87895	3	12131	09822 09832	1	90178 90168	54 53
7	2 56	57 4	78080	9	21920	87922	3	12078	09841	1	90159	52
9 10	7 2 40	57 12 4 57 20	78097 9. 78113	3	21903	87948 9. 87974	4	12052	10. 09861	1 3	90149	51 50
11	2 32	57 28	78130	3	21870	88000	5	12000	00870	3	90130	42 48
12	8 24 2 16	57 36	78147 78163	3	21853 21837	88027 88053	1	11973 11947	09880 09880	2	90120	48
13 14	2 8	57 44 57 52	78180	;	21820	88079	6	1194/	09899	-	90101	46
15 16	7 2 0	4 58 0	9. 78197	4	10. 21803	9. 88105	7	10. 11895	10. 09909	3	9. 90091	45
	I 52 I 44	58 8 58 16	78213 78230	5	21787 21770	88131 88158	7	11869 11842	09918 09928	3	90082	44
17 18	1 30	58 24	78246	5	21754	88184	7	11816	09937	3	90061	42
19 20	1 28 7 1 20	58 32 4 58 40	78263 9. 78280	5	21737	9. 88236	8	11790	09947 10. 09957	3	90053	41 40
21	1 12	58 48	78296	965	21704	88262	9	11738	09906	3	90034	39
22	0 56	58 56	78313	6	21687 21671	88289 88315	10	11711	09976 09586	1	90024	38
23 24	0 48	59 4 59 12	78329 78346	7	21654	88341	10	11659	99995	1 2	90005	37 36
25	7 0 40	4 59 20	9. 78362	7	10. 21638	9. 88367	11	10. 11633	10. 10005	4	9. 89995	35
26 27	0 32 0 24	59 28 59 36	78379 78395	7	21621 21605	88393 88420	11	11607 11580	10015	4	89985 89976	34 33
28	0 16	59 44	78412	8	21588	88446	12	11554	10034	5	89966	32
29	0 8	59 52	78428	8	21572	88472 9. 88498	13	11528	10044	5	89956 9. 89947	31 30
30 31	7 0 0 6 59 52	5 0 0	9. 78445 78461	;	10. 21555 21539	88524	13	11476	10063	5	89937	29 28
32	59 44	0 16	78478	9	21522	88550	14	11450	10073 10082	5	89927 89918	
33 34	59 36 59 28	0 24	78494 78510	9	21506 21490	88577 88603	14	11423	10092	3	89908	27 26
35	6 59 20	5 0 40	9- 78527	10	10. 21473	9. 88629	15	10. 11371	10. 10102	ě	9. 89898	25
36	59 12	0 48	78543 78560	10	21457 21440	88655 88681	16 16	11345 11319	10112	6	89888 89879	24
37 38	59 4 58 56	1 4	78576	10	21424	88707	17	11293	10131	6	89869	22
39	58 48	1 12	78592 9. 78609	11	21408	88733 9. 88759	17	11267	10. 10151	6	89859 9. 89849	21
40 41	6 58 40 58 32	5 1 20 1 28	78625	11	10. 21391 21375	88786	18	11214	10160	7	89840	19
42	58 24	1 36	78642	12	21358	88812	18	11188	101 70 10180	7	89830 89820	18
43 44	58 16 58 8	I 44 I 52	78658 78674	12	21342 21326	888 38 88864	19	11162	10180	7	89810	17 16
45 46	6 58 0	5 2 0	9. 78691	12	10. 21 309	9. 88890	20	10. 11110	10. 10199	7	9, 89801	15
46	57 52	2 8 2 16	78707 78723	13	21293	88916 88942	20	11084 11058	10209	7	89791 89781	14
47	57 44 57 36	2 24	78730	13	21261	88g68	21	11032	10229	8	89771	12
49	57 28	2 32	78756	13	21244	88994 9, 89020	21	11006	10239	8	89761 9. 89752	11
50 51	6 57 20 57 12	5 2 40 2 48	9. 78772 78788	14	10. 21228 #1212	89046	22	10. 10980	10258	8	89742	3
52	57 4	2 56	78805 78821	14	21195	80073	23	10927	10268	8	89732 89722	
53 54	56 56 56 48	3 4	788 17	15	21179 21163	89099 89125	23	10901	10278	9	89712	. 6
55 56	6 56 40	5 3 20	9. 78853	15	10. 21147	9, 89151	24	10. 10849	10, 10298	9	9. 89702	5
56	56 32 56 24	3 28 3 36	78869 78886	15	21131	89177 89203	24 25	10823	10307 1031 <i>7</i>	9	89693 89683	4 3
57 58	56 16	3 44	78902	16	21098	89229	25 26	10771	10327	9	89673 89663	2
59	56 8 56 o	3 52 4 0	78918 78934	16 16	21082	89255 89281	26	10745	10337 10347	10 10	89663 89653	;
M.	Hour P. M.	Hour A. M.	Cosine.	Diff.	Secant.	Cotangent.	Diff.	Tangent.	Concent.	Diff.	Sine.	ъ.
197												52°
										_		

SINES, TANGENTS, AND SECANTS.												
88°				,		,						1410
ж.	HOUTA M.	Hour P. M.	Sine.	Diff.	Cossoant.	Tangent.	Diff.	Cotangent.	Secent	Diff.	Cosine.	ж.
0	6 56 o	5 4 0	9. 78934	-	10. 21066	9 89281	0	10. 10719	10. 10347		0.80612	60
1	55 52	4 8	78950 78907	0	21050	89307	ě	10003	10357 10367	o	89643 89633 89624	59 58
3	55 44 55 36	4 16	78967 78983	1	21033 21017	89333 80350	:	10667	10367	ı °	89633	58
4	55 28	4 32	78999	1	21001	89359 89385	2	10615	10376 10386	1	89614	57 56
ş	6 55 20 55 12	5 4 40 4 48	9. 79015 79031	I	10. 20985 20969	9. 89411 89437	2	10. 10589	10. 10396 10406	1	9. 89604	55 54
7 8		4 48 4 56	79047	2	20053	89463	3	10537	10416	1	89594 89584	53
	54 56	5 4 5 12	79063 79079	2 2	20937 20921	89489 89515	3	10511	10426 10436	1 2	89574 89564	52 51
10	54 48 6 54 40	5 5 20	9. 79095	3	10. 20905	9. 89541	4	10. 10459	10, 10446	3	9. 89554	50
11	54 32	5 28	79111	3	20889 20872	89567	5	10433	10456	2	89544	49 48
12 13	54 24 54 16	5 36 5 44	79128 79144	3	20856	89593 89619	8	10407 10381	10466 10476	2 2	89534 89524	48
14	54 8	\$ 52	79160	4	20840	89645	6	10355	10486	2	89514	47 46
15	6 54 0 53 52	5 6 0	9. 79176 79192	4	10, 20824 20808	9. 89671 89697	6 7	10. 10329	10. 10496	3	9. 89504 80405	45 44
17	53 44	6 16	79208	5	20792	89723	ź	10277	10515	3	89495 89485	43
18	53 36 53 28	6 24 6 32	79224 79240	5	20776 20760	89749 89775	8	10251	10525 10535	3	89475 89465	43 41
20	6 53 20	5 6 40	0. 70256	ş	10, 20744 20728	9. 89801	9	10, 10199	10, 10545	3	9. 89455	40
21	53 12 53 4	6 48	79272 79288	6	20728	89827 89853	9	10173	10555	:	89445 89435	39 38
23	52 56	7 4	79304	6	20696	89879	10	10121	10575	1	89425	37 36
24	52 48	7 12	79319	7	20681	89905 9. 89931	10	10095	10, 10595	4	89415 9.89405	
25 26	52 32	5 7 20 7 28	9- 79335 79351	1 7	20649	89957	;;	10043	10605	1	89395 89385	35 34
27 28	52 24	7 36	79367	1 7 1	20633 20617	89983 90009	13	10017	10615 10625	5	89385	33 i
20	52 16 52 8	7 44 7 52	79383 79399	7 8	2001/ 20601	90035	13	09991 09965	10636	5	89375 89364	32 31
30	6 52 0	5 8 0	9- 79415	8	10, 20585	9. 90061	13	10. 09939	10, 10646	3	9. 89354	30
31 32	51 52 51 44	8 8 8 16	7943I 79447	8	20569 20553	90086	13	09914 09888	10656 10666	5	89344 89334	29 28
33	51 36	8 24 8 32	79463 79478	9	20537	90138 90164	14	09862	10676 10686	566	89324	27 26
34	51 28 6 51 20	8 32 5 8 40	9-79494	9	20522	9. 90190	15	09836 10, 09810	10. 10696	1 8	89314 9. 89304	25
35 36	51 12	8 48	79510	10	20490	90216	15 16	09784	10706	6	89294 89284	24
37 38	51 4 50 56	8 56	79526 79543	10	20474 20458	90242	16	09758 09732	10716 10726	6	89284 89274	23
39	50 48	9 12	79558	10	20442	90294	17	09706	10736	7	89264	21
40 41	6 50 40 50 32	5 9 20 9 28	9- 79573 79589	11	10. 20427 20411	9. 90320 90346	17	10. 09680	10. 10746 10756	7	9. 89254 89244	20
43	50 24	9 36	79605	11	20395	90371	18	09629	10767	7	89233	19 18
43 44	50 16 50 8	9 44	79624 79636	11	20379 20364	90397	19	09603 09577	10777	7	89223 89213	17 16
45 46	6 50 O	5 10 0	9. 79652	12	10. 20348	9. 90419	19	10. 09551	10, 10797	8	0. 80202	15
46	49 52 49 44	10 8	79668 79684	12	20332 20316	90475 90501	20	09525 09499	10807	8 8	89193 89183	14 13
48	49 36	10 24	79699	13	20301	90527	21	09473	10827	8	89173	12
50	49 28 6 49 20	5 10 40	79715 9- 79731	13	20285	90553 9. 90578	21	09447 10. 09422	10838 10, 10848	8	89162 9.89152	11
51	49 12	10 48	79746	14	20254	90604	22	09396	10858	9	89142	8
52 53	49 4 48 56	10 56 11 4	79762 79778	14	20238	90630 90656	22	09370 09344	10868 10878	9	89132 89123	
54	48 48	11 12	79793	14	20207	90682	23	09318	10888	9	89112	8
55 56	6 48 40	5 II 20 11 28	9. 79809 79825	15	10, 20191	9. 90708	24	10. 09292 09266	10. 10899	9	9. 89101	5
57	48 32 48 24	11 36	70840	15	20175 20160	90734 90759	24 25	09241	10909	10	. 8008t	3 2
58	48 24 48 16 48 8	11 44	79856 79872	15	20144 20128	90759 90785 90811	25 26	09215	10929	10	89071 89000	2
59 60	48 0	11 52 12 0	79872	16	20113	90837	26	09163	10940 10950	10	89050	6
м.	Hour P. M.	Hour A. M.	Cosine.	Diff.	Secant.	Cotangent.	Diff.	Tangent.	Cosecant.	Diff.	Sine.	X.
138			·		<u>' </u>	•	•		· <u>-</u> -			51°

M.	Houra.M.	Hour v. M.	Sine.	Diff.	Cosecant.	Tangent.	Diff.	Cotangent.	Secant.	Dur.	Coune	ы
1.00	-			-			-				7 111100	-
0	6 48 0 47 52	5 12 0 12 8	9. 79887	0	20097	9. 90837	0	10. 09103	10, 10050	0	9. 89050	6
2	47 44	12 16	79903	1	20082	go88g	i i	09137	10970	0	89930	5
3	47 36	12 24	79934	ī	20066	90914	1	09086	10980	1	Sgngo	5
4	47 28	12 32	79950	1	20050	90940	2	одоба	10991	1	89009	1 3
5	6 47 20	5 12 40	9- 79955	1	10, 20035	9. 90906	2	10, 09034	10, 11001	1	9, 88999	5
	47 12	12 48	79981	2	20019	90992	3	09008	11011	1	88989	5
7	47 4	12 56	79996 80012	2	20004	91018	3	08982	11022	1	88978	5
9	46 48	13 4	80012	2	19988	91043	3	p8957 p8931	11032	1 2	88968 88958	5
10	6 45 40	13 12			19973		4	10, 08905	10. 11052	2	g. 88g48	240
11	46 32	5 13 20 13 28	9, 80043 80058	3	10, 19957	9.91095	5	08879	11003	2	88937	13
12	46 24	13 36	80074	3	19926	91147	5	08853	11073	2	88927	4
13	46 16	13 44	8008g	3	19911	91172	5	08828	11083	2	88017	14
14	46 8	13 52	80105	4	19895	91198	6	688oz	11094	2	85906	4
15	6 46 0	5 14 0	9. 80120	4	10, 19880	9. 91224	6	10. 08776	10, 11104	3	9. 88896	4
16	45 52	14 8	80136	4	19864	91250	7	68750	11114	3	88836	4
17	45 44	14 16	80151 80166	4	19849	91276	7	08724	11125	3	88875 88865	13
19	45 36 45 28	14 24	80182	5	19834	91301	8	08673	11135	3	88855	4
20	6 45 20	5 14 40	9. 80107		10. 19803	9. 91353	9	10. 08647	10, 11156	3	9, 88844	3
11	45 12	14 48	80213	5	19787	91353	9	08521	11166	4	88834	3
22	45 4	14 56	80228	56	19772	91404	9	08596	17176	4	83824	3
23	44 56	15 4	80244	6	19756	91430	10	08570	11187	4	88813	3
24	44 48	15 12	80259	6	19741	91456	10	08544	11197	4	88803	3
25	6 44 40	5 15 20	9. 80274	6	10. 19726	9. 91482	11	10, 08518	10, 11207	-4	9.88793	3
26	44 32	15 28	80290	7	19710	91507	11	08491	11218	5	88782	13
17	44 24 44 16	15 36	80305 80320	7	19695	91533	12	08467 08441	11228	5	88772 88761	3
20	44 8	15 44 15 52	80336	7 7	19664	91559	12	08415	11249	5	88751	13
30	6 44 0	5 16 0	9. 80351	8	10, 19549	9.91610	13	10, 08390	10, 11259	5	9. 88741	3
31	43 52	16 8	80366	8	19634	91636	13	08704	11270	5	88730	В
32	43 44	16 16	80382	8	19618	91662	14	08338	11280	5	88720	1
33	43 36	16 24	80397	8	19603	91688	14	08313	11291	6	88709 88699	13
34	43 28	16 32	80412	9	19588	91713	15	08087	11301	6	58699	13
35	6 43 20	5 16 40	9. 80428	9	10, 19572	9, 91739	15	10, 08261	10, 11312	6	g. 88658 88678	3
36	43 12	16 48 16 56	80443 80458	9	19557	91705	15	p8235 p8200	11322	6	88668	
37	43 4 42 56	17 4	80473	10	19542	91791	16	pS184	1,1343	7	88657	l :
39	42 48	17 12	80489	10	19511	91842	17	08155	11353	7	88647	
40	0 42 40	5 17 20	9. 80504	10	10, 19496	9. 91868	17	10. 05132	10, 11364	7	9, 88636	1
11	42 32	17 28	80519	10	19481	91893	18	08107	11374	7	83625	3
f 2	42 24	17 36	80534	11	19466	91919	18	08081	11385	7	88615	ŀ
43	42 16	17 44	80550	11	19450	91945	18	08055 08020	11395	7 7 8	88504 88504	13
4	42 8	17 52	80565	11	19435	91971	19		11406	8	9, 58584	ъ.
5	6 42 0	5 48 0 18 8	9, 80580	12	10, 19420	9. 91996	19	10, 08004	10, 11416	8	83573	B
17	42 52 41 44	18 16	80505	12	19405	92048	20	07978	11427	8	88563	Ġ
8	41 16	18 24	80625	13	19375	92073	21	07932	31448	8	88552	
9	41 28	18 32	80641	13	19359	92099	21	07901	11458	9	83542	
10	6 41 20	5 18 40	9. 80656	13	10, 19344	9. 92125	21	10. 07875	10, 11469	9	9-88531	r
11	41 12	18 48	80671	13	19329	92150	22	07850	11479	9	88521	1
12	41 4 40 56	18 56	80686	13	19314	92176	22	07824	11490	9	88510 88499	П
3	40 48	19 4	80701 80716	14	19299	92202	23	07798	11501	9	88489	1
4	40 40	19 12		14				07773	10. 11522	10	9. 88473	1
50	40 32	5 19 20 19 28	9. 80731 80746	14	10, 19269	9. 92253	24	07721	11532	10	88468	1
7	40 32	19 36	80762	14	19254	92379	24	07696	11543	10	88457	1
57	40 16	19 44	80777	15	19223	92330	25	07570	11553	10	88447	1
9	40 8	19 52	80792	15	19208	92356	25	07644	11554	10	88430	1
0	40 0	20 0	80807	15	19193	92381	26	07619	31575	10	88425	1
L	Hour e. st.	Bour A. M.	Cosine	Diff.	Secant.	Cotangent.	Diff.	Tangedt.	Cosecant.	Diff.	Sine.	
			- warmed		Account.	- mg	1		222000	100	- C. LINE	1

CITATIO	TANGENTS	A KIT	CITY OF A NUMBER

40°											1	39"
ж.	Hour a. M.	Hour P. M.	Sine.	DIF.	Cosecant.	Tangent.	Diff.	Cotangent.	Secant.	Diff.	Cosine.	M.
•	640 0	.5 20 O	9. 80807	•	10. 19193	9. 92381	۰	10.07619	10. 11575	0	9. 88425	60
1 2	39 52 39 44	20 8 20 16	80822 80837	0	19178	92407 92433	0	07593 07567	11505	0	88415 88404	59 58
3	30 36	20 24	80812	1	19148	92458	1	07542	11606	1	88394	57
4	39 28-	20 32	80867	1	19133	92484	2	07516	11617	-	88383 9.88372	56
ş	6 39 20	5 20 40 20 48	9, 80882 80897	1	10. 19118	9. 92510 92535	3	10. 07490 07465	11638	1	9. 88372 88362	55 54
7	39 4 38 56	20 56	80912	2	19088	92561	3	07439	11649	1	88351	53
	38 56 38 48	2I 4	80927 80942	2	19073 19058	92587	3	07413 07388	11660 11670	:	88340 88330	52 51
10	6 38 40	5 21 20	9. 80957	3		9. 92638	4	10. 07362	10, 11681	1	9. 88319	30
11	38 32	21 28	80972	3	10. 19043 19028	92663	5	97337	11692		88308	49 48
12	38 24 38 16	21 36	80987 81002	3	19013	92689	\ {	07311	11702	2	88298 88287	
13	38 8	21 44 21 52	81017	3	18983	92740	6	07260	11724	3	88276	47 46
15	6 38 0	5 22 0	9. 81032	4	10, 18968	9. 92766	6	10. 07234	10, 11734	3	o. 88266	45
16	37 52	22 8 22 16	81047 81061	4	18953 18939	92792 92817	7	07208	11745	3	88255 89244	44
17	37 44 37 36	22 10	81076	4	18924	92843	7	07157	11756	3	88274	43 43
19	37 28	22 32	81091	5	18909	92868	8	07132	11777	3	88223	41
20	6 37 20	5 22 40	9. 81106 81121	5	10. 18894	9. 92894	9	10, 07106 07c80	10, 11788	4	9. 88212 88201	40
21	37 12 37 4	22 48 22 56	81136	5	1886₄	92920 92945	9	07055	11799	4	88101	39 38
23	36 56	23 4	81151	8	18849	92971	10	07029	11820	4	88180	37
24	36 48	23 12	9, 81180	6	18834 10, 18820	92996	10	07004	11831	4	88169 9.88158	36
25 26	6 36 40 35 32	5 23 20 23 28	81195	6	18805	9. 93022 93048	!!	10. 05978 06952	. 11852	5	88148	35 34
27	16 24	23 36	81210	7	18790	93073	12	06927	11863	5	88137	33
28	36 16 36 8	23 44	81225 81240	7	18775 18760	93099 93124	12	06901 06876	11874	5	88126 88115	32
29 30	6 36 0	23 52 5 24 0	9. 81254	7	10. 18746	9. 93150	13	10. 06850	10. 11895		0. 88105	31 30
31	35 52	24 8	81269	7	18731	93175	13	06825	11906	ş	88004	29
32	35 44	24 16	81284 81299	8	18716 18701	93201 93227	14	06799	11917	6	88083 88072	28 27
33 34	35 36 35 28	24 24 24 32	81314	8	18686	93252	14	06773 06748	11939	6	83o61	26
	6 35 20	5 24 40	0. 81 128	9	10, 18672	9. 93278	15	10. 06722	10, 11949	6	9. 88051	25
35 36	35 12	24 48	81343 81358	9	18657 18642	93303	15	06697 06671	11960	6	88040 88029	24
37 38	35 4 34 56	24 56 25 4	81372	9	18628	93329 93354	16	06646	11982	7	85018	2 j 22
39	34 48	25 12	81 387	10	18613	93380	17	06620	11993	1	88007	21
40	6 34 40	5 25 20	9. 81402	10	10. 18598	9. 93406	17	10.06594	10. 12004	7	9. 87996 87985	20
41 42	34 32 34 24	25 28 25 36	81417 81431	10	18583 18569	93431 93457	17	06569 06543	12015	7	87975	19
43	34 16	25 44	81446	11	18554	93482	18	06518	12036	8	87964	17
44	34 8	25 52	81461	11	18539	93508	19	06492	12047	8	87953	16
45 46	6 34 0 33 52	5 26 0 26 8	9. 81475 81490	11	10, 18525 18510	9- 93533 93559	19	10. 06467 06441	10: 12058	8	9. 87942 87931	15
47	33 44	26 16	81505	12	18495	93584	20	06416	1208ó	8	87920	13
48	33 36 13 28	26 24 26 12	81519 81534	12	18481 18466	93610 93636	20	06390 06364	12091	9	87909 87898	12
49 50	6 33 20	26 32 6 26 40	9. 81549	12	10. 18451	9. 93%1	21	10. 06339	10, 12113	9	9. 87887	10
51	33 12	26 48	81563	13	18437	93687	22	06313 06288	12123	9	87877	2
52	33 4	26 56	81578 81592	13	18422 18408	93712 93738	23	06288	12134 12145	100	87866 87855	
53 54	32 56 32 48	27 4 27 12	81007	13	18393	93730	23	06237	12156	10	87844	7
55 56	6 32 40	5 27 20	9, 81622	14	10. 18378	9. 93789	23	10, 06211	10. 12167	10	9. 87833	5
56	32 32 32 24	27 28	81636 81651	14	18364 18349	93814 93840	24	06160	12178	10	87822 87811	4 3
57 58	32 '24 32 16	27 36 27 44	81005	14	18335	93865	25	06135	12200	10	87800	1 2
59	32 8	27 52	81680	15	18320	93891	25	06109	12211	11	87789	1
_	32 0	28 0	81694	15	18306	93916	26	06084	12222	11	87778	°
M.	Hour P. M.	Houra. M.	Cosine.	Diff.	Secant,	Cotangent.	Diff.	Tangent.	Coeecant.	Diff.	Sine.	M.
130	•											49*

SINES, TANGENTS, AND SECANTS.												
41*											1	188°
M.	Hour A. M.	Hour P. M.	Sine.	Diff.	Conscant.	Tangent.	DIF.	Cotangent.	Secant.	DW.	Cosine.	M.
	6 32 0	5 28 0	9. 81694	۰	10. 18306	9. 93916	۰	10, 06084	10. 12222	۰	9.87778	60
1	31 52	28 8 28 16	81709 81723	°	18291	93942 93967	0	06058 06033	12233 12244	0	87767	59 58
3	31 44 31 30	28 24	81738	ĭ	18277 18262	93993 94018	i	06007	12255	i	87756 87745	57 56
4	32 28	28 32	81752	1	18248			05982			87734	
ş	6 31 20	5 28 40 28 48	9. 81767 81781	1	10. 18233 18219	9. 94044 94069	3	10. 05956 05931	10. 12277		9. 87723 87712	55 54
7		28 56	81796 81810	3	18204	94095	3	05905 05880	12299	1	87701	53
9	31 4 30 56 30 48	29 4 20 12	81810 81825	3	18190 18175	94120 94146	3	05880 05854	12310 12321	1 2	87690 87679	52 51
10	6 30 40	5 29 20	0, 81820	2	10. 18161	9.94171	4	10. 05829	10, 12332	2	9.87668	50
11	30 32	29 28	81854 81868	3	18146 18132	94197 94222	5	05803 05778	12343	2 2	87657 87646	49 48
12	30 24 30 16	29 36 29 44	81882	3	18118	94248	ş	05752	12354 12365	2	87635	47
14	30 8	29 52	81897	3	18103	94273	6	05727	12376	3	87624	46
15 16	6 30 0 29 52	5 30 0 30 8	9. 81911 81926	4	10. 18089 18074	9. 94299 94324	6 7	10. 05701	10. 12387	3	9. 87613 87601	45 44
17	29 44	30 16	81940	4	18060	94350	ź	05650	12410	3	87590	43
18	29 36 29 28	30 24 30 32	81955 81969	4 5	18045 18031	94375 94401	8	05625 05599	12421 12432	3	87579 87568	42 41
30	6 29 20	5 30 40	0. 81081		10. 18017	9. 94426	8	10. 05574	10. 12441	4	9. 87557	40
21	29 12	30.48	81998	5	18002 17988	94452	9	10. 05574 05548	12454 12465	4	87546	39 38
23	29 4 28 56	30 56 31 4	82012 82026	5	17974	94477 94503	10	05523 05497	12470	4	87535 87524	37
24	25 45	31 12	82041	ş	17959	94528	10	05472	12487	4	87513	37 36
25	6 28 46 28 32	5 31 20 31 28	9. 82055 82069	6	10. 17945 17931	9- 94554	11	10. 05446 05421	10, 12499	5	9. 87501 87490	35 34
27 28	28 24	31 36	82084 82098	6	17916	94579 94604	11.	05396	12521	5	87479 87468	33
	28 16 28 8	31 44	82098 82112	7 7	17902	94630 94655	12	05370 05345	12532 12543	1 5	87468 87457	32 31
29 30	6 28 o	31 52 5 32 0	9. 82126	+	10. 17874	9. 94681	13	10.05319		1 8	9. 87446	30
31	27 52	ີ 12 8 8	82141	7	17850	94706	13	05294 05268	10, 12554 12566	6	87434	29 28
32 33	27 44 27 36	32 16 32 24	82155 82169	8	17845 17831	94732	14	05200	12577 12588	6	87423 87412	20
34	27 28	32 32	82184	8	17816	94757 94783	14	05217	12599	6	87401	27 26
35 36	6 27 20 27 12	5 32 40 32 48	9. 82198 82212	8	10, 17802 17788	9. 94808 94834	15	10. 05192	10, 12610	7	9. 87390 87378	25 24
37 38		32 56	82226	9	17774 17760	94859 94884	15	05141	12611	7	87367	23
	27 4 26 56 26 48	33 4	82240 82255	9	17760 17745	94884	16	05116	12644 12655	7	87356 87345	22
39 40	6 26 40	33 12 5 33 20	9. 82269	10	10, 17731	9- 94935	17	10, 05065	10, 12666	7	9. 87334	20
41	26 32	33 28	82283	10	17717	94961	17	05039	12678 12689	8	87322	19 18
42 43	26 24 26 16	33 36 33 44	82297 82311	10	17 7 03 17689	95012	18	05014 04988	12700	8	87311 87300	17
44	s 6 8	33 57	82326	10	17674	95037	19	04963	12713	8	87288	16
45 46	6 a6 o a5 52	5 34 ° 34 8	9. 82340 82354	11	10, 17660 17646	9. 95062 95088	19	10.04938	10, 12723	8	9. 87277 87266	15 14
47		34 16	82354 82368	11	17612	95113	20	04912 04887	12745	9	87255	13
48 49	25 44 25 36 25 28	34 24 34 32	82382 82396	11	17618 17604	95139 95164	20	04861 04836	12757	9	87243 87232	12
50	6 25 20	5 34 40	9. 82410	12	10. 17590	9. 95190	21	10. 04810	10. 12779	9	9. 87221	10
51	25 12	34 48	82424	12	17576	95215	22	04785	12791	10	87209 87198	8
52 53	25 4 24 56	34 56 35 4	82439 82453	12	17561	95240 95266	22	04760 04734	12802	10	87187	7 6
53 54	24 48	35 12	82467	13	17533	95291	23	04700	12825	10	87175	
55 56	6 24 40 24 32	5 35 20 35 28	9. 82481 82495	13	10, 17519	9- 95317 95342	23	10. 04683 04658	10. 12836	10	9. 87164 87153	5
57 58	24 24 24 16	35 36	82509	14	17491	95368	24	04632	12850	11	87141	3 2
58	24 16 24 8	35 44	82523	14	17477 17463	95393 95418	25	04607 04582	12870 12881	11	87130 87119	1 1
59 60	24 0	35 52 36 0	82537 82551	14	17403	95444	25	04556	12893	111	87107	6
M.	Hour + M.	Hour A. M.	Cosine.	Diff.	Secant.	Cotangent.	Diff.	Tangent.	Cosecant.	DIF.	Sine.	M.
131				_				<u></u>			·	48°

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SINKS.	TANGENTS.	AND SECANT	Я.

49°												187
м.	Houra. M.	Hour p. M.	Sine.	Diff.	Cosecant.	Tangent.	DIF.	Cotangent.	Secant.	Diff.	Cosine.	₩.
0	6 24 0	5 36 0 36 8	9. 82551 82565	:	10. 17449	9- 95444	0	10. 04556	10, 12893 12004	0	9. 87107	60
اف	23 44	36 16	82570	ő	17435 17431	95469 95495	ĭ	04531 04505	12915		87096 87085	59 58
3	23 36 23 28	36 24	82593 82607	1	17407	95520	1 2	04480	12927	1	87073	57 56
4	6 23 20	36 32 5 36 40	9. 82621	÷	17393	95545 9-95571	2	10. 04429	12938	H	87062 9. 87050	55
5	23 12	36 48	82615	1	17365	95596	3	04404	12961	ī	87039	54
8	23 4 22 56	36 56 37 4	82649 82663	3	17351 17337	95622 95647	3	04378 04353	12973 12984	1 2	87028 87016	53 52
9	22 48	37 12	82677	2	17323	95672	4	04328	12995	3	87005	51
10	6 22 40 22 32	5 37 20 37 28	9. 82691 82705	3	10. 17309	9.95698	4	10. 04302	10. 13007	2 2	9. 86993 86982	50
12	22 24 23 16	37 28 37 36	82719	3	17295 17281	95723 95748	5	04277 04252	13030	2	86970	49 48
13	22 16 22 8	37 44	82733	3	17267	95774	5	04226	13041	3	86050	47 i
14	6 22 0	37 52 5 38 0	82747 9, 82761	3	17253	95799 9. 95825	1 6	04201 10. 04175	13053 10, 13064	3	86947 9. 86936	46 45
15 16	21 52	388	82775 82788	4	17225	95850	7	04150	13076 13087	3	86924	44
17	21 44 21 36	38 16 38 24	82788 82802	4	17212	95875 95901	7	04125	13087	3	86913 86902	43 42
19	21 28	38 32	82816	4	17184	95926	8	04074	13110	4	868go	41
20	6 21 20	5 38 40 38 48	9. 82830 82844	5	10. 17170	9- 95952	8	10.04048	10, 13121	4	9. 86879 86867	40
21 22	21 12	38 56	82858	5	17156	95977 96002	9	04023 03998	13133 13145	1 4	868<<	39 38
23	21 4 - 20 56	39 4	82872 82885	ş	17128	96028	10	03972	13156	4	86844	37 36
24 25	20 48 6 20 40	39 12 5 39 20	9. 82899	8	17115	96053	10	03947 10, 03922	13168	5	86832 9. 86821	36 35
28	20 32	39 28	82913	6	17087	96104	11	03896	13191	5	86809	33
·27 28	20 24	39 36	82927 82941	6	17073	96129	11	03871	13202 13214	5	86798 86786	33
29	20 8	39 44 39 52	82955	7	17059 17045	96155 96180	12	03845 03820	13225	8	86775	32 31
30	6 20 0	5 40 0	9. 82968	7	10. 17032	9. 96205	13	10.03795	10. 13237	6	9. 86763	30
31 32	19 52	40 8 40 16	82982 82996	7	17018 17004	96231 96256	13 14	03769 03744	13248 13260	6	86753 86740	29 28
33	19 36	40 24	83010	8	16990	96281	14	03719	13278	6	86728	27
34	89 28	40 32	83023	8	16977	96307	14	03693	13283	7	86717	26
35 36	19 20	5 40 40 40 48	9. 83037 83051	8	10, 16963 16949	9. 96332	15	10. 03668 03643	10. 13295 13306	7	9. 86705 86694	25 24
37 38	19 4	40 56	83065	8	16935	96357 96383	15 16	03617	13318	7	86682	23
38 39	18 56 18 48	41 4 41 12	83078 83092	9	16922 16908	96408 96433	16 16	03592 03567	13330 13341	7	86670 86659	22 21
40	6 18 40	5 41 20	9. 83106	9	10, 16894	9. 96459	17	10. 03541	10. 13353	8	9. 86647	20
41	18 32 18 24	41 28 41 36	83120 83133	9	16880 16867	96484 96510	17 18	03516	13365 13376	8	86035 86624	19 18
42 43	18 16	41 44	83147	10	16852	96535	18	03490 03465	13388	8	86612	
44	18 8	41 52	83161	10	16839	96560	19	03440	13400	8	86600	17 16
45 46	6 18 0 17 52	5 42 0 42 8	9. 83174 83188	10	10. 16826 16812	9. 96586 96611	19	10. 03414 03389	10. 13411	9	9, 86589 86577	15 14
47	17 44	42 16	83202	11	16798	96636	20	03364	13435	9	86565	13
48 49	17 36 17 28	42 24 42 32	83215 83229	11	16785 16771	96662 96687	20	03338 03313	13446 13458	9	86554 86542	12
50	6 17 20	5 42 40	9. 83242	11	10. 16758	9.96712	21	10, 03288	10. 13470	10	9. 86530	10
51	17 12	42 48	83256	13	16744	96738	22	03262	13482	10	86518	8
52 53	17 4 16 56	42 56 43 4	83270 83283	12	16730 16717	96763 967 <b>88</b>	22	03237 03212	13493 13505	10	86507 86495	7
54	16 48.	43 12	83297	12	16703	96814	23	03186	13517	10	86483	
55 56	6 16 40	5 43 20 43 28	9. 83310 83324	13	10, 16690 16676	9. 96839 96864	23 24	10. 03161 03136	10. 13528	11	9. 86472 86460	5
57 58	16 24	43 36	83338	13	16662	96890	24	03110	13552	11	86448	3
58	16 16	43 44	83351 83365	13	16649 16635	96915 96940	25 25	03085 03060	13564	11	86436 86425	2
59 60	16 0	43 52 44 0	83378	14	16622	96966	25	03034	13575 13587	12	80413	6
M.	Hour P. M.	Hour A. M.	Cosine.	DIF.	Secant.	Cotangent.	Diff.	Tangent.	Cosecant.	Diff.	Sine.	м.
182	•									-		41.

48°												138°
И,	Hour A. M.	Hour P. M.	Sine.	Diff.	Cosecant.	Tangent.	Diff.	Cotangent.	Secant.	Diff.	Cosine.	М.
٥	6 16 0	5 44 0	9. 83378	٥	10. 16622	9. 96966	۰	10, 03034	10. 13587	۰	9. 86413	60
1 2	15 52 15 44	44 8 44 16	83392 83405	0	16608 16595	96991 97016	°	03009	13599	l °	86401 86389	59 58
3	15 36	44 24	83419	1	16581 16568	97042	i	02958	13623	1	86377	57
4	15 28	44 32	83432	1		97067	2 2	02933	13634	<u>'</u>	80300	56
5	6 15 20	5 44 40 44 48	9. 83446 83459		10. 16554 16541	9. 97092 971 18	3	10. 02908 02882	10. 13646 13658	1	9. 86354 86342	55 54
7	15 4	44 56	83473 83486	2	16527	97143 97168	3	02857	11670	1 1	86330	53
8	14 56 14 48	45 4 45 12	83486	2 2	16514 16500	97168 97193	3 4	02832 02807	13682 13694	2 3	86318 86306	52 51
10	6 14 40	5 45 20	9. 83513	3	10. 16487	9. 97219	4	10, 02781	10. 13705	1	9. 86295	50
11	14 32	45 28	83527	2	16473	97244	5	02756	13717	2	86283	49 48
12	14 24 14 16	45 36 45 44	83540 83554	3	16460 16446	97269 97295	5	02731 02705	13729 13741	3	86271 86259	48 47
14	14 8	45 52	83567	3	16433	97320	6	02680	13753	3.	86247	46
15	6 14 0	5 46 0	9. 83581	3	10. 16419	9- 97345	6	10. 02655	10. 13765	3	9. 86235	45
17	13 52 13 44	46 8 46 16	83594 83608	4	16406	97371 97396	7	02629 02604	13777 13789	3	86223 86211	44 43
18	13 36	46 24	83621	4	16379	97421	8	02579	1 1800	1 4	86200	42
19	13 28	46 32	83634	4	16366	97447	8	02553	13812	4	86188	41
20	6 13 20	5 46 40 46 48	9. 83648 83661	4 5	16352	9. 97472 97497	8	10, 02528 02503	10. 13824	4	9.86176 86164	40
22	13 4	46 56	82674	5	16326	97523	9	02477	13848	7	86152	39 38
23	12 56 12 48	47 4	83688	5	16312	97548	10	02452	13860	5	86140	37
25	6 12 40	47 12 5 47 20	9. 83715	ş	16299	97573 9. 97598	10	02427	13872	5	86128 9. 86116	36 35
26	12 32	47 28	83728	6	16272	97624	111	02376	13896	5	86104	34
27 28	12 24 12 16	47 36	83741	6	16259	97649	11	02351	1 3908	5	86092 86080	33
29	12 8	47 44 47 52	83755 83768	6	16245 16232	97674 97700	12	02326	13920 13932	6	86068	32 31
30	6 12 0	5 48 O	9. 83781	7	10, 16219	9- 97725	13	10. 02275	10. 13944	6	9, 86056	30
31	11 52 11 44	48 8	83795	7	16205	97750	13	02250	13956	6	86044	29 28
32 33	11 44 11 36	48 16 48 24	83808 83821	7	16192 16179	977 <b>76</b> 97801	13	02224	13968 13980	6 7	86032 86020	27
34	11 28	48 32	83834	7 8	16166	97826	14	02174	13992	$\mathbf{i}$	86008	26
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37		48 48 48 56	81874	8	16139 16126	97877 97902	15 16	02123	14016	7	85984 85972	24
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43 44	10 16	49 41 49 52	83954 83967	10	16046 16033	98054 98079	18	01946	14100	9	85900 85888	17
	6 10 o	5 50 0	9. 83980	10	10, 16020	9, 98194	19	10, 01896	10, 14124	9	9, 85876	15
45 46	9 52	50 8	83993	10	16007	98130	19	01870	14136	9	85864	14
47 48	9 44 9 36	50 16 50 24	84006 84020	10	15994 15980	98155 98180	20	01845	14149	9	85851 85839	13
49	9 28	50 32	84033	1,1	15967	98206	21	01794	14173	*10	85827	11
50	6 9 20	5 50 40	9, 84046	11	10. 15954	9. 98231	21	10. 01 769	10, 14185	10	9. 85815	10
51 52	9 12	50 48 50 56	84059 81072	11	15941	98256 98281	22	01744 01719	14197 14209	10	85803 85791	8
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57 58	8 24	51 36	84138	13	15862	98408	24	01592	14270	111	85730	3
58	8 16 8 8	51 44	84151 84164	13	15849 15836	98433 98458	24	01567	14282 14294	12	85718 85706	2
59 60	8 0	51 52 52 0	84177	13	15823	98484	25 25	01542	14394	12	85693	6
M.	Hour r. M.	Hour A, M.	Cosine.	Diff.	Secant.	Cotangent.	_	Tangent.	Cosscant.	DIE.	Sine.	м.
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M.	Houra. M.	Hour r. m.	Sine.	D₩.	Cosecant.	Tangent.	Diff.	Cotangent.	Secant.	Diff.	Cosine.	M.
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1 2	7 52 7 44	52 8 52 16	84203		15797	98534 98560	i	01491 01466	14319 14331	:	8568r 85669	59 58
3	7 44 7 36 7 28	52 24 52 32	84216 84220	1	15784	98560 98585	I. 2	01440	14343	1	85657 85645	57 56
4	6 7 20	5 52 40	0, 84242	i	15771	9.98610	1	01415	14355 10. 14368	÷	9. 85632	55
8	7 12	52 48	84255 84269	1	15745	98635 98661	3	01 365	14380	1	85620 85608	54
8	6 56	52 56 53 4	84282	3	15731 15718	98686	3	01339	14392 14404	1 2	85596	53 52
9	6 48	53 12	84295	2	15705	98711	4	01289	14417	2	85583	51
10	6 6 40 6 32	5 53 20 53 28	9. 84308 84321	2 2	10. 15692 15679	9.98737 98762	5	10. 01263 01238	10. 14429 14441	2 2	9. 85571 85559	50
12	6 24	53 36	84334	3	15666	98787 98812	5	01213	14453 14466	2	85547	49 48
13 14	6 16	53 44 53 52	84347 84360	3	15653 15640	98812 98818	ş	01162	14466	3	85534 85522	47 46
	6 6 0	5 54 0	9. 84373	3	10. 15627	9.98863	6	10. 01137	14478 10. 14490	3	0. 85510	45
16	5 52	54 8	84385	3	15615	98888	7	01112	14503	3	85497	44
17	5 44 5 36	54 16 54 24	84398 84411	4	15602 15589	98913 98939	1 %	01087	14515 14527	4	85485 85473	43 42
19	5 28	54 32	84424	4	15576	98964	8	01036	14540	4	85460	41
20 21	6 5 20 5 12	5 54 40 54 48	9. 84437 84450	4 5	10. 15563 15550	9.98989 99015	8 9	10. 01011	10. 14552 14564	1 1	9. 85448	40
22	5 4	54 56	84463	3	15537	99040	اۋا	00960		5	85436 85423	39 38
23	4 56 4 48	55 4	84476	5	15524	99065	10	00935	14577 14589	Š	85411	37 36
24 25	6 4 40	5 55 20	84489 9. 84502	5	15511	9,99116	11	10. 00884	14601	5	85399 9. 85386	35
26	4 32	55 28	84515	ş	15485	99141	11	00859	14626	ş	85374	34
27 28	4 24 4 16	55 36 55 44	84528 84540	6	15472 15460	99166	11	00834	14639 14651	1 %	85361 85349	33 32
29	4 8	55 52	84553	6	15447	99217	12	00783	14663	6	85337	31
30	6 4 0	5 56 o 56 8	9. 84566	6	10. 15434	9.99242 99267	13	10.00758	10. 14676	6	9. 85324	30
31 32	3 52 3 44	56 16	84579 84592	7	15421 15408	99207	13	00733 00707	14000	7	85312 85200	29 28
33	3 36	56 24	84605	7	15395	99318	14	00707	14713	7	85299 85287	27 26
34	6 3 20	56 32 5 56 40	84618 9. 84630	7 8	15382	99343 9.99368	15	00657	14726	7	85274 9. 85262	25
35 36	3 12	56 48	84043	8	15357	99394	15	00606	14750	7 8	85250	24
37 38	3 4 2 56	56 56 57 4	84656 84660	8	15344 15331	99419 99444	16	00581 00556	14763	8	85237 85225	23
39	2 48	57 12	84682	8	15318	99469	16	∞531	14775 14788	8	85212	21
40	6 2 40	5 57 20	9. 84694	9	10. 15306	9.99495	17	10. 00505	10. 14800	8	9, 85200	20
41 42	2 32 2 24	57 28 57 36	84707 84720	9	15293 15280	99520 99545	17	00480 00455	14813	ا ۋ	85187 85175	19 18
43	2 16	57 44	84733	9	15267	99570	18	00430	14838	9	85162	17
44	6 2 0	57 52 5 58 0	84745 9. 84758	10	15255	99596	19	10. 00379	14850	9	85150 9. 85137	16
45 46	1 52	τ ₈ 8	84771	10	15220	99646	19	00354 00328	14875	10	85125	14
47 48	I 44 I 36	58 16 58 24	84784 84796	10	1 5216 15204	99672 99697	20	00328	14888	10	85112 85100	13 12
49	1 28	58 32	84809	11	15204	99097	21	00303 00278	14903	10	85087	11
50	6 1 20	5 58 40	9. 84822	11	10. 15178	9.99747	21	10. 00253	10. 14926	10	9. 85074	10
51 52	I 12	58 48 58 56	84835 84847	11	15165	99773 99798	21	00227	1 4938 14951	11	85062 85049	18
53	0 56	59 4	84860	11	15140	99823	22	00177	14963	11	83037	7
54 55	6 0 40	59 12 5 59 20	84873 9.84885	12	15127	99848	23	10, 00126	14976	11	85024 9. 85012	5
56	0 32	59 28	84898	12	15102	99899	24	00101	15001	12	84999	4
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